

RESEARCH MEMORANDUM

EFFECTS OF OPERATING PROPELLERS ON THE WING-SURFACE
PRESSURES OF A FOUR-ENGINE TRACTOR AIRPLANE CONFIGURATION HAVING A WING WITH 40° OF SWEEPBACK

By Carl D. Kolbe and Frederick W. Boltz

Ames Aeronautical Laboratory
Moffett Field, Calif.

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NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS

WASHINGTON

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CONFIDENTIAL

CONTENTAL

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EFFECTS OF OPERATING PROPELLERS ON THE WING-SURFACE

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SUMMARY

An investigation has been made to evaluate the effects of operating propellers and of nacelles on the wing-surface pressures on a semispan model of a four-engine tractor airplane configuration having a wing with 40° of sweepback and an aspect ratio of 10. The model represented the right-hand side of the airplane and had single-rotation right-hand propellers. The tests were conducted at Reynolds numbers of 4,000,000 and 8,000,000 at low speed and at Reynolds numbers of 1,000,000 and 2,000,000 for Mach numbers from 0.60 to 0.90.

At high thrust coefficients and a Mach number of 0.082, the propeller slipstream caused large changes in the spanwise distribution of loading over the region of the wing immersed in the propeller slipstream. The strong rotational components within the slipstream were responsible for inflections in the spanwise distribution of loading, there being large increases with increasing thrust coefficient in the normal force of those wing stations behind the up-going propeller blades with relatively small changes for sections behind the down-going blades. Consequently, the center of pressure moved inward with increasing thrust coefficient. At high subsonic Mach numbers, the over-all effects of operating propellers were not large when compared with the low-speed case.

The section data indicate that for most subsonic Mach numbers the addition of the nacelles (propellers removed) caused an increase in the normal-force curve slopes and an increase in the angle of attack for zero section lift.

INTRODUCTION

The aerodynamic problems associated with long-range airplanes designed to fly at high subsonic speeds have been the subject of a series of investigations in the Ames 12-foot pressure wind tunnel. These investigations (refs. 1 to 8) have dealt with the aerodynamic characteristics of several combinations of the components of a hypothetical airplane configuration with a sweptback wing, including the effects of operating propellers on the longitudinal characteristics (refs. 7 and 8). Measurements of the distribution of pressure over the wing have been included in these studies to provide loads data and to facilitate an understanding of the local flow phenomena on the wing. Pressure-distribution data for the wing without nacelles have been presented and analyzed in reference 3.

The present report is concerned with the effects on the wing-surface pressures of operating propellers, as well as the effects of adding nacelles and an extended split flap. The results of pressure-distribution measurements at nine semispan stations of the wing are presented and analyzed in the present report.

NOTATION

8.	mean-line	designation,	fraction	of chord		over which		the	design
	load is	uniform							

 $\frac{b}{2}$ wing semispan, perpendicular to the plane of symmetry

b' propeller-blade width

 C_L lift coefficient, $\frac{\text{lift}}{\text{qS}}$

ΔC_T change in lift coefficient

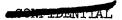
 ΔC_{Lg} change in lift coefficient attributable to the propeller slipstream (based on the total lift of the model with propellers operating less the lift component of the direct propeller force)

C_m pitching-moment coefficient about quarter point of the mean aerodynamic chord, pitching moment (See fig. 1(a).) qSc

 ΔC_m change in pitching-moment coefficient

 ΔC_{m_S} change in pitching-moment coefficient attributable to the propeller slipstream (based on the total pitching moment of the model with propellers operating less the pitching moment due to the direct propeller force)

Cx longitudinal-force coefficient, parallel to free-stream direction and positive in the dragwise direction, longitudinal force



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- c local wing chord, parallel to plane of symmetry
- c' local wing chord, perpendicular to the reference sweep line
- c_{av} average wing chord, parallel to the plane of symmetry, $\frac{2S}{b}$
- $\frac{1}{c} \qquad \text{mean aerodynamic chord, } \frac{\int_0^{b/2} c^2 dy}{\int_0^{b/2} c dy}$
- c_{l} , wing-section design lift coefficient
- cm section pitching-moment coefficient, cn (0.25 c.p.)
- cn section normal-force coefficient, section normal force
- Δc_{ng} change in section normal-force coefficient attributable to the propeller slipstream
- c.p. section center of pressure
- D propeller diameter
- h maximum thickness of propeller-blade section
- J propeller advance ratio, $\frac{V}{nD}$
- M free-stream Mach number
- n propeller rotational speed
- P pressure coefficient, P1 pq
- p, local static pressure
- p free-stream static pressure
- q free-stream dynamic pressure
- R Reynolds number, based on the wing mean aerodynamic chord
- R^t propeller-tip radius
- r propeller-blade-section radius
- S area of semispan wing
- T thrust per propeller, parallel to air stream

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T_{C}	thrust coefficient per propeller, $\frac{T}{\rho V^2D^2}$	
t	section maximum thickness	
V	free-stream velocity	•
У	lateral distance from the plane of symmetry	
α	angle of attack of the wing chord at the plane of (referred to herein as the wing-root chord)	symmetry
$\alpha_{\mathbf{u}}$	angle of attack of the wing-root chord at the plan uncorrected for tunnel-wall interference and ang counter correction	
β	propeller-blade angle, measured at 0.70 of the tip	radius
e t	propeller_blade_section angle	

- lp radius
- propeller-blade-section angle
- δ flap angle, measured relative to the local chord in planes normal to the reference sweep line
- angle of twist, measured in planes parallel to the plane of φ symmetry, positive for washin
- fraction of semispan, $\frac{2y}{\lambda}$ η
- spanwise location of the center of pressure, fraction of semispan
- ρ air density

MODEL

The semispan model represented the right-hand side of a hypothetical airplane. The geometry of the model is given in figure 1 and table I. The selection of the geometric properties and the details of the construction of the wing, fuselage, upper-surface fences, nacelles, and flaps have been discussed in references 1 through 4. Four upper-surface wing fences, as shown in figure 1(c), were used throughout the present investigation.

The wing was equipped with nine rows of pressure orifices on both the upper and lower surfaces (fig. 1(c)). The orifices were distributed along the chord from the leading edge to the 95-percent-chord point and were staggered one-eighth inch on either side of the station planes. There were no orifices in the extended trailing-edge flap.

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Each propeller in the two different sets used in this investigation had three blades and right-hand rotation. The propellers used for the tests at high subsonic Mach numbers (M = 0.60 and above) were the NACA 1.167-(0)(03)-058 supersonic propellers. For the tests at low subsonic Mach numbers, a thicker propeller, the NACA 1.167-(0)(05)-058, was used to withstand the very high blade loadings that accompany low-speed, high-density, wind-tunnel operation. The characteristics of these propellers and details of the motor-gearbox combination used to drive them are given in reference 6. Blade-form curves of the propellers are presented in figure 2 of this report.

Figure 3 is a photograph of the model mounted in the wind tunnel. The turntable upon which the model was mounted is directly connected to the force-measuring apparatus.

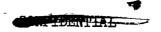
TESTS

The pressure-distribution data presented in this report were obtained simultaneously with the wind-tunnel balance measurements of the total lift, longitudinal force, and pitching moment on the model. Tests were made with the propellers operating and with the propellers removed, covering the range of conditions indicated in table II.

With the propellers operating, the Mach number, Reynolds number, and angle of attack were maintained constant while data were obtained at several selected thrust coefficients, T_c. Selection of the propeller rotational speeds to provide these thrust coefficients was based upon a previous propeller calibration in which the thrust characteristics of the propeller in the presence of the spinner and nacelle forebody were measured for the range of test conditions covered in tests of the complete model (see ref. 6). The results of the calibrations of the two different propellers that are pertinent to this report are presented in figures 4 and 5.

CORRECTIONS

The dynamic pressure, Mach number, and pressure coefficients have been corrected for constriction effects due to the presence of the tunnel walls by the method of reference 9. The force data have been corrected for tunnel-wall-interference effects originating from lift on the model and for drag tares caused by aerodynamic forces on the exposed portion of the turntable on which the model was mounted. The corrections that were applied to data obtained with propellers operating were the same as those reported in references 7 and 8. The corrections used



for the configuration with propellers removed are given in references 2 and 5.

The pressure data and the coefficients derived therefrom are presented in this report for values of uncorrected angle of attack $\alpha_{\rm U}$. The relation between the corrected and uncorrected angle of attack is as follows:

$$\alpha = 0.99 \alpha_0 + \Delta \alpha$$

The constant 0.99 is the ratio between the geometric angle of attack and the uncorrected reading of the angle-of-attack counter. The correction for the tunnel-wall interference is $\Delta \alpha$, and is defined as follows:

$$\Delta \alpha = 0.377 C_{Lwing}$$

where

$$C_{Lwing} = C_{Ltotal} - \Delta C_{LP}$$

and ΔC_{Lp} is the increment of lift coefficient due to propeller thrust and propeller normal force (obtained during the tests reported in ref. 6).

RESULTS AND DISCUSSION

The results of this investigation include a considerable amount of data obtained with the propellers removed, many of which serve as a base for comparison with comparable data obtained with propellers operating. It is convenient, therefore, to defer discussion of the effects of operating propellers until the propellers-off data have been presented and discussed. The latter data include the effects of nacelles and of an extended trailing-edge flap on both the local wing pressures and on the coefficients of lift, drag, and pitching moment.

Tabulated pressure data for nine spanwise stations of the wing (with and without operating propellers) are presented in tables III through XIX. Table II is an index to these data.

A portion of the lift, longitudinal-force, and pitching-moment data at Mach numbers of 0.86 and 0.90 were faired with dotted curves to indicate data obtained under conditions in which the wind tunnel may have been partially choked. It is to be understood that the corresponding pressure data fall within the same limitations of reliability.



Effects of Nacelles (Propellers Off)

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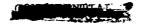
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Low speed .- The chordwise distributions of pressure coefficient in the region of the nacelles for a Mach number of 0.165 and a Reynolds number of 8,000,000 are compared with those of the wing-fuselage configuration (ref. 3) in figure 6. The corresponding coefficients of section normal force and section pitching moment, and of the total lift, longitudinal force, and pitching moment are presented in figure 7. The data in figure 6 indicate an increase in velocity over the lower surface of those stations in the vicinity of the nacelles. This increase in velocity became smaller with increasing angle of attack. As can be seen in figure 7, these velocity changes contributed to a reduction in the section loading for low angles of attack, an increase in the slopes of the lift and section normal-force curves, and an increase in the angle of attack for zero section lift. References 10 through 12 indicate the same effects for similar configurations. Data obtainable from table XV indicate that this effect diminished toward the wing tip. Further inspection of figure 6 reveals that, with the addition of nacelles to the wing, flow separation occurred on the upper surface at a lower angle of attack, with the attendant decrease in lift-curve slope and increase in drag (fig. 7).

The effect of the nacelles on the spanwise distribution of loading coefficient is shown in figure 8. The general nature of the inflection in the spanwise distribution of loading due to the nacelles is discernible; however, lack of pressure data over the nacelles prevents an accurate estimate of the changes in the location of the spanwise center of pressure. It is apparent, though, that such changes were small.

High speed.— The effects of the nacelles on the over-all force characteristics and section characteristics for Mach numbers ranging from 0.60 to 0.90 and a constant Reynolds number of 2,000,000 are shown in figures 9 through 12, respectively. Cognizance should be taken of the difference in Reynolds number between this and the preceding section. It was noted in reference 3 that for a Mach number of 0.25 the effect of this same change in Reynolds number was not large. A cross plot of the section normal-force data from these figures is presented in figure 13 as a function of Mach number.

In general, the effects of the addition of the nacelles for a Mach number of 0.60 were similar to those at low speed. The effects of increasing Mach number, however, were to reduce slightly the effect of the nacelles on both the section normal-force curve slopes and the angle of attack for zero lift.



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Effects of Flaps

The effects of an extended trailing-edge flap ($\delta = 30^{\circ}$) on the over-all force characteristics and on the section characteristics of the wing-fuselage-nacelles combination at a Mach number of 0.082 and a Reynolds number of 4,000,000 are shown in figure 14. Since no pressure measurements were made over the flap itself, estimates of the chordwise pressure distributions, similar to those shown in figure 15, were used to obtain the section coefficients. The effects of the flaps on the spanwise distribution of loading are shown in figure 16. It is evident that the flaps not only caused large increases in normal forces at those sections within the flap span ($\eta = 0.07$ to $\eta = 0.46$) but also caused substantial increases in loading over the outer portion of the wing. The center of pressure obviously moved inward a considerable distance when the flaps were deflected (fig. 16). Reference to figure 14(c) reveals that there was a large rearward movement of the section center of pressure in the region of the flaps. These changes had little effect on the wing pitching moments (fig. 14(a)).

Effects of Operating Propellers

Low speed. - The effects of operating propellers on the chordwise distribution of pressure coefficient in the region of the nacelles at a Mach number of 0.082 and a Reynolds number of 4,000,000 are shown in figure 17. The corresponding over-all force characteristics and section characteristics are shown in figure 18. Inspection of the data in figure 17 reveals that at the highest thrust coefficients ($T_c = 0.8$) the pressure distributions changed radically from those which existed with the propellers operating at $T_c = 0$ or with the propellers removed. Furthermore, increasing Tc also caused large changes in the stagnation pressure at the leading edge. Figure 18(b) shows that the propeller slipstreams caused large changes in the section normal-force coefficients and that those changes were not symmetrical over the portion of the wing immersed in the slipstreams as would be expected from simple axial-momentum theory. The asymmetrical effects of the operating propellers are further illustrated in figure 19 wherein the change in section normal-force coefficient due to propellers, $\Delta c_{n_{st}}$, is shown as a function of T_c . It may be seen that there were large increases in Δc_{ns} with increasing T_c at wing stations behind the up-going propeller blades (stations $\eta = 0.19$ and $\eta = 0.44$) at all angles of attack from 40 to 160. At wing stations behind the down-going 1 Cognizance should be taken of the fact that the total force and moment data in this and later similar figures include the effects of the pro-

Cognizance should be taken of the fact that the total force and moment data in this and later similar figures include the effects of the propeller thrust and propeller normal force as well as the effects of the propeller slipstream. (See refs. 7 and 8.)

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propeller blades ($\eta=0.31$ and $\eta=0.56$), $\Delta c_{\rm ng}$ decreased with increasing $T_{\rm c}$ at angles of attack below about $8^{\rm o}$ and increased only slightly with increasing $T_{\rm c}$ at higher angles of attack. These effects are indicative of the strong rotational components within the slipstream which change the effective angle of attack of the wing sections immersed in the propeller slipstream.

Figure 20 shows the effect of operating propellers on the spanwise distribution of the loading coefficient $c_n \frac{c}{c_{av}}$ for several angles of attack. The pronounced distortion of the spanwise distribution of load associated with increasing T_c is apparent. The effect of propeller operation on the spanwise center of pressure $\eta_{c.p.}$ is shown in figure 21. These data were obtained by integrating the loading data presented in figure 20, utilizing a straight-line fairing between the data points adjacent to the nacelles. The center of pressure moved inward with increasing T_c , the amount decreasing as the angle of attack was increased to 12° .

Figure 22 shows the importance of these aforementioned pressure-distribution changes with regard to the changes in the total lift and pitching-moment coefficients attributable to the operating propellers. It can be seen that the lift due to the propeller slipstream (ΔC_{L_B}) accounted for about 60 percent of the total change in lift with varying angle of attack; whereas the slipstream contribution to the change in pitching moment (ΔC_{m_B}) was apparently unaffected by increasing angle of attack.

High speed.— The effects of the operating propellers on the over-all force characteristics and section characteristics for Mach numbers from 0.70 to 0.90 for a constant Reynolds number of 1,000,000 are presented in figures 23 to 26. It is evident from the data in these figures that the effects of the operating propellers were not large compared to the propeller effects for the low-speed case. This is a consequence of the fact that the thrust coefficient is decreased considerably for the same power input.

The effects of increasing T_c on the chordwise distribution of pressure in the region of the nacelles are shown in figure 27 for a Mach number of 0.80. At the higher angles of attack, the apparent increase in pressure recovery for those stations between the nacelles might have been due to an increase in stagnation pressure caused by the operating propellers.

As indicated in figure 28, the effects of slipstream rotation at a Mach number of 0.80 on the spanwise distribution of loading were much less pronounced than in the previously cited low-speed case due to the lower values of thrust coefficient.



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CONCLUDING REMARKS

Measurements of the surface pressures and forces on a semispan model of a wing-fuselage-nacelles combination representing the right-hand side of a hypothetical four-engine airplane have been presented. The effects of single-rotation right-hand propellers, of nacelles, and of extended trailing-edge flaps on the wing-surface pressures have been discussed.

At high thrust coefficients and a Mach number of 0.082, the propeller slipstream caused large changes in the spanwise distribution of loading over the region of the wing immersed in the propeller slipstream. The strong rotational components within the slipstream were responsible for inflections in the spanwise distribution of loading, there being large increases with thrust coefficient in the normal force of wing sections behind the up-going propeller blades with relatively small changes for sections behind the down-going blades. As a result, the center of pressure moved inward with increasing thrust coefficient.

At high subsonic Mach numbers, the over-all effects of operating propellers were not large when compared with the low-speed case for the same power input; this is a direct consequence of the large reductions in thrust coefficient with increases in free-stream velocity.

The addition of the nacelles to the plain wing (propellers removed) increased the velocity over the lower surface at those stations in the vicinity of the nacelles. These velocity changes contributed to an increase in the slopes of the lift and normal-force curves and a general increase in the angle of attack for zero lift.

Deflection of extended trailing-edge flaps ($\delta = 30^{\circ}$) over the inner 46 percent of the wing semispan (propellers removed) produced substantial gains in section lift over the complete semispan. The wing pitching moments were little affected by the flap deflection.

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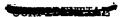


TABLE I.- GEOMETRIC PROPERTIES OF THE MODEL

Wing
Reference sweepline: locus of the quarter chords of sections inclined 40° to the plane of symmetry
Aspect ratio
Nacelles Frontal area (each)
Inclination (with respect to wing root chord)
Inboard
Propellers
Diameter
For low speed tests

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CONTRACT TO

Fuselage

TABLE I.- GEOMETRIC PROPERTIES OF THE MODEL - Concluded

_		
Fineness ratio		12.6
Frontal area (semispan	model)	0.273 ft ²
Fuselage coordinates:		

Distance from	Radius,
nose, in.	in.
0	0
1.27	1.04
2.54	1.57
5 . 08	2.35
10.16	3.36
20.31	4.44
30.47	4.90
39.44	5.00
50.00	5.00
60.00	5.00
70.00	5.00
76.00	4.96
82.00	4.83
88.00	4.61
94.00	4.27
100.00	3.77
106.00	3.03
126.00	0



TABLE II.- INDEX OF TABULATED PRESSURE COEFFICIENTS

Table No.	R × 10 ⁻⁶	М	$\mathtt{T}_{\mathtt{C}}$	Configuration	$\alpha_{ m u}$ range
III	4.0	0.082	0	Wing-fuselage-nacelles	2° to 16°
V V			.2 .4		Ī
AI	•		.6		
VIII	1.0	.80	.8 0		2 ⁰ to 10 ⁰
IX		.80	-04	<u> </u>	2° to 10°
X	↓	.90 .90	.03		2° to 8° 2° to 8°
XII	4.0	.082	Props off		20 to 200
XIV	1.0 1.0	.80	I		-2° to 20°
XV	8.0	.90 .165		<u> </u>	-2° to 20°
XVI	2.0	.80			-2° to 20°
XVII	2.0 8.0	.90 .165		Wing-fuselage	-2° to 10° -2° to 20°
XIX	4.0	.082	₩	Wing-fuselage-nacelles	2° to 20°
				plus extended split trailing-edge flap	

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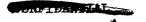
TABLE III.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. $M = 0.082; R = 4.000,000; T_c = 0$ (a) $\alpha_u = 2^{\circ}, 4^{\circ}, 6^{\circ}, 8^{\circ}, 10^{\circ}, 12^{\circ}$

	Per-				surface _			П				murface		
Spanwise stations	cent		l fo		fattack			ll				attack 80		150
0.10 b/2	0 1.5 7.0 10.0 15.0 20.0 30.0 50.0 60.0 70.0 80.0 90.0	20 0.57 34 35 35 36 36 36 36 36 37 36 37 36 36 36 37 36 36 36 36 36 36 36 36	0.56 36 37 53 51 59 39 39 30 25 20 0	0.42 -73 -75 -69 -69 -59 -59 -33 -28 -21 -33 -20 -30	8° 0.13 -1.14 -1.0396837570595413629220701	19 99 99 99 99 99 99 99 99 99 99 99 99 9	10 0 4 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		0.05	0.31 .09 05 07 10 05 05 01	8 1.50 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.61 .13 .25 .14 .09 .06 .05 .05	100 0.66 55 37 9 9 4 18 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.65 .64 .47 .42 .33 .25 .29 .15 .15
0.19 Ъ/2	0 1.5 1.0 10.0 10.0 10.0 10.0 10.0 10.0 10	643394 550 - 334 550 - 43338 585 - 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	49 68 72 70 64 51 46 39 31 26 20 07	-12 -1.22 -1.06 94 87 77 76 43 35 35 21 09 01	49 -1.84 -1.45 -1.16 99 55 37 37 30 01	-1.45 -2.61 -1.70 -1.48 -1.33 -1.11 74 61 41 31 20 08	47444 1 8653 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		.14 06 31 35 29 18 06 01	01 11 18 18 11 04 01	.59 .12 .07 .02 .07 .06 .01	.61 .56 .38 .23 .11 .02 .01	.50 .64 .38 .24 .11 .07	.26 .64 .51 .37 .21 .14 .09 .10
0.31 b/2	0 1.50 7.00 150.00 150.00 150.00 150.00 760.00 760.00 760.00 760.00 760.00	199 11350 11350 111111111111111111111111111	.49 503 661 457 459 332 381 001	-34 -92 -94 -89 -83 -79 -77 -57 -31 -31 -24 -09	.03 -1.42 -1.28 -1.17 -1.02 93 67 57 49 33 23 23	100838138174777777855435488	1.02 -2.69 -2.69 -2.57 -1.51 -1.30 -1.87 -35 -35 -35 -35 -35 -35 -35 -35 -35 -35		.09 22 25 24 21 19 16 11	.25 .04 07 11 11 10 06	.08 .08 .08 .09 04 04 04	.84 .14 .23 .13 .05 .05 .05	.71 .78 .36 .26 .21 .16 .12 .10 .07	.72 .70 .49 .37 .34 .25 .20 .16 .13
0.375 b/2	0 1.50 7.00 150.00 150.00 150.00 700.00 700.00 700.00 700.00 700.00	534994355 %3554866 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	- 6866466 - 6666 - 5771799	19 -1.20 -1.00 -97 -80 72 52 43 35 20 05	41 -1.89 -1.37 -1.25 -1.15 -1.00 89 60 50 40 31 21 05	-1.33 -2.76 -1.87 -1.61 -1.20 -1.05 53 32 32 05	4.65%5.00 4.45%5.00 4.4144 1.555%1.00 1.00		- 24 - 24 - 24 - 23 - 26 - 26 - 26 - 26 - 26 - 26 - 26 - 26	31.88	.52 .31 .08 .05 .01 .01 .04 .05	.58 .47 .23 .14 .09 .07 .07	.51 .57 .31 .26 .19 .16 .13 .11	.32 .60 .51 .42 .36 .28 .24 .15 .15
0.44 B/2	0 1.5 7.0 15.0 15.0 20.0 30.0 40.0 70.0 70.0 80.0 95.0	63 63 63 63 63 63 63 63 63 63 63 63 63 6	- 19 - 79 - 79 - 79 - 79 - 60 - 53 - 38 - 38 - 38 - 39 - 00 - 00	-1.43 -1.17 -1.09 83 51 51 52 327 19 03	-81 -2.17 -1.56 -1.39 -1.01 58 58 58 39 29 20 20 20 20	-2.06 -3.10 -2.09 -1.78 -1.72 -1.23 -1.80 63 51 40 29 17 01	7,538 44,17 44,17 14,17 14,18 16,54 11,18		13 09 24 30 36 29 19 11 05 .01	.46 .22 .02 09 16 17 13 06 01 .04			.32 .64 56 .43 .32 .16 .10 .10 .10 .10	

COM LUENTIAL

TABLE III.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; $T_c = 0$ - Continued (a) $\alpha_u = 2^0$, 4^0 , 6^0 , 8^0 , 10^0 , 12^0 - Concluded

	Per-				surface				<u> </u>			surface		
Spanwise stations	cent				fattack							of attack		
SCECIOIS .	chord 0	2º 0.46	0.48	0.31	-0.03	-0.61	12° -1.31	H	50				100	120
0.56 b/2	1.5 4.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	50 59 62 57 57 46 41 35 29 24 18 06	93 91 81 76 83 75 48 41 33 26 20	-1.48 -1.28 -1.19 -1.03 90 79 66 57 50 38 30 22 06	-2.14 -1.70 -1.47 -1.32 -1.13 76 54 53 41 32 06 .01	-2.81 -4.80 -1.80		200 and	0.24 0 10 11 11 09 07 01 .01	0.48 .83 .00 .00 .00 .00 .00 .00 .00 .00 .00	0.63 - 41 - 106 -	0.70 .56 .26 .22 .15 .14 .10	0.71 .68 .48 .37 .20 .21 .18 .10
0.68 b/2	1.5 4.0 15.0 15.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 2	្ត មន្ត្រីនិងមិនមិនមិនមិនមិនមិន មន្ត្រីនិងមិនមិនមិនមិនមិនមិនមិនមិនមិនមិនមិនមិនមិនម	36 55 57 57 57 59 45 27 21 21	99 99 88 56 49 49 34 34 34	-1.24 -1.24 -1.25 -2.85 -2.77 -36 -2.77 -36 -2.77 -36 -2.77 -36	-1.87 -1.53 -1.53 -1.35 -1.01 -82 52 38 27 01	14944444 1494444 14444 1444 1444 1444 1		17 1 50 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.23 .03 07 08 09 09 09	\$ 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	.95 .44 .19 .14 .10 .10 .10 .10	90.55 	3.8. 9.35.5.4. 9.35.7.48. 1.35.7.48.
0.80 ъ/2	0 1.5 4.0 7.0 15.0 20.0 30.0 40.0 50.0 70.0 80.0 90.0	\$8554485 \$8554485 \$8554485 \$8554 \$85545 \$85545 \$85545 \$85545 \$85545 \$85545 \$85545 \$85545 \$85545 \$85545 \$85545 \$85545 \$85545 \$85545 \$85545 \$85545 \$85545 \$85545 \$8554 \$85545 \$85545 \$85545 \$85545 \$8554 \$85555 \$85545 \$85545 \$8554 \$85545 \$85545 \$85545 \$85545 \$85545 \$85545 \$85545 \$85545 \$85545	-53 -36 -49 -55 -56 -35 -35 -35 -35 -35 -35 -35 -35 -35 -35	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	# 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	######################################			1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		\\ \\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	.56 .49 .45 .45 .45 .45 .45 .40 .41 .41 .40 .40 .40	.36 .28 .24 .18 .17 .13 .11	.47 .57 .39 .33 .25 .18 .17 .15 .13
0.94 b/2	0 1.50 7.00 15.00 20.00 30.00 50.00 70.00 80.00 90.00	0.38 .16 04 15 20 22 25 23 21 21 14 10 0	0.56 18 31 40 39 39 31 26 31 26	######################################	0 1 0 5 5 5 4 2 7 5 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	F% \$ 2.5 & F. 5 & F. 8 2 4 5 5 5 5 5 5 8 2 4 5 5 5 5 5 6 5 6 5 6 5 6 5 6 5 6 6 6 6	-1.81 -2.85 -1.85 -1.85 -1.86 -1.86 -1.86 -1.86 -1.86 -1.86 -1.86 -1.86 -1.86 -1.86 -1.86		- 34 - 30 - 30 - 24 - 19 - 04 - 09 - 04 - 06 - 06 - 06	5 5 7 5 5 5 5 5 5 5		55 88 1 88 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	.53 .39 .82 .18 .10 .09 .06 .06 .06	.48 .39 .32 .24 .18 .11 .08



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TABLE III.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; T_c = 0 - Continued (b) α_u = 14°, 16°

	Per-			Upper	urfece		Lower surface						
Sperwise stations	cent	.10	16°	Angle of	attack			- 20	Argle o	f attack			
o.10 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 \$0.0 50.0 70.0 80.0 90.0 95.0	4 N8888485885355415	16° 				14° 0.59 71	16 0.73 0.54 0.54 0.83 0.85 0.85 0.85 0.85 0.85 0.85 0.85 0.85					
0.19 b/ 2	0 1.5 4.0 7.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	9.4.75 9.4.75 9.4.75 9.4.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.	-5.51 -5.02 -3.19 -2.01 -1.55 74 56 42 06 05				-09 -60 -52 -52 -49 -30 -19 -12 -12 -04 -,02	.78 .79 .78 .70 .75 .75 .16 .15 .04 .					
0.31 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 40.0 50.0 60.0 70.0 80.0 90.0	######################################	-2.64 -4.13 -2.89 -2.01 -1.70 -1.44 -1.07 59 54 39 25 06				.68 .78 .79 .49 .41 .33 .27 .24 .18	**************************************					
0.375 b/2	0 1.5 4.0 70.0 15.0 20.0 30.0 40.0 50.0 70.0 80.0 95.0	5.25.45.88. 5.88.89.89.89.89.89.89.89.89.89.89.89.89.	5554 F. 8851 - 866 \$484 55				.01 .57 .58 .59 .36 .29 .19 .19	-42 -47 -63 -57 -57 -25 -25 -15					
Օ.եե Ե/2	0 1.50 7.0 10.0 15.0 20.0 30.0 \$0.0 50.0 60.0 70.0 80.0 90.0	**************************************	-7.60 -7.60 -7.60 -7.60 -7.40				67 .49 74 .67 .57 .38 .26 .20 .16 .15	-1.38 .30 .764 .574 .32 .22 .23 .29 .20 .29					

DISTRIPLE - STATE

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TABLE III.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; T_c = 0 - Concluded (b) α_u = 14°, 16° - Concluded

	Per-	1		Upper		T			Lower	surface	 		
Spanwise stations	cent				of attack				_		Angle o	of attack	
Stations	chord	140	16°				T	140	•	16°			
0.56 b/2	0 1.5 \$.0 7.0 10.0 20.0 30.0 \$0.0 50.0 60.0 70.0 80.0 90.0	4.18 4.55 4.55 4.55 1.55 1.55 1.55 1.55 1.55	3.19 4.38 3.04 4.51 1.73 1.74 1.87 1.87 1.54 1.87 1.96 1.96 1.96 1.96						657 650412864 184411	0.50 79 .56 .56 .54 .34 .31 .42 .54			
0.63 b/2	0 1.00000000000000000000000000000000000	######################################	7.55 7.55 7.55 7.55 7.58 7.15 1.15 1.15 1.15 1.15 1.15 1.15 1.15						- 2006 - 3756 1328 - 33917118	5.46 5.56 5.56 5.56 5.56 5.56 5.56 5.56			
O .80 b/2	0 1.5 4.0 7.0 15.0 20.0 30.0 40.0 50.0 70.0 80.0 95.0	# \\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	6.51.51.51.51.51.51.51.51.51.51.51.51.51.						96 - 3899 - 29649	29 .48 .56 .52 .44 .36 .24 .20 .15			
0.94 b/2	0 1.5 7.0 10.0 15.0 20.0 30.0 50.0 50.0 50.0 50.0	7.85 9.85 9.15 17.55 17.55 17.55 17.55 17.55 17.55	1088886538654485858585858585858585858585858585858						5 (2580364 - 25				



TABLE IV.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; T_c = 0.2 (a) α_u = 2°, 4° , 6° , 8° , 10° , 12°

- 1	Per-			Upper	surface						Lower a			
Spenvise	cent				f attack							f attack		
stations	chord	50	ţ0	60	80	10°	150	Н	50	- 4°	6°	8°	10°	120
0.10 b/2	0 1.5 7.0 10.0 15.0 15.0 15.0 15.0 15.0 15.0 15	**************************************	**************************************	୫୯୭୯୫୭୫୯୬୫୯୭୧ ୦ ୮ ୮ ୮ ୮ ୮ ୮ ୮ ୮ ୮ ୮ ୮	8258652453484888 677 (() () () () () (\$\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	\$		88 77 7 7 8 8 8 8 8	0.34 -1.4 -0.35 -0	৯৯ ঀৢয়ৢয়ৢঀয়ৢয়ৢড়ৢৼৢড়ৼৢ৾ৢঢ়ড়	63. 88. 88. 88. 88. 88. 88. 88. 88. 88. 8		0.63 .67 .53 .46 .39 .30 .20 .23 .20 .29
0.19 b/2	0 1.4 1.5 2.5 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0	%୫୫୫୫ଟ ଦୁଖ୍ୟ ଅନ୍ତ ଓ	\$ # \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	इंडेस्स्न्रेट्ट । क्ट्रिस्ट १९८५ नेनेनेने । तिनेति हो	82 -2.69 -1.91 -1.95 -1.15 61 76 39 39 32 21 06	-2.00 -3.69 -2.59 -1.73 -1.73 -1.39 -85 53 32 33 21 06	######################################		6.4 888 886		1.04 84 .49 .06 .04 .04 .04 .05 .05	1.03 1.00 .69 .43 .23 .07 .05 .08 .11	.94 1,10 .87 .60 .15 .11 .11 .16	1.18 1.18 1.03 .76 .51 .26 .18 .14 .40
0.31 b/2	0 1.5 4.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0	895848584658 895848584858	89888888888888888888888888888888888888	8.55 P38 86 T P68 57 4 39 34 56 66 66 66 66 66 66 66 66 66 66 66 66	.73 99 -1.14 -1.08 -1.04 99 65 55 36 36 36 36 36	51 -1.59 -1.45 -1.68 -1.68 -1.69 -1.	21757225625656565434105		50 61 53 50 36 36 24 19 10	-04 -26 -30 -30 -26 -20 -15 -13 -08	385 - 199 -	.62 .31 .09 .02 .04 .03 .03 .03 .04	.86 .53 .13 .16 .14 .19 .11	1.04 .74 .27 .26 .21 .19 .16 .15
0.375 b/2	0 1.57 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	500 28 28 28 28 28 28 28 28 28 28 28 28 28	5315560 8855 4 THE 694 65	20 -1.11 91 88 78 78 37 37 37 32 36	-43 -1.83 -1.82 -1.21 -1.00 -1.52 -1.52 -1.54 -1.08 -1.08	-1.43 -2.74 -1.63 -1.42 -1.07 -74 -79 -49 -37 -26 -10	-2.57 -2.57 -1.57 -1.57 -1.57 -2.56 -2.53		09 24 24 21 20 15 05 05 06	.29 .09 04 05 05 05 05 05 05	.53 .35 .19 .19 .09 .05 .04 .06 .07	.59 .52 .36 .27 .22 .15 .11 .11	.50 .60 .98 .33 .325 .20 .20 .16 .15	.27 .61
o.¥4 ъ/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 70.0 80.0 90.0 95.0	1.00 63 64 65 65 40 33 27 27 22 16 03	.63 -1.33 -1.07 83 79 83 79 39 39 30 00	194444884XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX	121213656858411365685841136566584113656858411365665841136566584113656658411365666584113656666666666666666666666666666666666	9795887887887854265			.63 .26 .26 .19 .30 .30 .30 .30 .05 .06	.93 .60 .89 .08 80 15 09 02 .04 .10	1.04 .86 .54 .30 .12 .02 0 .04 .07 .11	.75 .75 .75 .32 .32 .09 .09 .11	.73 1.13 .95 .89 .23 .15 .15 .10 .09	1.13 .86 .65 .36 .24 .19 .18 .20



TABLE IV.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; T_c = 0.2 - Continued (a) α_u = 2°, μ °, 6°, 8°, 10°, 12° - Concluded

	Per-	1		Upper	surface			т	1		Lower	surface		
Spanwise stations	cent				of attack			1			Angle			··
SCRUTTORS	chord	20	¥0	. 6°	80	20°	120	1	20	30	60	80	100	120
0.56 b/e	0 1.5 4.0 7.0 10.0 20.0 30.0 40.0 50.0 80.0 90.0	0.49217295865554882247536 0.1111111111158	0.77 10 43 57 57 57 48 43 36 26 20 05	0.86 52 79 79 554 554 554 554 554 554 554 554 554 554 554 554 554 554 554 554 554 556 554 55	0.750.221.04 -1.04 -1.04 -	0.49 -1.59 -1.498 -1.21 -1.00 84 59 47 37 37 06	0.15 -2.26 -1.98 -1.80 -1.64 -1.41 -1.99 66 54 43 31 30		-0.66 75 50 48 26 21 01 01 03	-0.15 -37 -37 -35 -35 -35 -25 -17 -13 -01 .03 .05 .10	0.29 05 18 17 17 15 07 07	0.62 .23 .02 .05 .05 .05 .08 0	0.78 .46 .11 .09 .07 .06 .06	1.07 .67 .36 .24 .19 .13 .13 .13
о.68 ъ/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 90.0 95.0	**************************************	.56 6.58 6.58 6.59 6.59 6.59 6.39 6.21 6.21 6.07	######################################	15.325548655485566 14441111111	1.88 1.89 1.59 1.36 1.19 1.64 1.53 1.19 1.64 1.53 1.64 1.53 1.64 1.64	\$		ଅନ୍ତ କଥିଲା ପ୍ରତ୍ତ କଥ	18 d 1 7 7 9 6 5 8 1 1 4 5 5 8 8 1 1	.47 .26 .05 .04 .09 .05 .08 .08 .08	.57 .45 .27 .20 .16 .12 .12 .12 .12	.49.54 .40.51.51.51.51.51.51.51.51.51.51.51.51.51.	- 100 55 - 51 - 200 - 51 - 200 - 200
0.80 b/2	0 1.50 7.00 15.00 20.00	#158888885495568	584744488888888888888888888888888888888	38824884488255 11111111111	इक्ष्ण्य विक्र स्थापन स्थापन विक्र स्थापन विक्र स्थापन स्थापन स्थापन स्थापन स्थापन स्थापन स्थापन स्थापन स्थापन	\$\$5\$888588885555 1911111111	\$\$\$\$\$\$##\$\$\$\$\$\$\$\$\$\$\$		- 28 - 33 - 28 - 17 - 17 - 17 - 17 - 05 - 01 - 06 - 09	୍ । ଚ୍ଛଟ୍ଟେମ	1400 11585 8889999	.58 .44 .26 .20 .16 .13 .10 .11 .11 .10	.52 .53 .38 .29 .26 .20 .16 .25 .15 .11	33 -57 -49 -40 -34 -87 -15 -13 -10 -08
0.94 в/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 50.0 70.0 70.0 90.0 95.0	.35 .19 01 16 20 24 21 20 20 20 21 08	55525555555555555555555555555555555555	#888###888## 8 6 111111111 8	8 H88*55598886888	- 4-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-	-1.96 -2.28 -1.57 -1.51 -1.57 -1.57 -1.57 -1.57 -1.50 -1.32		- 47 - 27 - 29 - 19 - 14 04 04 04 05 04	- 1 9 - 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.34 .12 .06 .06 .01 .03 .03 .08	-51 -88 -19 -14 -10 -06 -07 -06 -07 -08 -08	- 53 - 49 - 23 - 19 - 11 - 12 - 19 - 11 - 12 - 13 - 14 - 15 - 15 - 15 - 15 - 15 - 15 - 15 - 15	. 42 . 47 . 40 . 32 . 24 . 19 . 14 . 11 . 09 . 07

TABLE IV.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 14 ,000,000; T_c = 0.2 - Continued (b) α_u = 14° , 16°

	7			Uoper	surface	 			Lower	surface	
Spanvise stations	Per- cent				f attack					of attack	
BOALLOUS	chord	140	16°				140	16°			
0.10 b/2	0 1.5 7.0 7.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 95.0	1.87 -3.04 -2.15 -1.29 -1.29 -1.46 -1.29 -1.46 -	2.72 2.77 2.77 2.77 2.70 1.70 1.70 1.70 1.70 1.70 1.70 1.70 1				0.54 -73 -63 -54 -38 -39 -29 -29 -24 -12	0.40 .74 .68 .58 .53 .34 .38 .39 .29			
0.19 b/2	0 H.4 F.9.00000000000000000000000000000000000	3588855 88855 888558	687555% 8869%588				1.18 1.18 .86 .94 .95 .91	- 38 - 86 - 71 - 12 - 32 - 24 - 25 - 11			
0.31 b/2	0 1.5 7.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15	14548564395594368	7548555668686533591 1344444111111111111111111111111111111				1.80 .92 .54 .36 .31 .26 .25	1.20 85.433.32 8 45			
0.375 b/2	0 1.5 4.0 10.0 10.0 10.0 30.0 50.0 70.0 70.0 70.0 70.0 70.0 70.0	1586#16641 9156#3000	45.63 45.63 45.63 45.65 45.65 45.65 45.65 46 46.65 46 46 46 46 46 46 46 46 46 46 46 46 46				09 55 56 50 36 27 25 18	- 66 .68 .550 .14 .30 .16 .16			
0.44 5/2	0 1.5 7.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15	%%%#&#&#\$</td><td>ታሉተ ጥጥ ተተ ነ ነ ነ ነ ነ ነ ነ ነ ነ ነ ነ ነ ነ ነ ነ ነ</td><td></td><td></td><td></td><td>-57 -57 -72 -1.16 -64 -76 -44 -33 -25 -24 -24 -11</td><td></td><td></td><td></td><td></td></tr></tbody></table>									

COMPANDAL --

TABLE IV.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; T_c = 0.2 - Concluded (b) α_u = 140, 160 - Concluded

ŗ	Per-			Upper	surface	 	\top		Lower	surface	
Spanwise stations	cent			Angle o	of attack				Angle	of attack	
20201078	chord	140	160				140	16°			
0.56 b/2	0 1.50 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	भ्राम्यत्वस्य स्थाप्ति । ११११मन् ने ने ने ने ने ने ने ने	525568858585858 17999777771111				1.21 .85 .50 .38 .24 .23 .20 .20 .22 .19	ଜୁନ୍ମ ଜୁଲ୍ଲ ମଧ୍ୟ କଥା । ଜୁଲ୍ଲ			
0.68 b/2	0 1.5 4.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 95.0	ଗ୍ରେଟ୍ଟେଟ୍ଟେଟ୍ଟେଟ୍ଟେଟ୍ଟ ↑↑ዮ଼୩୩નને (बंध्रह्मक्षत्रक्षक्षक्षक्षक्षक्ष्म प्राप्तिक्षित्ति ।				195 55559 1880409	555845 88899			
0.80 ъ/2	0 1.5 1.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 95.0	\$185558884553788 1199777111111	957949259543355438754814					194 85349 888499			
0.94 ъ/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 60.0 70.0 90.0 95.0	%\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	5.79.88 24.80 5.43 34.22.7 5.44 6.60 6.60 6.60 6.60 6.60 6.60 6.60 6			·	.47 .47 .48 .24 .19 .10 .05	13 -57 .57 .53 .47 .38 .29 .23 .19 04			

COMPLDENTIAL



TABLE V.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; T_c = 0.4 (a) α_u = 2°, 4°, 6°, 8°, 10°, 12°

	Per-			Upper s				T			Lower s			
Spanwise stations	cent	- 0 1	10 1	Angle of	80	100	120	ŀ	20	¥0	60	80	10°	12°
0.10 ъ/2	0 1.5 4.0 7.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	20 0.56 0 186 0 186 0 1.34 1 3.34 1 3.34 1 3.35 1 2.34 1 2.35 1 3.35 1 3	0.56 34 49 47 47 45 38 28 28 28	0-40 72 73 68 64 59 53 46 40 33 27 20 05	0.03 -1.21 -1.03 97 85 72 62 53 36 30 23 07	-0.50 -1.81 -1.81 -1.82 -1.07 86 71 60 50 33 33 08	-1.16 -2.39 -1.77 -1.50 -1.12 99 -81 94 95 35 35 10		09 07 09 09 09 07 05 05 05	0.36 .17 .04 .04 .01 .01 .01 .02 .05	0.54 .36 .36 .18 .15 .10 .09 .07 .09	0.64 .51 .36 .30 .25 .20 .17 .14 .13 .13 .06	0.66 .61 .47 .40 .34 .28 .24 .20 .18 .18	0.61 .70 .57 .49 .42 .35 .30 .25 .23 .20
0.19 5/2	0 1.5 2.0 7.0 15.0 20.0 30.0 40.0 50.0 70.0 80.0 95.0	1.17 98 90 817 68 146 427 29 13	-67 -1.66 -1.66 -1.71 -1.88 -1.77 -1.88 -1.77 -1.88 -1.88 -1.86 -1.88 -1	46 48 48 43	- 98 -7.32 -2.85 -1.59 -	2.49%	କ୍ରକ୍ଷ୍ଟ । ଓ ନ୍ୟୁ ନ୍ୟୁ ଓ ଗ କ୍ରକ୍ଷ୍ୟ ନ୍ୟୁ ନ୍ୟୁ ନ୍ୟୁ ଓ ଗ		1.14 .73 .24 06 24 13 01 .11	1.36 1.01 19 15 15 57 43	1.46 1.23 .74 .38 .15 02 .03 .08 .15	1.44 1.39 .95 .59 .31 .11 .10 .18	1.15	1.22 1.62 1.62 1.34 .94 .60 .30 .25
0.31 ъ/2	0 1.5 4.0 7.0 10.0 15.0 20.0 40.0 50.0 60.0 70.0 95.0	-69 -41 -09 -28 -35 -40 -41 -35 -36 -32 -25 -25	1.00 .12 36 50 57 60 57 47 41 35 30 22	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	1.13 73 -1.04 -1.04 -1.09 97 57 41 29 05	1.03 -1.26 -1.49 -1.39 -1.23 -1.21 -1.88 66 66 32 32 32	85 1.84 1.87 1.4.30 1.75 1.4.30 1.75 1.4.30 1.75 1.4.30 1.75 1.4.30 1.75 1.4.30 1.75 1.4.30 1.75 1.4.30 1.75 1.4.30 1.75 1.75 1.75 1.75 1.75 1.75 1.75 1.75		90 96 71 72 40 29 22 11	36 57 53 54 29 29 15 07	 .12 21 22 32 21 17 11 06 08	.53 .13 07 12 06 03 0 .02 	.84 .40 .11 .01 .07 .07 .09 .10	1.13 .65 .16 .18 .16 .15 .16
0 . 375 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 70.0 80.0 90.0	.48 .08 12 27 34 35 35 25 20 15 02	-54 -39 -44 -50 -51 -52 -51 -36 -31 -25 -18 -04	.27 98 82 83	32 -1.67 -1.23 -1.15 -1.07 96 87 63 32 43 24 24 24	-1.19 -2.53 -1.75 -1.57 -1.38 -1.21 -1.06 50 39 26 39 26	-2.34 -3.34 -2.23 -1.91 -1.49 -1.49 -1.27 87 67 55 42 30 10		15 26 24 24 20 18 12 05 .01	.28 .10 .01 .02 -03 -03 -05 -03 -01 .01	.53 .36 .22 .15	.60 .54 .29 .28 .20 .217 .14 .15	.52 .62 .51 .39 .36 .25 .25 .25 .19 .19	.32 .61 .59 .51 .48 .39 .34 .26 .25
0.44 6/2	0 1.5 4.0 7.0 15.0 20.0 30.0 40.0 50.0 70.0 80.0 90.0	1.28 96 84 90 76 58 40 33 32 22 212	0.75 -1.80 -1.33 -1.28 -1.09 78 61 47 39 31 20 05	15 -2.76 -1.90 -1.73 -1.14 -1.20	-1.40 -3.82 -2.53 -2.20 -1.45 -1.20 89 56 52 40 30 30	7,14 7,14 7,14 1,07 1,07 1,4 1,07 1,4 1,07 1,4 1,07 1,07 1,07 1,07 1,07 1,07 1,07 1,07	-5.00 -6.51 -4.11 -3.32 -2.67 -2.04 -1.17 86 -1.17 51 36 21 01		1.09 .63 07 27 29 16 06 .03 .12	1.37 .97 93 .21 01 06 .01 .06 .05 .09	1.45 1.25 .80 .46 .21 .01 .05	1.38 1.43 -1.03 .70 .42 .18 .27 .15 .18	1.17 1.56 1.25 .88 .80 .20 .21 .25	.93 1.66 1.45 1.07 .76 .41 .32 .29 .27 .30

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TABLE V.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; $T_c = 0.4$ - Continued (a) $\alpha_u = 2^\circ$, 4° , 6° , 8° , 10° , 12° - Concluded

Spanwise	Per-			Upper	surface			т-			ī.cr-	r surface		
stations	Cent			Angle	of attacl			1				of attac		
	chord	20	40	6º	80	100	120	1	20	i o	60			
0.56 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 50.0 60.0 90.0 95.0	0.47 04 24 34 39 36 35 30 25 19 01	0.90 .16 31 50 56 50 45 38 38 32 26 21	1.14 24 64 67 81 76	1,20 71 99 -1.04 96 89 73 54 44 36 36 37 36 37	1.10 -1.30 -1.47 -1.46 -1.25 -1.05 89 79 64 51 32 06	0.88 -1.90 -1.89 -1.69 -1.47 -1.04 91 72 57 46 34 07		-1.18 -1.16 78 66 50 34 25 01 01	-0.56 76 57 48 38 29 19 01 .03 .06 .15	0.01 35 42 10	80 0.48 01 20 19 14 07 03 .12 .13	0.83 .26 02 05 05 .01 .03 05 .16 .15 .21	12° 1.13 -5318 .04 .09 .1003 .21 .20
0.68 b/2	0 1.5 4.0 7.0 10.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	33999000000000000000000000000000000000	.55 43 43 50 44 33 30 12 0 00	. 140 80 87 81 	16 -1.52 -1.34 -1.19 -1.0291816653432413 .08	-1.15 -2.45 -1.87 -1.56 -1.19 -1.03 64 51 38 26	-2.54 -3.50 -2.45 -1.70 -1.44 -1.22 55 55 27 11 .10		36 40 33 28 20 16 10	-15 02 10 09 06 03 04 .07 .09	.45	.57 .45 .27 .20 .18 .14 .14 .14 .14 .13	.50 .55 .40 .31 .29 .21 .19 .18 .15 .15	.26 .58 .51 .51 .43 .39 .31 .27 .20 .19
ი.მი ъ/2	0 1.5 1.0 7.0 10.0 20.0 30.0 40.0 50.0 60.0 80.0 90.0	5.48 	- 56 - 28 - 39 - 44 - 45 - 45 - 37 - 31 - 26 - 22 - 18 - 19	78 78 77 71 71	44 -1.57 -1.26 -1.23 98 84 71 57 50 30 22 13 .05	-1.60 -2.47 -1.75 -1.49 -1.31 -1.09 71 59 36 25 13 03	-3.04 -3.50 -2.29 -1.87 -1.62 -1.32 -1.11 83 65 50 36 23 10		31 35 33 83 18 14 04 0 04 .07	.17 0 07 06 04 01 .05 .06 .09 .10	.47 .26 .08 .06 .05 .07 .08 .10	.59 .45 .27 .23 .17 .13 .12 .12 .12 .11	.52 .54 .39 .31 .26 .21 .15 .15 .15	-33 .58 .49 .42 .35 .29 .20 .20 .16 .15
0.94 b/2	0 1.5 4.0 7.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	.33 .21 .01 16 19 21 23 20 20 20 11 08	.56 13 28 35 35 35 32 27 25 25 29 09	-61 -63 -63 -56 -54 -138 -110 -7	01 -1.19 -1.04 95 80 67 55 43 39 33 28 19 10	872.08 -1.45 -1.24 -1.068671554537302011	-2.02 -2.29 -1.90 -1.58 -1.31 -1.06 65 51 40 31 19 09		52 39 39 24 19 18 08 03 03	0 08 12 10 09 09 09 09 0 0 0 0 0	.34 .12 .06 .01 .01 .01 .04 .04 .06 .08	.52 -29 .20 .15 .10 .07 .07 .08	.53 .41 .31 .24 .20 .13 .11 .10 .09 .08	.41 -41 .41 .35 .26 .19 .15 .14

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TABLE V.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; T_c = 0.4 - Continued (b) α_u = 14°, 16°

 -	Per-			Upper	surface	 			Lower	surface	
Spanwise stations	cent				f attack					fattack	
o.10 b/2	0 1.5 1.0 10.0 10.0 10.0 10.0 10.0 10.0	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	8 884 4 54 8 8 8 8 5 8 8 5 9 9 9 9 9 9 9 9 9 9 9 9				14°	19 1 10 5 1 10 5 1 10 5 10 10 10 10 10 10 10 10 10 10 10 10 10			
0.19 1/2	0 1.500000000000000000000000000000000000	०५म ग्रेस् । न् । । । । । । । । । । । । । । । । ।	######################################				1.09 1.69 1.08 1.08 1.08 2.74 .41 .32 .30	1.54 1.53 1.10 .83 .49 .39 .30			
0.31 b/2	0 1.5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	\$43388884556845533864 \$44444411111	\$\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\				1.368 .55893544 .45	1.51 1.06 1.77 1.40 3.34 3.31 3.30 2.80 1.27			
0.375	0 1.5 7.0 15.0 15.0 30.0 50.0 70.0 70.0 70.0 70.0 70.0 70.0 7	######################################	5.34 5.34 5.34 5.38 6.38 6.38 6.53 6.53 6.53 6.53 6.53 6.53 6.53 6.53				02 56 57 58 43 43 34 39	-51 -51 -70 -68 -65 -549 -38 -35 -25 -22			
0.44 b/2	0 1500000000000000000000000000000000000	######################################	፟ ፟ ፟ ፟ ፟ ፟ ፟ ፟ ፟ ፟ ፟ ፟ ፟ ፟ ፟				.05 1.64 1.57 1.114 .92 .53 .39 .35 .35 .35 .34	-1.49 FT - 1.59 S.55 FT - 39 S.55 FT - 30 S.			

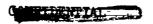


TABLE V.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; T_c = 0.4 - Concluded (b) α_u = 140, 160 - Concluded

	Per-			Upper	surface	 	Т			Lover	surface	
Spanvise stations	cent chord			Angle o	of attack	 				Angle	of attack	-
0.56 b/2	0 1.5 1.0 7.0 10.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	14° 0.55 -0.58 -0.36 -0.19 -1.98 -1.17 -1.17 -1.01816351363636	16° 0.11 -7.387 -2.59 -2.59 -1.95 -1.14 -1.14 -1.15 -1.16 -1					1.37 .77 .35 .22 .20 .14 .16 .17	1.53 .93 .28 .21 .25 .23 .30 .30			
o.68 ъ/2	0 1.5 4.0 15.0 15.0 20.0 20.0 20.0 70.0 80.0 70.0 80.0	4434868884448888448888448888448888844888884848	4.50 75.70 7					-14 -54 -58 -58 -58 -58 -38 -34 -27 -24 -21 -21 -10	74 .40 .56 .51 .44 .38 .29 .24 .16			
0.80 ъ/2	0 1.5 4.0 7.0 10.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	1-87 1-87 1-87 1-87 1-87 1-71 1-73 1-13 1-13 1-13 1-13 1-13 1-1	6.98 -5.35 -2.29 -1.05 -					02 .54 .50 .50 .42 .34 .25 .21 .20 .14	-50 -57 -57 -57 -57 -58 -39 -38 -34 -34 -34 -35 -38 -34 -34 -35 -36 -36 -36 -36 -36 -36 -36 -36 -36 -36			
0.94 b/2	0 1.5 4.0 7.0 10.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	-3.51 -3.01 -2.41 -1.57 -1.25 -1.02 74 57 41 31 17 10 05 04	-9.28 -3.86 -2.32 -1.82 -1.82 -1.85616143252016					.19 .48 .41 .34 .25 .19 .15 .10 .07	17 55 .52 .45 .39 .29 .21 .18 09 .05			

TABLE VI.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4 ,000,000; T_c = 0.6 (a) $\alpha_{\rm ll}$ = 2°, 4 °, 6°, 8°, 10°, 12°

_	Per-			Upper	surface					Lover	surface		
Spanwise stations	cent	Ļ		Angle o	fattack						f attack		
Stations	chord 0 1.5	2° 0.57 .01	0.56 32	6° 0.40 –.71	0.02 -1.20	-0.51 -1.80	12 ⁰ -1.24 -2.44	0.10	0.36	6° 0.55	 0.64	10° 0.66	12°
0•10 p/2	7.0 7.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15	151288830 111110 1110 110 110	111111111111111111111111111111111111111	11111111111111111111111111111111111111	1.03 - 84 - 76 - 76 - 76 - 76 - 76 - 76 - 76 - 76	-1.42 -1.05 94 60 50 432 08	######################################	65 166 166 166 168 168 168 168 168 168 168	# 85.685.685.68 # 88.685.685 88.685.685 88.685	.38 .24 .20 .18 .13 .12 .10 .10 .10	.53 -39 .32 .30 .25 .25 .29 .16 .17 -11	.63 .50 .439 .388 .384 .200 .200 .118	.71 .60 .51 .48 .39 .35 .32 .27
0.19 b/2	0 1.5 7.0 7.0 15.0 20.0 50.0 70.0 80.0 95.0	1.30 -1.38 -1.98 87 76 50 33 17 02 09	73 -2.16 -1.60 -1.33 -1.17 58 36 33 14 05	ଟ୍ରମ୍ୟୁକ୍ଷ ଅନ୍ୟୁନ୍ଷ୍ୟ ଅନ୍ଧ୍ର	1990 1990 1990 1991 1990 1990 1990 1990	4577447 (((() () () () () () () ()	%&************************************	1.81 1.86 1.86 1.86 1.86 1.86 1.86 1.86	1.78 1.38 1.38 71 .03 13 01 .08 .20	1.91 1.63 .98 .50 .23 .01 .05	1.90 1.81 1.23 .73 .40 .14 .17 .20 .29	1.82 1.97 1.44 .93 .56 .25 .25 .25 .24 .35	1.66 2.07 1.64 1.13 .37 .37 .33 .42 .22 .17
0.31 b/2	0 1.5 0 79.0 15.0 0 15.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	65746333333333333444 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1.14 2331.5285667012921 	#86688688548854	1.44 - 48 - 400 - 1.00 - 1.00 - 77 - 77 - 38 - 20 - 19	1.00 3 3 3 3 2 1 3 6 8 8 5 5 1 8 8 8 5 5 1 8 8 8 8 5 5 1 8 8 8 8	356825548355285358 1111111111111111111111111111111111	1.29 1.33 1.08 1.08 1.08 1.09 1.09 1.09 1.09 1.09 1.09 1.09 1.09	291 791 737 7382 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	159 1993541 199 190 190	- 34 - 10 - 26 - 30 - 16 - 08 - 08 - 03 - 03 - 17 - 25	.73 .22 06 13 0 .05 .09 .11 16	1.10 .53 .02 .14 .16 .17 .19 .22 .28
0.375 b/2	0 1.5 4.0 7.0 15.0 20.0 30.0 40.0 70.0 80.0 90.0 95.0	- 43 - 16 - 04 - 18 - 23 - 33 - 26 - 101 - 07	56 236 7 47 1 47 1 7 48 1 7 1 7 1 7 1 7 1 7 1 7 1 7 1 7 1 7 1 7	- 37 - 84 - 75 - 73 - 73 - 73 - 73 - 73 - 73 - 73 - 73	-15 -1.72 -1.15 -1.10 -1.94 86 54 55 35 35 35 35	-91 -92 -1.63 -1.48 -1.06 -1.06 -1.32 -1.3	\$444 4744 4744 11111	-22 -30 -25 -21 -19 -13 -05 0	24 .08 .0 .04 .03 .02 .05 .11 .14	.52 .37 .16 .14 .10 .10 .10	.64 .56 .43 .32 .30 .21 .20	.60 .66 .54 .44 .31 .30 .24 .24	. 46 . 68 . 67 . 59 . 45 . 45 . 31 . 31 . 31 . 28
0.44 b/2	0 1.5 7.0 15.0 20.0 30.0 40.0 60.0 70.0 80.0 95.0	1.48 -1.35 -1.04 -88 -631 -37 -37 -21 -30 -30 -30	.81 -9.27 -1.53 -1.53 -1.03 -1.49 -1.49 -1.14 -1.29 -1.14 -1.09	1334 13 06 13 26 06 15 15 16 16 16 16 16 16 16 16 16 16 16 16 16	1.59 1.55 1.55 1.55 1.55 1.35 1.35 1.35 1.35	-3.36 -5.93 -3.77 -3.50 -3.50 -1.50 -3.60	5.48655855555555555555555555555555555555	1.5* .98 .95 .21 .27 .15 .03 .05 .16	1.80 1.35 74 .33 .05 10 05 11 .21 12 08	1.90 1.65 -62 .30 .03 .09 .14 .18 .26	1.82 1.86 1.86 1.3* .87 .23 .17 .20 .24 .30	1.62 2.01 1.58 1.08 1.08 27 27 29 34 	1.34 2.11 1.78 1.29 .33 .35 .35 .39





TABLE VI.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; T_c = 0.6 - Continued (a) α_u = 2°, 4°, 6°, 8°, 10°, 12° - Concluded

_	Per-			Upper	surface		_	_	Γ		Lower	surface		
Spanwise stations	cent				of attack			ŀ				of attack		
SCATTLONIS.	chord	20	¥°	6°	8°	10°	120	1.	20	ho.	60	80	100	120
0.56 b/2	0 1.50 7.0 10.0 20.0 30.0 40.0 50.0 60.0 70.0 90.0	0.43 .03 .233 .233 .233 .233 .233 .233 .233	0.97 -38 -24 -58 -59 -59 -59 -59 -34 -24 -03	1.32 -574 -8479 -649 -590 -34 -255 -14	1 - 49 1 - 48 1 - 19 1 - 19	1.52 -1.36 -1.42 -1.43 -1.28 -1.95 68 56 35 35	14.888.53388.5488853888538885388853888538		1.66 1.56 1.56 1.20 1.02 1.64 1.30 1.04 1.04	-1.00 -1.1* -92 -82 -66 -51 -30 -22 -03 .07	-0.35 -70 -68 -59 -19 -39 -22 -16 -03 .09 .11	0.23 31 44 40 37 16 09 02	0.68 .01 24 23 20 16 05 01 03 .18 .18	1.08 .33 01 06 06 05 .05 .05 .04 .24 .23
0.68 b/2	0 1400 1400 1400 1400 1400 1400 1400 14	200668888888459995	.56 19144 46 45 32 32 17 22 17 07	**************************************	122210888514205	388845888884198 191711111	-2.53 -3.47 -2.43 -1.67 -1.41 -1.67 -1.41 -7.55 71 75 39 11 04		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-10 06 12 12 09 03 03 04 06	.44 .24 - 10 .05 .05 .05 .06 - 10 .11 .13	.58 .45 .28 .20 .17 .13 .13 .13 .13	.51 .57 .40 .32 .29 .24 .19 .17 .16	.27 .60 .51 .39 .31 .29 .24 .22 .20 .15
о.80 ъ/2	50000000000000000000000000000000000000	្នុះកូតុសូសូសូសូងក្នុង ខ	-57 -27 -38 -445 -45 -45 -36 -25 -217 -111 0	268478777883378837883788378837883788378837	48 1457.465.984.258.99.44.33 1111.41.11.11.11.11.11.11.11.11.11.11.11	선수 73 73 88 이 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	7.51.29 7.51.29 7.74.56 7.74.74 7.74.7		- 35 - 36 - 23 - 18 - 12 - 03 - 01 - 05 - 07 - 12	15 15 16 16 16 16 16 16 16 16 16 16 16 16 16	46 .26 .26 .09 .09 .06 .09 09 .10 .10	.59 .45 .28 .28 .19 .15 .13 .14 .14 .13	.53 .54 .40 .31 .27 .21 .17 .16 .15 .14	.32 .58 .51 .45 .36 .29 .21 .20 .18 .11
0.9 4 b/2	0147999999999999999999999999999999999999	***************************************	-56 -13 -28 -33 -33 -33 -33 -22 -20 -13 -04	. 635 . 635	-01 -1.19 -1.03 94 65 53 41 31 26 17 03	- 898 - 4.45 - 4.45 - 686 - 1.54 - 1.54 - 1.54 - 1.54 - 1.68 - 1.54 - 1.68 - 1.	-2.06 -2.29 -1.57 -1.50			06 10 07 07 05 01 .08	.34 .06 .03 .01 .04 .04 .06 .08 .09	.52 .31 .24 .15 .12 .09 .09 .09 .09		.41 55 .47 .35 .28 .20 .15 .14 10 .06



TABLE VI.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; T_c = 0.6 - Continued (b) α_u = 14°, 16°

Spanvise	Per-				surface	 				surface	
stations	cent			Angle	of attack	 	 	1	Angle o	f attack	
0.10 b/2	0 1.5 1.0 10.0 15.0 20.0 30.0 50.0 60.0 70.0 80.0	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	16° 3.86 - 1.754 200 80 80 80 80 80 80 80 80 80 80 80 80 8				14°	0.25 0.27 0.27 0.27 0.39 0.39 0.39 0.39 0.39 0.39			
0.19 8/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	5.56 -7.56 -7.59 -7.59 -1.66 -7.59 -1.66 -7.59 -1.66 -7.59 -1.66 -7.59 -1.66 -7.59 -1.66 -7.59 -1.66 -7.59 -1.66 -7.59 -1.66 -7.59 -1.66 -7.59 -1.66 -7.59 -1.66 -7.66 -	7-8-51 				1.46 2.14 1.79 1.26 .87 .47 .40 .44 .28	2.09 2.09 1.87 1.34 .58 .58 .50 1.43			
0.31 5/2	0 1.5 1.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 90.0	1.16 -2.17 -2.26 -2.09 -1.87 -1.53 -1.54 -2.53 -1.05 -2.53 -0.23	89844444444444444444444444444444444444				1.40 .79 .31 .16 .25 .26 .28 .29	1.64 1.01 .46 .28 .34 .30 .31 .32 .31			
0.375 b/2	0 11000 11000 1150	311280021 - 4.51	-5.15 -5.13 -2.70 -2.58 -1.72 -1.55 74 55 13 15 55				.17 .66 .76 .70 .69 .71 .87 .37	-29 .53 -80 .77 .74 .63 .55 -25 .41 			
0.44 5/2	0 1.00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	4954593882598456	19.63 19.45 19.75				2.13 1.85 1.86 1.08 .61 .50 .41 .39	1.61 1.61 1.79 1.29 1.13 .70 .86 .44 .44 .44			

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TABLE VI.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; T_c = 0.6 - Concluded (b) α_u = 14°, 16° - Concluded

····	Per-			Umper	surface		— т			Lover	surface	
Spanvise	cent				f attack					Angle o	fattack	
stations	opord	140	16°					140	16°			
0.56 b/2	0 1.5 4.0 15.0 15.0 20.0 40.0 70.0 70.0 80.0 95.0	ୡୣଌୄଊୣଌୄଌୄଌୄଋୣଌଌୄୣ ୳ୣୣୣୣୣୣ୴ଡ଼ୣଡ଼ଡ଼ୣ୷୷୷୷୷୷୷୷୷୷୷୷୷୷୷୷୷୷୷୷୷୷୷୷୷୷୷	0.88 49.60 40 40 40 40 40 40 40 40 40 40 40 40 40					1.12 .60 .05 .05 .04 .11 .12 	1.63 .81 .17 .17 .11 .29 .39 .39			
o.68 b/2	0 1.5 4.0 10.0 15.0 20.0 30.0 40.0 70.0 80.0 95.0	%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%	455E5435&8888##### 457444############################			1		14 -54 -59 -59 -36 -36 -38 -26 -22 -22 -16	- 60 - 57 - 45 - 57 - 45 - 33 - 29 - 29 - 12			
0.80 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	4.99 4.99 4.99 4.95 1.30 1.36 1.36 1.36 1.10	7.14 -5.41 -3.54 -2.74 -2.80 -1.46 -1.07 -1.46 -1.07 -1.30 -1.30 -1.20 -1.19					04 54 57 51 44 37 25 26 16 11	-57 -58 -56 -50 -50 -29 -26 -21 -16 -10			
0.94 7/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	3.58 -3.65 -2.42 -1.54 -	-5.36 -3.88 -2.92 -2.26 -1.40 -1.14 -1.06 -1.14 -1.06 -1.14					.17 				



TABLE VII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; T_c = 0.8 (a) α_u = 2°, 4°, 6°, 8°, 10°, 12°

	Per-			Upper	surface.			Т	_		Lower	surface	·	
Spanwise stations	cent				of attack]			Angle	of attack		
	chord	0.57	0.57	6°	0.02	10° -0.58	12°	1	20	#o	6º	80	10 ^C	120
0.10 b/2	1.5 4.0 7.0 10.0 15.0 20.0 30.0 50.0 60.0 70.0 80.0 95.0	.04	29 37 43 43 43 40 35 27 21 15 02	- 69 - 70 - 66 - 55 - 55 - 55 - 35 - 35 - 35 - 35 - 35	-1.20 -1.02 84 75 70 61 36 29 21 06	-0.58 -1.63 -1.41 -1.22 -1.06 95 73 61 49 41 33 23 10	-2.47 -1.80 -1.510 -1.30 -1.83 -1.30		0.10 04 04 04	0.37 .20 .11 .09 .09 .07 .07 .07	0.555 .40 .22 .22 .18 .16 .15 .15 .15	0.555 14.35338448191155	0.65 65 25 25 25 26 26 26 26 27 27 27 27 27 27 27 27 27 27 27 27 27	0.58 .71 .53 .49 .41 .36 .33 .29 .27
o.19 b/2	0 1.5 4.0 7.0 10.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	1.38 -1.80 -1.37 -1.13 98 82 	.70 -2.62 -1.86 -1.72 -1.27 -1.27 -1.27 -37 -30 -23 -15 -01	17 -3.59 -2.43 -1.62 -1.30 74 54 33 25 04	-1.26 -1.63 -3.05 -2.38 -1.97 -1.76 64 36 29 20 05	-2.65 -5.87 -3.93 -2.91 -2.39 -1.86 -1.01 75 43 33 22 07	-4.16 -7.14 -4.54 -3.39 -2.77 -2.11 -1.15 -84 -66 -37 -25 -06		2.05 1.50 .67 .19 11 24	2.24 1.79 .97 .44 .06 0	2.34 2.05 1.24 .64 .31 .04 .12 .18 .30	2.33 2.24 1.51 .91 .49 .18 .20 .21	2.24 2.39 1.73 1.10 .67 .30 .29 .40	2.14 2.53 1.94 1.30 .85 .44 .39 .46
0.31 b/ 2	0 1.5 7.0 10.0 15.0 20.0 30.0 50.0 70.0 80.0 90.0 95.0	.81 .74 01 28	1.26 .92 .25 .51 .63 .61 .51 .35 .35 .31 .24	1.55 .20 56 76 76 81 81 60 61 59 41 35 25	1.68 23 -1.90 -1.05 -1.09 -1.06 -1.00 75 61 50 41	1.72 -1.34 -1.35 -1.31 -1.31 -1.31 -1.31 -1.31 -1.35 -1.31 -1.31 -1.35 -1.30 -	1.71 -1.30 -1.74 -1.72 -1.66 -1.56 -1.44 -2.11 -1.01 66 55 04 20		-1.77 -1.75 -1.28 -1.16	-1.10 -1.26 -1.03 94 64 45 27 20	- 46 - 81 - 75 - 70 - 45 - 29 - 15 - 08 - 02	- 12 - 35 - 48 - 48 - 30 - 16 - 06 0	.61 .05 .24 .29 .15 .06 .05 .11	1.02 .27 02 13 02 04 .07 .10
0.375 b/2	0 1.5 1.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	.38 .24 .04 .09 -17 -27 -31 -28 -25 -20 -15	- 27 - 27 - 37 - 45 - 45 - 45 - 45 - 45 - 45 - 45 - 45	\$5000000000000000000000000000000000000	.05 -1.34 -1.04 -1.03 97 85 53 45 36 05	67 -2.12 -1.55 -1.44 -1.31 -1.38 -1.07 78 63 79 49 06	-1.60 -2.93 -2.05 -1.84 -1.47 -1.31 74 60 46 98 08		30 35 24 25 17 12 05 .02	.20 .05 .01 .02 .01 .03 .07	.51 .34 .25 .19 .18 .12 .11 .10 .12	.67 .56 .36 .35 .26 .24 .18		.60 .76 .73 .64 .60 .49 .44
0.44 b/2	0. 1.5 1.0 70.0 15.0 20.0 30.0 40.0 50.0 70.0 80.0 95.0	1.61 -1.77 -1.25 98 83 65 38 36 38 25 17 07	-2.76 -1.86 -1.73 -1.11 86 49 49 24 11 34 24	29 -3.95 -2.54 -2.26 -1.78 -1.13 58 46 36 26 16 01 08	-1.78 -5.23 -3.33 -2.85 -2.23 -1.76 -1.38 54 54 39 54 39 17 01	-3.65 -6.72 -1.22 -3.74 -2.12 -1.64 -1.82 -3.33 -2.00 0.09	-5.84 -8.47 -5.20 -4.19 -3.25 -2.47 -1.91 -1.93 70 52 37 03		2.00 1.39 .19 -15 -25 -13 0 .09 .21	2.24 1.75 1.01 .50 .15 06 0 .10 .15 .28	2.34 2.06 1.34 .80 .41 .10 .12 .18 .22 .32	2.24 2.28 2.28 1.63 1.07 .67 .28 .25 .25 .30 .37	2.02 2.45 1.88 1.29 .42 .33 .35 .42 .42 .13	1.75 2.77 2.11 1.50 1.08 .78 .47 .42 .41 .46

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TABLE VII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; T_c = 0.8 - Continued (a) α_u = 2°, 4°, 6°, 8°, 10°, 12° - Concluded

	Per-			Upper	surface						Lower	surface		
Spanwise	cent			Angle o	of attack							f attack		
stations	chord	20	†o	6º	8°	10°	12°	Ш	50	Ťο	6°	80	100	120
0.56 b/2	0. 1.5 4.0 7.0 15.0 15.0 30.0 90.0 90.0 90.0 90.0	\$E\$\$\$\$\$\$\$\$\$\$\$\$	28954864854857 28757	1.45 2.63 7.87 8.87 6.55 1.58 1.58 1.58 1.58 1.58 1.58 1.58 1	1.71 22 87 -1.06 -1.14 -1.20 95 85 79 43 35 06	1.83 78 -1.32 -1.44 -1.47 -1.33 -1.15 -991 72 99 49 39 06	1.85 -1.76 -1.76 -1.60 -1.76 -1.65 -1.36 -1.36 -1.36 -1.36 -1.36 -1.36 -1.36 -1.36 -1.36		-2.20 -1.95 -1.25 -96 -75 -33 -01 -06	-1.47 -1.55 -1.05 -85 -36 -26 -06 -10 -25	** 6	-0.05 -63 -70 -60 -537 -22 -14 -04 -15 -28	0.05 -24 -35 -36 -24 -36 -36 -37 -39 -30 -39 -30 -30 -30 -30 -30 -30 -30 -30 -30 -30	0.96 .10 .24 .25 .22 .17 .05 .01 .03 .24 .23
o.68 b/2	0 1,0 7,0 1,5 2,0 3,0 2,0 2,0 2,0 2,0 2,0 2,0 2,0 2,0 2,0 2	246899906500599999999999999999999999999999	8,4,4,4,4,4,4,4,4,4,4,4,4,4,4,4,4,4,4,4	\$885584588158 \$111158	- 08 -1.43 -1.28 -1.13 86 76 65 41 31 23 11 04	-1.04 -2.33 -1.78 -1.49 -1.31 -1.15 -99 -79 -61 -49 -35 -24 -11	2724884848284 474444		-34 -36 -31 -24 -19 -12 -01 -03 -06 -10	.08 .08 .13 .19 .09 .00 .00 .01 .11	.44 .83 .09 .05 .04 .06 .10 .12 .12 .12	.50 .45 .27 .20 .17 .13 .14 .14 .15 .14	. 24 . 33 . 29 . 24 . 20 . 19 . 18 . 17 . 14	.29 .60 .52 .44 .39 .29 .26 .21 .20 .15
o.8o ъ/2	0 1.5 4.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	.48 .19 .08 .18 .24 .23 .22 .23 .21 .15 .15 .01	ଞ୍ଜ୍ୟ ଅନ୍ୟୁ ହ ନିର୍ଦ୍ଦର୍ଶନ ଓ ଜ୍ୟୁ ଅନ୍ୟୁ ହ ନିର୍ଦ୍ଦର୍ଶନ ଓ	.28 .81 .76 .74 .65 .52 .33 .33 .26 .213 .07	- \$3 -1.55 -1.24 -1.03 84 70 56 40 30 23 12 0	-1.60 -2.44 -1.72 -1.47 -1.29 -1.07 -90 -70 -56 -45 -34 -21 0	-3.13 -3.52 -2.30 -1.64 -1.33 -1.11 83 65 36 23 10 04		37 38 31 24	.15 06 05 05 03 01 05 09 10	.46 .26 .12 .10 .07 .06 .10 .11 .11	.79 .45 .28 .22 .18 .15 .12 .14 .13 .12 .11	.52 .55 .40 .33 .27 .22 .17 .16 .15 .14 .11	.32 .58 .51 .43 .36 .30 .20 .18 .11
o.94 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	.31	.56 11 25 32 33 33 33 33 24 21 19 19 06 04	- 58 - 61 - 60 - 549 - 36 - 37 - 225 - 225 - 225 - 20 - 20 - 20 - 20 - 20 - 20 - 20 - 20	-14 -1.18 -1.02 976 65 54 38 26 18 102	89 -2.05 -1.44 -1.25 86 70 54 35 39 10	-2.10 -2.29 -1.91 -1.59 -1.31 -1.86 -63 -31 -18 -09 -01		24	01 07 10 09 09 05 01 .01 06 .09 10	.34 .09 .02 .02 .02 .04 .05 .06 .10	.52 30 .23 .15 .11 .09 .09 .09 .09	.53 42 .34 .26 .21 .15 .12 .11 09 .09	. 10 . 15 . 14 . 34 . 29 . 21 . 15 . 14 10 . 09 . 06

TABLE VII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; T_c = 0.8 - Continued (b) α_u = 140, 16

Spanwise Stations	Per-			Upper	surface			Lower surface						
		Angle of attack						Angle of attack						
	chord	140	16°				-	140	160					
0.10 ь/2	0 1.5 7.0 10.0 20.0 30.0 50.0 60.0 70.0 80.0 95.0	-2.22 -3.25 -2.26 -1.84 -1.34 -1.14 92 75 49 49 10	-3.31 -3.87 -2.76 -2.16 -1.76 -1.25 -1.00 80 50 39 25 11					0.45 .74 .69 .60 .77 .45 .42 .38 .34 .30	0.22 .83 .73 .64 .59 .51 .47 .43 .39 .36					
0-19 b/2	0 1.50 7.00 15.00 120.0	-5.40 -8.57 -5.40 -3.95 -3.21 -2.41 -1.27 -68 -55 -1.25 -00	-7.88 -9.98 -5.21 -5.68 -2.68 -1.40 -1.56 -1.56 -2.56 -2.56					1.89 2.62 2.11 1.47 1.01 .56 .53 .42 .49 28	1.38 2.55 2.19 1.54 1.14 .64 .60 .56 .56		:			
0.31 b/2	0 1.50 7.0 10.0 15.0 20.0 30.0 50.0 60.0 70.0 95.0	1.64 -1.87 -2.19 -2.19 -1.83 -1.65 -1.25 -1.15 74 61	1.\$2.638 29.088 1.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2.2					1.36 .66 .15 .01 .09 .12 .14 .20 .22	1.67 .90 .31 .14 .20 .22 .26 .26 .29					
0.375 b/2	0. 1.5 2.0 15.0 20.0 30.0 40.0 50.0 60.0 90.0 95.0	-2.85 -3.88 -2.62 -2.29 -2.07 -1.55 -1.05 85 57 36 99	14.90 13.92 13.92 13.92 14.95 15.95					.23 .75 .82 .75 .71 .79 .54 .45 .43	03 .64 .95 .98 .78 .66 .60 .50 .46					
0.44 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 50.0 50.0 70.0 80.0 90.0	-8.29 -9.23 -5.28 -5.28 -3.78 -1.41 -9.73 -1.41 -9.73 -1.41 -0.4	-11.19 -11.89 -7.44 -1.98 -2.22 -1.05 80 44 26 31					1.17 2.78 2.26 1.64 1.23 .68 .50 .47 .71	08 2.24 2.21 1.59 1.31 .55 .55 .55 .52 .26 .18			(Z)		



TABLE VII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; T_c = 0.8 - Concluded (b) α_u = 14°, 16° - Concluded

	Per- cent chord			Upper	surface			Lower surface						
Spanwise stations		Angle of attack								Angle	of attack			
0.56 b/2	0 1.5 *.0 10.0 15.0 20.0 30.0 \$0.0 50.0 50.0 80.0 90.0	14° 1.76 -1.94 -2.22 -2.19 -2.08 -1.87 -1.31 -1.179374624609	1.50 -2.65 -2.79 -2.43 -2.13 -1.46 -1.29 -1.02 88 98					1.36 .40 .12 .09 .07 .08 .29 .29	1.68 .66 .03 0 .01 .11 .14 .33 .30					
0.68 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	-4.28 -4.26 -3.06 -2.41 -2.04 -1.67 -1.41 -1.06 81 99 16	-6.45 -5.49 -3.75 -2.89 -2.42 -1.61 -1.20 91 68 51 23 23					13 .55 .59 .53 .48 .39 .34 .29 .25 .24	-175 .42 -61 .58 .45 .45 .40 -33 .29 .25					
0.80 b/2	0 1.5 4.0 7.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	-5.00 -4.30 -2.31 -1.20 -1.20 -1.20 -1.30	-7.25 -5.45 -3.56 -2.75 -2.80 -1.45 -1.04 75 -31 -31 -26 -22 -20						60 42 59 .56 .50 .41 30 .26 .24 .17					
0.94 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 50.0 60.0 70.0 80.0 90.0	-3.63 -3.06 -2.43 -1.94 -1.25 -1.25 -1.00 71 40 30 16 05	-5.44 -3.91 -2.93 -2.27 -1.40 -1.14 79 59 41 35 20 18 16					17 56 .53 .43 .35 .25 .20 .16 10 .07	.21 .555 .48 .40 .32 .25 .08 .04					

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TABLE VIII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.80; R = 1,000,000; $T_c = 0$ (a) $\alpha_u = 2^\circ$, 4° , 6° , 8° , 10°

	Per-	Upper surface							Lover surface						
Spanwise Stations	cent	20	10		of attack]			Angle	of attack			
0.10 b/2	chord 0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	0.64 07 -15 -29 -38 -41 -45 -43 -37 -37 -38 -37 -37 -39 -30 0	0.68 16 37 57 53 57 57 56 57 36 27 10	ତ ଚୁଣ୍ଟ ଓଡ଼ିଆ ବିଷ୍ଟ୍ର ଓଡ଼ିଆ ବିଷ୍ଟ ଓଡ଼ିଆ ବିଷ୍ଟ୍ର ଓଡ଼ିଆ ବିଷ	8° 0.577.850 1.850 1.850 1.880 1.800	100 0.49 -1.01 -1.05 -1.16 -1.10 -1.05 96 96 96 96 96 96			20 0.15 00 20 21 24 25 20 20 20 20 20 20 20 20	-035 -130 -036 -140 -155 -155 -155 -006	0.52 .30 .33 .07 .04 01 04 03 .01	8° 0.64 .43 .24 .15 .06 .04 .01 0 .04	10° 0.75 .36 .28 .24 .16 .12 .06 .09		
0.19 8/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 50.0 50.0 70.0 80.0 95.0	र् १ जन्दा । जन्म अनुस्थ	.67 41 67 78 -1.00 76 53 32 32 32	\$5844888 835844 \$58584888	33 1.55 1.35 1.35 1.36 1.36 1.36 1.36 1.36 1.36 1.36 1.36	13 -1.21 -1.50 -1.45 -1.45 -1.41 -1.60 -1.60 -1.60 -1.60 -1.61 -1.60 -1.			-17 -378 -71 -378 -71 -34 -50	.45 20 0 228 -58 -41 -12 -02 -01	-59 -19 -03 -31 -21 -08 -0 0	.67 .54 .32 .11 .22 .06 .0 .0	.70 .45 .29 .06 .01 .05 .05		
0.31 b/2	0 1.5 1.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	.63 06 38 5e 59 59 56 22 45 31 21	96 k	.54 61 91 -1.01 -1.05 -1.15 -1.09 -1.01 47 40 30 21 06	.50 84 -1.28 -1.31 -1.36 -1.39 -1.32 -1.32 -1.32 54 54 55 14 06	. 15 - 94 - 1.27 - 1.39 - 1.41 - 1.39 - 1.25 - 1.69 - 1.40 - 1.69 - 1.69 - 1.60 - 1.60			.03 19 26 28 26 23 23 23 23	.27 .05 .20 .21 .12 .12 .14 .14 .13	09 12 01 05 05 09 04	\$39 \$39 \$39 \$39 \$5 \$5 \$5 \$5 \$5 \$5 \$5 \$5 \$5 \$5 \$5 \$5 \$5	?? 5 3 4 9 1 4 8 8 5 7 7		
0.375 b/2	0 1.5 1.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 70.0 80.0 90.0 95.0	.60 05 27 46 61 67 57 33 31 21 05	.60 47 61 81 91 97 93 63 33 33 33 33	-50 90 92 -1.08 -1.19 -1.25 -1.25 47 34 34 34	-35 -1.14 -1.27 -1.31 -1.35 -1.27 -1.27 84 74 50 35	21 -1.29 -1.30 -1.42 -1.42 -1.42 -1.43 -1.45 -1.			-32 -33 -33 -34 -18 -05 -05	.31 .06 09 15 40 20 14 20 15	50.00 50.00	.60 .41 .21 .13 .08 .03 .03 .05 .01	क इ.स. १५६ १ ५५ १ ५५ १ ५५		
0.44 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	.71 17 41 61 67 87 99 40 44 28 17 00	.65 60 76 76 -1.04 -1.18 -1.21 -1.10 49 44 38 29 19 05	48 97 -1.11 -1.20 -1.24 -1.19 -1.18 -1.01 85 64 49 35 24 15	.26 -1.20 -1.27 -1.21 -1.20 -1.06 -1.01 91 82 59 49 49	.08 -1.01 -1.04 98 95 91 87 81 75 68 54 49 37			.23 06 21 38 65 73 33 16 04	.38 .20 .33 .142 .39 .168 .05	.61 .41 .20 .32 .32 .32 .35 .35 .35	.66 .54 .39 .19 03 21 06 03 0	.67 .69 .45 .28 .08 .13 .11 .06 .06 .04		

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TABLE VIII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.80; R = 1,000,000; T_c = 0 -. Concluded (a) α_u = 2°, 4°, 6°, 8°, 10° - Concluded

	Per-			Upper	surface					Lover	surface		
Враду іве	cent				f attack		 . 1			Angle (of attack		
stations	chord	50	140	60	8°	700		50	40	60	80	10°	
0.56 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	0.49 - 13 - 55 - 56 - 55 - 55 - 55 - 54 - 12 - 18 - 18 - 18 - 18 - 18	0.51 44 65 86 95 86 97 86 97 47 47 49 19 05	0.49 -1.50 -1.68 -1.168 -1.168 -1.168 -1.168 -1.168 -1.168 -1.168 -1.168 -1.168 -1.168 -1.168 -1.168 -1.168	0.45 90 -1.10 -1.20 -1.31 -1.29 -1.21 12 44 40 36 27 12	0.42		-0.02 26 32 31 29 24 19 04	0.25 .81 11 15 14 14 12 11	0.45 .23 .06 .01 0 01 03 03 03	0.55 .33 .12 .09 .06 .03 .01 01 03 .01	0.62 .41 .21 .13 .11 .06 .04 .01	
0.68 ъ/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 70.0 80.0 90.0	\$11336 \$5\$5 \$5\$5 \$5\$5 \$5\$5 \$5\$5 \$5\$6 \$5\$6 \$	\$266698848674864658	.54 63 -1.00 -1.10 -1.15 -1.11 -1.15 -1.11 30 20	\$9.14.4 11.45.5 11.45.	35 8 8 8 8 5 5 5 5 5 5 8 8 8 8 8 8 8 8 8		1936363639241601 .03 .08 .10 .11	-21 -01 -116 -15 -12 -09 -01 -01 -10	.45 .24 .09 .01 .01 .01 .01 .05 .06 .10	.54 .35 .16 .09 .07 .03 .03 .04 .04	.58 .41 .24 .16 .13 .06 .05 .01 .04	
0.80 ъ/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	8.14889358858858 	.61 -34 -53 -76 -76 -77 -61 -55 -32 -32 -16 -01	.46 77 91 -1.03 72 -1.04 -1.00 96 57 38 29 10 0	ଞ୍ଚଳ ବ୍ୟକ୍ତ ପ୍ରଥ ଓ ୭.୬.୬.୬.୬.୭.୭.୭.୬.୭.୭.୭.୭.୭.୭.୭.୭.୭.୭.୭	8 5 5 8 8 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5		-25 -37 -35 -33 -26 -20 -05 -01 -08 -10	.20 01 11 14 11 09 03 0 .06 .09 .09	.44 .25 .09 .04 .01 .05 .06 .08 .10	.66 .54 .35 .19 03 21 11 06 03 0	.67 .60 .45 .28 .08 .01 .11 .09 .04	
0.94 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 97.0	.48 .19 02 25 30 31 35 31 24 24 24 24	.60 21 40 51 56 57 57 45 37 26 17 10	.54 66 79 90 -1.87 87 36 30 21 08	-1.05 -1.05 -1.06 -1.06 -1.08 -1.91 54 35 36 00	.29 -1.26 -1.16 -1.06 -1.00 -1.00 -1.00 80 70 59 51 31 22 16		49 40 35 30 20 09 04 09 12	.06 11 15 15 11 09 05 06 .09	.38 11 .05 0 0 01 .01 02 .06 .10	.48 .07 .07 .01 .01 .01 .04 .06	.54 .19 .12 .09 .01 0	

COMPLETED IN IT ALL

TABLE IX.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.80; R = 1,000,000; T_c = 0.04 (a) α_u = 2°, μ^o , 6°, 8°, 10°

	Per-			Upper	surface		 П			Lover	surface		
Spanwise Stations	cent				of attack		ſt				of attack		
Bracions	chord 0 1.5	2° 0.66 .09	0.69 15	60 0.66 42	8° 0.59 70	0.48 -1.04	H	20 0.17	40 0.37	6º 0.55	80 0.66	10° 0.76	
0.10 b/2	1.70 7.00 10.00 20.00 30.00 40.00 50.00 60.00 90.00 95.00	55568545455858588 1111111110	35 36 50 56 57 57 60 33 27 08		81 95 91 83 86 80 80 36 25 07	-1.04 -1.06 -1.13 -1.10 -1.01 91 85 70 52 41 22		06 14 16 20 20 21 21 07	.37 .15 .03 09 10 10 07 02	.16 .11 .09 .04 .01		.57 .39 .33 .28 .20 .16 .11	
0.19 b /2	0 1.5 4.0 7.0 15.0 20.0 30.0 40.0 50.0 70.0 80.0 95.0	858881 6887888 858887888	.72 56 81 86 91 -1.08 95 36 50 43 35 28 08	-59 -1.19 -1.19 -1.19 -1.19 -50 -1.19 -50 -1.19 -50 -1.50 -1.50 -1.50 -1.50 -1.50 -1.50	-1.10 -1.41 -1.45 -1.44 -1.51 	-1.27 -1.52 -1.45 -1.40 -1.21 -1.84 65 48 28 23		.48 .23 01 85 66 82 11 03 .03	.66 .43 .19 06 45 53 09 01 .04		.84 .70 .49 .26 03 09 01 .04 .06	.86 .80 .40 .13 .01 .04 .07	
0.31 b/2	0 1.5 7.0 10.0 15.0 20.0 40.0 50.0 70.0 70.0 80.0 90.0	5.000 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	.60 20 55 68 73 80 76 80 72 51 46 36 24 05	-60 -48 -84 -1.84 -1.16 -1.16 -1.16 -1.53 45 33 66	.59 - 68 -1.03 -1.15 -1.20 -1.20 -1.23 -1.29 -1.29 -1.44 30 24 30	-59 -81 -1.20 -1.31 -1.43 -1.43 -1.43 -1.43 -1.43 -1.46 87 59 40 18		12 36 35 39 25 25 23 23	15 15 16 19 12 14 14 12	.40 .19 .03 01 01 05 05 05	58 .35 .16 .10 .07 .04 .07	.68 .47 .26 .20 .18 .14 .09 .05 01	
0.375 b/2	0 1.5 7.0 15.0 15.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 2	ଓ ପ୍ରକ୍ରନ୍ତ କ୍ଷନ୍ତ କ୍ଷମ କ୍ଷନ୍ତ କ୍ଷନ୍ତ କ୍ଷନ୍ତ କ୍ଷନ୍ତ କ୍ଷନ୍ତ କ୍ଷନ୍ତ କ୍ଷନ୍ତ କ୍ଷନ୍ତ କ୍ଷମ କ୍ଷନ୍ତ କ୍ଷମ କ୍ଷମ କ୍ଷମ କ୍ଷମ କ୍ଷମ କ୍ଷମ କ୍ଷମ କ୍ଷମ	64 41 56 76 82 90 91 82 70 36 30 20 04	-51 -86 -89 -1.05 -1.23 -1.26 -1.26 -1.44 44 42 07	.39 -1.11 -1.25 -1.33 -1.35 -1.31 -1.31 91 97 67 67 36	-1.40 -1.42 -1.42 -1.35 -1.35 -1.35 -1.35 -1.35 -1.35 -1.35 -1.36 -1.36		01 24 30 31 31 31 31 09 09	.30 .07 06 12 15 17 20 11 02	.49 .29 .29 .11 .03 0 05 09 06 01	.60 .43 .25 .16 .11 .04 01 04	.65 .54 .24 .20 .11 .05 01 01	
0.44 5/2	0 1.5 4.0 7.0 15.0 20.0 30.0 40.0 50.0 60.0 90.0 95.0	.82 - 25674515590 	.69 75 87 -1.02 -1.11 -1.24 -1.26 -1.19 67 34 27 17 03	-50 -1.08 -1.29 -1.31 -1.25 -1.25 -1.09 97 75 56 24 14	.30 -1.20 -1.20 -1.06 -1.06 97 96 91 80 71 58 49 37	.10 -1.06 -1.11 -1.04 94 99 86 77 59 51 41		05 26 26 35 05 05 .08	- 64 - 39 - 15 - 36 - 36 - 36 - 36 - 36 - 36 - 36 - 36	.77 .78 .34 .14 10 36 10 04 01	.82 .69 .47 .29 .05 .21 .09 .04 04 02	.85 .79 .59 .40 .17 10 04 02 0	

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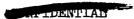


TABLE IX.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.80; R = 1,000,000; T_c = 0.04 - Concluded (a) α_u = 2°, 4°, 6°, 8°, 10° - Concluded

	Per-			Upper	surface		 ГΤ			Lover	surface		
Spanwise stations	cent			Angle (of attack		l [Angle	of attack		
10000000	chard	20	40	60	80	10°	LF.	20	ħo.	60	80	100	
0.56 b/2	0 1.5 4.0 7.0 15.0 20.0 30.0 40.0 50.0 70.0 80.0 90.0 95.0	\$588558\$\$\$\$\$\$\$\$\$\$\$\$\$	0.57 25 52 70 80 96 51 51 30 30 30 30	0.59 53 76 99 -1.16 -1.19 -1.09 64 45 36 30 21 06	0,56 -,71 -1,95 -1,12 -1,24 -1,27 -1,21 -,85 -,37 -,34 -,37 -,11 -,04	0.54 -1.85 -1.19 -1.35 -1.33 -1.85 -1.40 36 30 10		-0.21 45 44 38 31 24 21 12 04	0.12 25 25 21 18 16 13 10 03 .01	0.38 .10 07 08 08 06 06 06 05	0.49 .23 .06 .01 01 01 02 03 03 .02 01	0.60 .36 .17 .10 .08 .05 .05 .02 -01	
0.68 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 50.0 50.0 80.0 95.0	47 -14 -34 -45 -45 -45 -43 -45 -43 -43 -45 -43 -45 -45 -45 -45 -45 -45 -45 -45 -45 -45	.59 82 81 81 82 33 42 43 43 43 43 43 43 43 43	.53 69 -1.15 -1.15 -1.16 -1.14 31 31 31 31	-1.10 -1.10 -1.09 -1.09 -1.74 74 74 74 74 74 74 79 39 14	-29 -1.11 -1.05 -1.01 -1.04 -1.0980765747403025		40 40 39 32 26 15 02 .08	13 13 13 15 13 09 01	.41 .21 .06 0 0 .05 .05 .05 .11 .10	906 65 6 1 55 8 6 6 6 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.58 .43 .26 .17 .14 .09 .07 .06 .06 .03	
0.80 b/2	0 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.5	59.44885434445558887 8	.60 31 63 69 70 50 33 43 43 22 10 08	- 46 - 80 - 94 - 1.06 - 1.06 - 1.06 - 1.99 - 49 - 1.30 - 1.11 - 1.05	2004 11112 11114 11114 1114 1114 1114 11	15 11.22 11.26 11.12 11.12 11.12 11.12 11.13 11.		40 40 35 86 60 00 00 00 00 00 10		. 44 . 24 . 09 . 04 . 04 . 01 . 05 . 05 . 09 . 09 . 09	54.46.465.5888855		
0.94 b/2	0 1.5 4.0 7.0 10.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	.47 .20 .01 22 28 33 34 31 27 22 11	63 - 19 - 37 - 34 - 54 - 54 - 54 - 54 - 54 - 54 - 54 - 5	54 - 69 - 89 - 89 - 89 - 10 - 10 - 10 - 10 - 10 - 10 - 10 - 10	.40 -1.07 -1.19 -1.19 -1.04 -1.55 -1.35 -1.19 -1.19 -1.00 -1.19 -1	.27 -1.30 -1.15 -1.09 -1.07 -1.00 -7.79 70 56 50 30 30		51 39 35 29 21 07 04 06 09 12	.07 14 15 12 11 06 06	.37 .11 .05 001 04 01 007	.48 .21 .14 .08 .05 .01 .04 .05 .05	.54 .29 .21 .14 .10 .05 .04 .01 .04 .04	





TABLE X.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.90; R = 1,000,000; T_c = 0 (a) α_u = 2°, μ^o , 6°, 8°

Spanwise	Per-			Upper	surface.	 			Lover	surface	
stations	cent chord			Angle o	f attack				Angle c	fattack	
0.10 8/2	0 1.5 4.0 7.0 10.0 15.0 20.0 50.0 50.0 70.0 80.0 90.0	% 6 111111111188278	4° 0.72 0.72 0.72 0.72 0.72 0.72 0.72 0.72	6° 0.70 16 19 19 19 54 55 55 69 16	8° 0.69\$1567073676768667186		2° 0.20041315192327414601	-01 -05 -07 -07 -12 -16 -23 -36 -36 -06	.15 .10 .06 .07 .15 .06 .07 .11 .15 .07 .07	8° 0.65 .4426 .39 .030105	
0.19 b/2	0 1.5 7.0 10.0 15.0 20.0 \$0.0 \$0.0 70.0 80.0 90.0 95.0	83088888 830888888888888888888888888888	Passed 88884485	.63 86 68 86 77 86 67 66 67	.53 68 99 -1.00 -1.13 12 84 84 85 85		.34 .13 05 61 63 63 11 .01	.49 .20 .07 14 51 56 56 56	.60 .43 .04 -29 -555 -66		
0.31 ъ/2	0 1.5 4.0 7.0 15.0 20.0 40.0 50.0 70.0 70.0 70.0 70.0	80000000000000000000000000000000000000	55446 8666 867 867 867 867 867 867 867 867 8	- 59 - 26 - 55 - 75 - 75 - 75 - 80 - 83 - 84 - 75 - 26 - 22	.61 -49 -69 -69 -69 -69 -69 -69 -69 -69 -69 -6		1 05 29 1 39 55 1 26 26 26 1 37 1 35 55 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	15 -06 -18 -20 -19 -18 -20 -21 -3 -27	.37 .18 .04 -01 -01 -02 -06 -09 -29	.63 .34 .15 .09 .06 .04 .08 08 18	
0.375 b/2	0 1.5 7.0 15.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9	\$69%\$\$\$\$ Pappast	63 - 20 - 39 - 66 84 - 50 - 73 - 73 - 73 - 73 - 73 - 73 - 73 - 73	- 56 - 56 - 56 - 58 - 59 - 59 - 59 - 59 - 59 - 59 - 59 - 59	.54 -75 -82 -91 -1.00 -1.11 65 73 73 59 51		02 26 32 33 34 37 37 33 34 37	.24 0 14 19 21 26 30 46 40	.43 .20 .04 04 07 13 20 35 35	.55 .55 .07 .01 .08 .11 .30 .12 .12 .21	
0.44 ъ/2	0 1.5 7.0 10.0 15.0 20.0 30.0 50.0 70.0 80.0 95.0	74 1 27 1 37 1 37 1 37 1 37 1 37 1 37 1 37 1 3	.80 51 666 91 976 79	.627 -770 -886 -866 -775 -863 -750 -750 -750 -750 -750 -750 -750 -750	.48 81 -1.01 93 86 84 76 79 75 73 69 51		.25 04 11 56 63 48 34 34 22	0 15 - 40 - 15 - 18 - 01 - 08 - 08	.57 .35 -01 -22 -54 -75 -39 -04 .04	.66 .49 .10 .14 .10 .45 .68 .17 .06 .05	

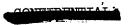


TABLE X.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.90; R = 1,000,000; T_c = 0 - Concluded (a) α_u = 2°, 4°, 6°, 8° - Concluded

	Per-			Upper	surface		Т			Lower	surface	
Spanwise	cent		·		f attack						fattack	
stations	chord	20	40	60	8°		[20	ì.º	8	8°	
0.56 b/2	0 1.5 7.0 15.0 15.0 30.0 40.0 50.0 70.0 90.0 90.0	0.45 01 27 56 69 73 63 18 19 01	0.51 - 144 - 1596 - 837 - 837 - 857 - 857 - 166 - 166 - 166	0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.51 55 75 63 1-1-5 1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1			1931 428 1330 11300 11300 11300 11300 11300 11300 11300 11300 11300 11300	୍ରୀ । ଅଧିକ ।	0.000	0.118	
0.68 b/2	0 15.0 10.0 10.0 20.0 40.0 56.0 70.0 95.0	\$4150950899868654 111111111111111111111111111111111111	569598777834577719 111111111111111111111111111111111	.59 30 79 79 70 44 33 24 20	.51 52 55 851 83 51 51 44 51 433 30			21 42 43 44 37 30 16 01 .04 .09	.10 13 22 26 24 20 16 05 .01 .05	.30 .08 .05 .12 .11 -12 08 01 .04 02	. 22 . 23 . 03 . 03 . 03 . 05 . 05 . 06 . 04 . 08 09 15	
0.80 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	33.428955499548831 1111111111111111111111111111111111	45%500000000000000000000000000000000000	598 - 586 - 686 -	- 64 - 89 - 100 -			22 39 40 35 29 24 04 .01 .06 .10 .12	10 10 19 21 16 13 05 01 .07 .10	-31 -10 -03 -08 -06 -06 -01 -01 -01 -04 -09	.44 .21 .05 .01 .01 .05 .05 .05 .03	
0.94 b/2	0 1.5 4.0 7.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 90.0 95.0	.51 0 15 -15 -25 -36 -36 -33 -29 -23 0 09	.62 09 30 36 57 55 59 56 54 20 05 09	-64 -34 -47 -676 -766 -663 -631 -45 -322 -106 -03	-51 -64 -78 -89 -82 -75 -54 -54 -327 -25			47 43 36 32 25 09 03 08 .13 .15	0 15 19 20 14 09 06 11 .13	.26 03 04 07 07 07 05 05 05 05 05	.38 .05 -01 -05 -07 -08 -08 -08	ACA

<u>د</u> - TABLE XI.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.90; R = 1,000,000; T_c = 0.03 (a) α_u = 2°, 4°, 6°, 8°

	Per-			Upper	surface		 т		Lower	surface		
Spenvise Stations	cent				f attack					fattack		
peacions	chord	50	10	€	80	[T	20	70	€_	-8°		
0.10 ъ/2	0 1.5 4.0 7.0 10.0 20.0 30.0 40.0 50.0 60.0 70.0 90.0 95.0	0.69 .19 05 16 22 28 33 34 37 55 55	0.74 022 36 41 45 51 55 69 69 21	0.74 20 40 51 53 54 60 61 61 71 81 31	0.69 41 37 70 67 66 70 66 67 79 86 39 35		0.51 01 10 12 14 16 21 28 38 38	0.39 .16 .01 02 06 12 18 13 24	0.54 .31 .17 .11 .09 .03 10 16 05	0.66 .46 		
0.19 b/2	0 150 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	81.06 83.35.61 - 70.64 - 55.57.68 80.08	.84 26 54 68 85 87 64 89 87 64 37 17	.69 78 84 01 77 77 24 21	.55 71 99 -1.03 -1.05 -1.15 84 84 84 28		.36 .15 .03 .22 .57 .79 .78	.65 .41 .20 .05 .41 .80 .61 .05 .05	.75 .55 .99 .27 01 01 .03	.84 .66 .41 .21 .11 .41 .01 01		
0.31 b/2	0 150 700 1500 1500 1500 1500 1500 1500	50 038 934 55 66 664 141 104	.60 06 41 75 86 91 98 72 29 14	. 64 - 58 - 59 - 59 - 1. 69 - 79 - 1. 69 - 79 - 1. 69 - 79 - 1. 69 - 79 - 79 - 79 - 79 - 79 - 79 - 79 - 7	.64 42 75 86 91 -1.05 -1.10 -1.09 -1.00 73 64 73		13 25 32 38 25 23 23 23 23		.31 .10 .04 .06 .06 .06 .10	.27 .27 .27 .05 .05 .01 -06 18		
0.375 b/2	0 1.5 4.0 7.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	.58 .08 -16 -36 -46 -59 -65 -82 -82 -751 -04	.68 -36 -57 -67 -83 -95 -99 -99 -131 -131	63 - 55 - 65 - 65 - 65 - 65 - 65 - 65 - 65	.54 71 76 99 -1.07 -1.11 -1.02 84 74 74 68 63 56		1.8.1.8.8.8.8.8.1.1.1.1.1.1.1.1.1.1.1.1	.24 0 12 18 24 24 24 25 24 25 25 25	.41 .19 .04 04 07 13 19 36 41	.55 .35 .17 .09 .05 .04 .10 .28 .35		
0. 1 4 b/2	0 1.5 4.0 10.0 15.0 20.0 20.0 20.0 50.0 70.0 60.0 95.0	.82 10 31 59 75 83 -1.00 06 11 64 14 01	.76 37 55 70 94 -1.00 96 70 60 41 31 26	.63 63 91 91 91 861 73 45	.51 -84 -1.00 91 85 85 76 74 74 86 75		25 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	.5% 26 .69 .37 .37 .38 .37 .38 .38 .39 .39 .39 .39 .39 .39 .39 .39 .39 .39	.68 .44 .25 .66 .29	.77 .79 .39 .21 .04 .33 .01 .20 .30	£ (2)	

TABLE XI.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.90; R = 1,000,000; T_c = 0.03 - Concluded (a) α_u = 2°, 4°, 6°, 8° - Concluded

	Per-			Upper	surface	 	П			Lover	surface	
Spanwise	cent			Angle o	of attack	 				Angle o	f attack	
stations	chord	50	Ιφο	6°_	80			50	ý0	60	80	
0.56 b/e	0 1.5 4.0 7.0 15.0 20.0 20.0 \$0.0 \$0.0 \$0.0 \$0.0 \$0.0 \$0	0.48 .06 22 30 67 77 77 65 30 30 30	0.54 16 41 57 65 83 87 90 85 45 22 20 06	0.55 -30 52 66 75 89 95 96 91 57 31 22 14	0.5*497086 -1.00 -1.04 -1.10 -1.05 -1.6544302218			-0.17 -43 -55 -49 -46 -37 -22 -15 -29 -23	0.07 -18 -29 -29 -26 -27 -21 -19 -05 -05	0.24 01 15 16 16 14 15 06 06	0.36 .114 .01 .05 .06 .09 .10 .10 .10 .10	
0.68 b/2	0 11000 1200	.16 .15 -20 -36 -,46 -,56 -,56 -,56 -,17 -,17 -,17 -,10	.57 08 44 56 77 75 74 75 40 26 15 05	.57 30 61 74 79 77 74 50 35 35 21	.68 51 90 90 85 85 65 57 49 431 29			24 46 45 45 37 30 15 04 10	.10 11 21 25 22 19 12 04 .08	.26 .06 .09 13 13 10 04 04 02	4 .055 .06 .05 .06 .05 .07	
0.80 b/2	0 1.5 7.0 10.0 15.0 20.0 20.0 70.0 80.0 70.0 80.0	.61 .16 10 36 45 51 44 39 33 24 06	.65 15 37 53 61 71 79 70 68 65 32 16 07	.58 39 57 80 87 85 79 69 52 16	.46 65 81 99 96 -1.02 97 94 69 73 61 52 35 29			23 39 35 28 21 03 .03 .01 .11	.13 06 17 20 15 11 04 .03 .08 .10	.31 .10 05 09 07 07 02 .04 .08 .08	.43 .24 .06 .01 .01 .04 .02 0	
0.94 6/2	0 1.5 4.0 10.0 15.0 20.0 30.0 40.0 50.0 70.0 80.0 95.0	.52 04 02 22 27 35 37 34 31 26 21	.64 10 29 45 57 58 65 56 56 56 56 56 50 01	.61 35 50 63 77 76 76 65 46 23 23 25 05	.54 64 75 93 94 82 75 63 54 41 34 23			45 41 40 35 30 20 06 0	.04 14 17 20 15 14 09 06 07 11 .13 .15	.05 .09 .09 .09 .09 .09 .05	.43 .12 .05 01 04 05 06 06	

TAPPIAI.

TABLE XII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; PROPELLERS REMOVED (a) $\alpha_{\rm U}$ = 2°. 4°. 6°, 8°, 10°, 12°

				Upper so	rface			-			Lower su	rface		 -
Spacorise	Per-			Angle of			$\overline{}$	ı h			Angle of	attack		
stations	cent chord	20	40	60	80	10°	120		. 2º),o	60	80	100	12 ⁰
0.10 ъ/2	0 1.5 7.0 19.0 19.0 30.0 30.0 50.0 70.0 80.0 70.0 80.0 70.0	0.55 04 20 30 35 35 35 35 26 25 25 218 11	0 1 1 1 1 1 1 1 1 1	0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.19 1.08 98 980 1.08	-0.57 -1.57 -1.39 -80 55 39 39 39 39 39 39 39 39	-0.11 -e.11 -i.16		0.02 17 19 20 20 16 13 15 05	୍ଷ୍ଟ୍ର ଓଟ୍ଡର୍ଗ ଓଟ୍ଡର୍ଗ ପ୍ର	දැන පිහිසුස් ස් දේ සිසු	্র্যা মান্ত্র হত্ত হ	0.65 .53 .35 .27 .23 .16 .12 .19 .10	68 GERPERE
0.19 Ъ/2	0 1.0 7.0 15.0 150.0 30.0 50.0 780.0 780.0 780.0 780.0 780.0	-40 -17 -37 -40 -43 -48 -31 -27 -23 -21 -27 -01	0.000 0.000	748886 52458850	39 11111109 16575692858	1.50 1.14 1.13 1.14 1.14 1.14 1.14 1.14 1.14	9.37 9.37 9.47 9.47 1.48 1.49 1.49 1.49 1.49 1.49 1.49 1.49 1.49		08 13 29 33 36 29 19 07 07 03	.38 .15 05 14 20 19 12 04 .01		.60 .55 .21 .01 .01 .01 .03	98, 35 BBG 66 BB	.32 .64 .64 .35 .19 .14 .93 .19
0.31 b/2	0 1.5 7.0 7.0 19.0 19.0 20.0 20.0 70.0 70.0 70.0 70.0 70.0	.48 37 40 41 45 36 36 38 24 19 01	1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-	\$58855554 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	27.326.58888.4335.6 111111111111111111111111111111111111	1916 1916 1917 1917 1977 1977 1977 1977	1.286 1.48.28 1.4.53 1.4.4.3.3.5 1.4.5.3.5 1.4.5.3.5 1.6.5 1		្នាក់	.66 .05 07 11 11 10 06	.47 .28 .09 .03 .02 01 02 03 03 03	.60 .45 .24 .17 .14 .10 .05 .04 .03	49. 4 HERES & 149.	
0.375 b/2	0 1.5 2.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	5.5.5.0.0.5.3.5.0.5.5.0.5.5.0.5.5.0.5.5.5.5	48 60 63 63 63 63 63 63 63 63 63 63 63 63 63	.18 -1.20 -1.01 87 79 72 52 43 35 29 05	- 42 -1.89 -1.37 -1.24 -1.14 -1.00 89 49 40 31 05	-1.26 -2.69 -1.83 -1.59 -1.42 -1.21 -1.06 68 99 43 23 06 0	2.63557138 P.5955858		- 20 - 20 - 20 - 20 - 20 - 20 - 20 - 20	.31 .08 05 08 11 11 09 03 0	.51 .30 -14 .06 .04 0 0	.577 .47 .28 .20 .15 .10 .08 .07 .07	.50 .56 .30 .30 .35 .18 .15 .11 .19	.33 .60 .51 .42 .35 .26 .22 .15 .15
0.44 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 76.0 80.0 95.0	- 59 - 73 - 149 -	49 -74 -73 -73 -767 -660 -545 -383 -395 -1950	.04 -1.36 -1.16 -1.06 83 78 61 51 43 37 19 05	75 -2.16 -1.52 -1.39 -1.04 58 48 39 19 05	-1.87 -3.04 -2.06 -1.77 -1.23 -1.10 82 53 \$1 19 03	\$\$\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	•	.08 ,14 23 30 36 30 11 05 0	.43 .19 .01 .09 .16 .17 .12 .06 .08	.59 .43 .22 .10 .01 06 04 01 .05 04	.57 .57 .57 .41 .27 .17 .05 .03 .04 .05 .07	.54 .53 .54 .29 .14 .99 .99 .91 .04 .01	6.64 5.54 5.60 9.11 9.11 9.11 9.11 9.11 9.11 9.11 9.1

TABLE XII. - PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; PROPELLERS REMOVED - Continued (a) α_u = 2°, 4°, 6°, 8°, 10°, 12° - Concluded

	Per-			Upper	surface							surface		
Spanwise stations	cent chord				fattack							fattack	100	120
	Q	2° 0.47	40 0.46	6º 0.23	-0.25	10° -0.96	12 ⁰ -1.92	Н	50	_ + ₀				
0.56 b/2	1.5 1.0 10.0 15.0 20.0 30.0 50.0 50.0 50.0 95.0	1.01 1.339 1.450 1.339 1.450 1.339 1.450 1.339 1.450 1	29616366659555555584858	\$	-1.34 -1.34 -1.39 -1.05 -1.05 -1.55 -1.55 -1.55 -1.57 -1.37 -1.37 -1.39 -1.06 -1.06	00000000000000000000000000000000000000	74.85932.6767.74.332.668 8		-0.06 25 26 24 21 16 13 01	0.26 .03 09 10 11 09 07	े. ११ १९ १९ १९ १९ १९ १९ १९ १९ १९ १९ १९ १९	0.60 .44 .24 .17 .14 .09 .06 .06	0.59 .56 .38 .29 .18 .15 .12 .10 .06	0.51 .64 .50 .42 .35 .27 .22 .19 .09
0.68 b/2	0 1.5 1.0 10.0 15.0 20.0 30.0 40.0 70.0 80.0 90.0 90.0	. 45 . 04 . 23 . 33 . 33 . 33 . 33 . 33 . 33 . 33	.54 57 57 51 51 34 33 36 101 00	88. 	1.39 1.18 1.18 1.88 1.58 1.58 1.58 1.58 1.58	-2.37 -1.33 -1.52 -1.36 -1.36 -1.33 64 52 38 26 26	7 1 - 31 7 1 - 37 7 1 - 39 7 1 -		15 26 24 22 16 14 09 03 .06 .08	23 03 1 5578864 1 58899	- 17 - 17 - 18 - 18 - 18 - 18 - 18 - 18 - 18 - 18	.26 .18 .16 .12 .11 .11 .12 .10	.50 .53 	.31 .57 .47 .39 .34 .26 .22 .19 .16 .19
о.80 ъ/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 90.0 95.0	.53 .05 14 25 31 32 32 37 25 20 11	.53 37 48 51 52 50 45 41 35 25 21 03	.21 91 84 80 73 69 46 43 36 36 24 24	1-578 1-1-578 1-1-1-1-60 1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-	1.42 2.33 1.43 1.43 1.29 1.59 1.59 1.59 1.32 1.32 1.32 1.32 1.32 1.32 1.32 1.32	-2.70 -2.79 -2.81 -1.81 -1.57 -1.88 51 58 51 58 51 59 51		- 21 - 27 - 21 - 21 - 21 - 21 - 21 - 21 - 21 - 21		- 145 - 11656 - 659999	.56 .42 .25 .18 .15 .11 .10 .10	.53 .51 .36 .27 .24 .19 .11 .13 .11	.38 .55 .37 .37 .32 .25 .16 .15 .12
0.94 b/2	0 1.5 1.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	.39 .16 03 20 21 24 25 20 21 21 09	.56 20 32 39 40 38 38 34 30 26 216 10	.43 63 65 59 55 41 33 26 11 0 .06	.01 -1.18 -1.04 80 55 44 34 34 29 20	74 -1.93 -1.39 -1.22 -1.05877146383112 0	-1.80 -2.26 -1.84 -1.56 -1.30 -1.06865242332001		- 40 - 26 - 29 - 23 - 23 - 23 - 24 - 25 - 25 - 25 - 25 - 25 - 25 - 25 - 25		.33 12 .05 .01 01 01 04 05 .07	.49 .12 .09 .05 .05 .05 .05 .05 .05 .05 .05 .05 .05	.52 .38 .30 .21 .17 .11 .09 .09 .09	. 44 47 . 39 . 30 . 24 . 18 . 13 . 11 08 . 06 . 09

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TABLE XII. - PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; PROPELLERS REMOVED - Continued (b) α_u = 14°, 16°, 18°, 20°

	Per-	1		Upper a	urface	 			Lower s	urface	
Spanwise stations	cent			Angle of	attack				Angle of	attaok	
······································	ohord 0 1.5	114° -1.41 -2.68	16° -2.15 -3.33	18° -2.92 -3.92 -2.66	20° -3.65 -4.21		0.60	0.50	18° 0.38	0.25 	
0.10 b/2	4.0 7.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	-1.95 -1.39 -1.18 -1.83 66 53 53 34 10	38553288655333218 417771111111	-2.86 -2.77 -1.20 757 579 34 149	-2.90 -2.27 -1.84 -1.01 93 77 61 27 20		.70 .46 .39 .30 .26 .23 .20 .19	.73 .61 .82 .46 .37 .33 .33 .30 .20 .4	.74 .68 .52 .36 .33 .36 .26 .1.4 .07	.73 .61 .56 .45 .40 .35 .30 .27	·
0.19 5/2	0 1.50 7.00 105.	3.64 4.01 4.069 4.069 4.791 1.79 1.79 1.29 1.29 1.078	549.65 43.65 43.75	-6.52 -5.708 -2.61 -2.61 -5.74 -2.40 -3.15 -3.15 -3.15 -3.15 -3.15 -3.15 -3.15 -3.15			.60 .60 .69 .85 .유기 기기 기기 1 .64	-38 -51 -74 -67 -55 -36 -26 -17 -16	-82 .39 -77 .74 .62 .42 .30 -19 .19	-55 -59 -79 -74 -62 -31 -19 -17 -01	
0.31 b/2	0 1.5 7.0 10.0 15.0 20.0 30.0 40.0 50.0 70.0 80.0 90.0	**************************************	3.50 3.50 3.41 3.68 -1.68 -1.66 -1.65 -1.65 -1.65 -1.65 -1.65	4.52 -5.17 -2.18 -2.18 -1.19 -	-5.00 -5.17 -3.47 -2.23 -1.79 -1.45 77 61 59 39 36		. 40 .69 .59 .51 .36 .28 .24 .17	.33 .70 .68 .59 .54 .35 .29	01 .68 .73 .66 .59 .49 .38 .32 .19 .06	-15 .64 .75 .68 .63 .51 .41 .34 .19	
0.375 b/2	0 1.5 4.0 7.0 19.0 15.0 20.0 30.0 50.0 50.0 70.0 80.0 95.0	ନ୍ଧ୍ର ଅଧିକ ଅଧିକ ଅଧିକ ଅଧିକ ଅଧିକ ଅଧିକ ଅଧିକ ଅଧିକ	28282745 882545234 55744777 1 1 1 1 1 1 1 1 1	%%%%%%%% \$\$\\\\\\\\\\\\\\\\\\\\\\\\\\\\	4.8 5.97 5.27 1.13 1.06 1.09 1		.04 .56 .56 .50 .44 .35 .30 .22 .19	27 -53 -63 -57 -51 -51 -34 -20 -09	47 .51 .68 .61 .55 .43 .35 22 .16	68 .46 .69 .64 .58 .46 .37 22 .16 19	
O.44 b/2	0 1.5 4.0 7.0 15.0 20.0 30.0 40.0 50.0 60.0 90.0	7.4 7.4 4.4 7.4 7.4 7.4 7.4 7.4 7.4 7.4	5.74 7.74 7.74 7.74 7.74 7.74 7.74 7.74	7.74 7.74 7.74 7.74 7.74 7.74 7.74 7.74	-3.13 -1.12 -1.01 96 99 -1.04 99 -1.04 81 81 33 33		53 .51 .71 .64 .35 .35 .19 .16 .15	56 55 56 57 68 57 38 26 20 11 08	-33 .62 .77 .88 .98 .25 .19 .10 05	27 .63 .79 .69 .38 .25 .19 .19 .09	

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TABLE XII. - PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; PROPELLERS REMOVED - Concluded (b) $\alpha_{\rm U}$ = 14°, 16°, 18°, 20° - Concluded

	Per-			Upper	surface					surface		
Spanvice	cent			Angle o	fattack					f attack		
stations	chord	14°	16°	18 ⁰	20°		14°	16°	18°	20°		
0.56 b/2	0 1.5 7.0 10.0 15.0 20.0 20.0 50.0 70.0 90.0 90.0	77747777	-3.80 -4.37 -2.93 -2.39 -1.62 -1.31 -1.61 78 48 25 12	1479491111 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	+ 89 + 79 + 79 + 79 + 12 + 136 - 136 - 133 - 22 - 27		0.32 .68 .51 .34 .35 .29 .29 .16 .10	0.17	0.06 .67 .67 .60 .53 .44 .36 .31 .11	-0.09 .65 71 .64 .57 .39 .34 .19 .06		
0.68 b/2	0 1.5 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	\$8834854858844166	\$\f\$\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	29.7.7.85388.4.10.7.5.3538.284.284 	\$5.00 \$5.00		13 .55 .53 .46 .41 .33 .27 22 .19 .16 .11	34 49 57 46 37 46 37 46 37 46 38 48 38 48 38 38 38 38 38 38 38 3	67 .54 .50 .90 .90 .90 .90 .90 .90 .90 .90	56 .46 .56 .51 .41 .35 26 .21 .16		
o.8o ъ/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 90.0 95.0	4.17 -3.90 -2.70 -2.16 -1.97 -1.93937355391307	-5.68 -3.16 -2.19 -2.10 -1.36 -1.36 -1.00 -7.75 -39 -25 -118 -1.13	7.16 -7.55 -3.56 -2.80 -1.80 -1.80 -1.99 -1.337 -2.19	7.94 7.94 7.94 7.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1		.12 .55 .55 .38 .30 21 .20 .16 .13	20 .50 .50 .53 .45 .45 .24 .24 .20 .15		- 25 - 25 - 25 - 25 - 25 - 25 - 25 - 25		
0.9h b/2	0 1.5 1.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 95.0	-3.07 -2.83 -2.88 -1.87 -1.54 -1.00 73 34 34 05	-4.49 -3.55 -2.75 -1.75 -1.37 -1.31 79 60 44 33 20 14 11	-6.00 -4.23 -3.14 -2.42 -1.50 -1.21 -85 -47 -41 -30 -24 -21	-2.54 -1.66 -1.18 81 77 74 57 46 35 33		.24 .53 .45 .38 .30 .22 .16 .14 .05 .03	01 57 .52 .44 .36 .28 .20 .17 00	33 57 .57 .40 .31 .23 .19 .09 .05	.19 .55 .49 .42 .35 .26 .18 .13 .04 .01	N	

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TABLE XIII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.080; R = 1,000,000; PROPELLERS REMOVED (a) $\alpha_{\rm U}$ = -2°, 0°, 2°, 4°, 6°, 8°

	Per-			Upper	surface						Lover	surface		
Spacurise stations	cent	-20	00	Angle o	f attack	6°	- 8º		50		Angle o	of attack		
0.10 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0	0.43 .38 .35 .01 05 19 25 26 27 27 27	0.55 .26 .04 10 16 28 33 33 31 31 29	0.65 .06 -16 -28 -32 -39 -41 -45 -39 -33 -33 -37 -37	0.67 16 37 39 50 57 57 56 36 28	0.65 41 60 71 70 71 72 69 70 54 40	0.59 69 81 95 85 85 85 75 75 71 36 26		- 34 - 50 - 45 - 41 - 32 - 25 - 21 - 25 - 21	-0.11 -34 -37 -36 -35 -35 -35 -26 -25 -17	0.15 07 18 21 21 25 25 20 11	0.33 .11 03 07 09 13 15 16 12	.052 .28 .11 .05 .03 .03 .06 .06 .05	8° 0.64 .43 .25 .18 .14 .08 .04 .02 .05
0-19 b/2	97.0 0 1.5 4.0 7.0 10.0 20.0 30.0 40.0 50.0 60.0 70.0 90.0 95.0	04 -53 -41 02 21 35 38 38 31 28 28 24 14	01 .65 .25 05 22 36 49 45 44 40 34 28 28 20 03	.01 .71 .04 .33 .48 .60 .75 .54 .35 .31 .21	01 66 37 62 73 81 97 64 61 35 35 24 10	03537297 -1.05 -1.2190644936251009	043799 -1.29 -1.29 -1.41755745231005	-	.06 .41 .55 .56 .50 .46 .51 .50 .40	04 12 31 46 52 51 48 55 41 26	.01 .21 0 .21 .42 .64 .52 .49 .10 .02	.01 44 .21 03 25 61 44 16	.060 .40 .166 .055 .386 .266 .100	.01 69 .56 34 11 12 06 06
0.31 b/2	0 1.5 2.0 15.0 15.0 20.0 20.0 40.0 70.0 80.0 80.0 95.0	29 29 29 20 20 20 20 20 20 20 20 20 20 20 20 20	.41 .17 -11 -23 -36 -41 -42 -41 -35 -31 -24 -09	.53 .06 .38 .55 .68 .55 .55 .68 .55 .55 .68 .55 .55 .68 .55 .55 .68 .55 .55 .55 .55 .55 .55 .55 .55 .55 .5	.55 35 65 81 86 86 76 71 51 51 35 25 35	.51 .64 .94 -1.03 -1.05 -1.15 -1.06 99 47 41 36 28 09	.45 85 -1.15 -1.25 -1.25 -1.26 -1.20 -1.00 79 58 43 29 17	-	.555 .774 .855 .744 .506 .424 .36	-36 -60 -55 -51 -39 -35 -23 -23	0 -24 -33 -33 -37 -27 -27 -27 -27 -27	.25 .03 .12 .15 .15 .17 .18	.45 .23 .05 001 07 10	.59 .41 .21 .13 .11 .06 .01 .01
0.375 b/2	0 1.5 1.0 15.0 15.0 20.0 20.0 70.0 70.0 70.0 70.0 70.0 70	.23 .40 .16 .01 .21 .29 .37 .37 .39 .39	.41 .25 .01 -18 -27 -37 -41 -46 -41 -38 -34 -24 -06	88688666 - 8854 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.58 45 60 76 93 99 56 34 31 20 20	.49 .86 .91 -1.05 -1.13 -1.20 -1.13 -1.67 -39 -26	.37 -1.13 -1.23 -1.15 -1.16 -1.15 -1.11 84 75 66 61 55 47		7599 8588 68 47 29 19 15 19 5	- 44 - 69 - 64 - 29 - 35 - 46 - 35 - 18 - 11	ं अर्थ । जैने के के अर्थ । अर्थ । जैने	.30 .06 .09 .15 .17 .21 .21 .13 .06	.49 .26 .09 .01 03 08 10	.58 .39 .21 .12 .06 .05 05 06 06
0.44 b/2	1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	. 40 . 42 . 16 	.95 .24 01 23 53 56 56 54 41 30 23 13 06	66 12 355 68 85 P 54 35 P 6 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.63 54 71 86 95 -1.10 -1.11 -1.00 49 45 39 28 17 05	.49 93 -1.02 -1.12 -1.11 -1.10 84 60 55 41 29 19	.30 -1.16 -1.14 -1.16 -1.05 85 80 80 80 75 66 77 50 41		60 90 65 54 30 34 84 1 29 24	- 31 - 59 - 53 - 53 - 44 - 35 - 44 - 45 - 14 - 15 - 14 - 15	.15 11 26 41 57 54 35 35 35 35 35 35 35 35	.44 .19 0 19 43 20 08 01 05	.60 .39 .20 .04 21 34 14 05 01	.68 .54 .16 06 23 14 09 06 03



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TABLE XIII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.80; R = 1,000,000; PROPELLERS REMOVED - Continued (a) $\alpha_{\rm U}$ = -2°, 0°, 2°, 4°, 6°, 8° - Concluded

	Per-			Upper	surface							surface		
Spanwise	cent			Angle o	f attack			l				f attack		
stations	chord	-2°	00	2°	40	6⁰	80	[-20	00	2°	40	6°	8º
0.56 b/2	0 1.5 4.0 10.0 15.0 20.0 30.0 50.0 50.0 50.0 90.0	0.21 .31 .09 .05 .14 .21 .25 .25 .25 .25 .25	0.35 .19 .09 .29 .35 .35 .36 .35 .26 .24 .24 .04	0 - 14 48 514 4 55 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	0.54 - 38 - 57 - 81 - 81 - 51 - 326 - 183 - 183	0.49 66 85 94 -1.01 -1.14 -1.02 60 45 30 21 05	0.41 89 -1.04 -1.09 -1.15 -1.26 -1.20 -1.15 57 50 42 36 28 13 05		-0.69 90 95 83 83 39 31 18 06 09	-0.51 75 75 66 57 45 35 29 17 05	-0.06 31 37 38 38 24 21 11	0.24 01 13 16 15 11 12 11	0.43 .20 .20 .01 .01 .04 .04 .05 .05	0.5h .29 .1h .07 .04 .01 0 01
0.68 b/2	0 1.5 10.0 10.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	06 .50 .25 .31 .02 14 20 22 21 19 15 13	.13 .39 .05 .14 .22 .27 .31 .31 .24 .21 .21	. 46 .13 .21 .35 .43 .46 .50 .51 .44 .39 .35 .20 .15	.58 -259 -83 -78 -75 -69 -75 -39 -31 -24 -15 -102	.52 64 95 -1.11 -1.09 -1.07 74 30 11 30 11 30	. 11 86 -1.12 -1.05 -1.05 -1.03 99 81 66 56 46 37 30 21		-1.15 -1.21 -1.11 -1.05 66 41 25 07 02 .05 .09	90 -1.02 86 71 50 32 22 07 .01 .08 .10	21 36 35 35 37 17 01 04 09 11	.23 .01 10 14 12 11 06 03 .10 .11	.42 .23 01 .01 0 .03 .03 .10 .10	.52 .33 .18 .10 .08 .05 .05 .05 .05 .06 .09 .03 .03
o.84 ъ/2	0 1.5 4.0 7.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	.19 .50 .30 .16 .08 03 08 17 17 17 15 19 09	.35 .12 .17 .04 09 15 21 22 24 19 16 11	.60 .12 -13 -27 -35 -41 -44 -37 -34 -28 -25 -15 -01	.62 29 51 66 70 66 56 51 45 30 21 13 .01	. \$7 74 89 -1.06 97 94 97 38 29 10 .01	.33 -1.00 -1.17 -1.18 -1.11 -1.06 -1.06 99 72 55 34 24 12		89 82 73 66 54 31 21 11 05	-1.02 91 68 42 27 11 04 .02 .07 .10	26 36 31 26 19 04 0 .04 .09	.21 .01 10 06 06	.43 .24 .06 .03 .01 .04 .06 .06 .10	.53 .35 .18 .10 .10 .05 .05 .08 .09 .10
0.9 4 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	.05 .50 .35 .20 .11 .03 05 12 16 18 15 11	.12 .14 .26 .12 .02 06 12 19 20 16 11 11	.47 .20 .01 14 24 29 33 34 26 21 16 .05 .11	.63 15 34 45 51 51 52 45 40 34 26 15 08	-54 -62 -76 -88 -92 -81 -76 -68 -40 -31 -24 -08 -03	.43 -1.00 -1.05 -1.03 96 96 99 49 31 22 14 06		54 53 50 45 41 38 36 26 20 15	99 91 85 63 46 34 19 09 09	- 52 - 39 - 35 - 29 - 22 - 09 - 02 - 06 - 10 - 12 - 11	.061013141210060307111214	.36 .11 .05 .01 .03 .01 .05 .03 .01 .05 .03 .13 .11	.48 .23 .15 .09 .03 .02 .03 .03 .07

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TABLE XIII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.80; R = 1,000,000; PROPELLERS REMOVED - Continued (b) α_u = 10°, 12°, 14°, 16°, 18°, 20°

	Per-			Upper	surface						Lower	surface		
Spanwise stations	cent chord	100	120	Angle o	f attack	180	20°	1	10°	12°	Angle o	f attack	180	200
о.10 ъ/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	0.19 -1.00 -1.04 -1.15 -1.10 -1.08 -1.00 -95 -66 -70 -43 -25 -20	0.39 -1.20 -1.26 -1.34 -1.26 -1.29 -1.11 94 71 75 75 75 38 38	0.26 -1.36 -1.50 -1.41 -1.43 -1.22 -1.07 86 81 76 55	0.14 -1.43 -1.43 -1.36 -1.30 -1.24 -1.16 -1.06 -1.00 93 89 81 66	0.01 -1.40 -1.38 -1.34 -1.29 -1.26 -1.21 -1.16 -1.11 -1.05 -1.00 91 76	-0.11 -1.41 -1.40 -1.36 -1.36 -1.39 -1.25 -1.25 -1.25 -1.26 -1.09 -1.03 94 82		0.74 .54 .35 .27 .23 .16 .09 .07	0.81 .65 .37 .32 .24 .18 .11 .11	0.85 .72 .53 .43 .39 .29 .24 .18 .11 .13	.61 .52 .45 .36 .25 .20 .18	0.92 .86 .57 .52 .42 .29 .24 .20	20 0.93 .91 .62 .56 .46 .40 .34 .27 .25
0.19 5/2	0 1100 0 1100 0 1100 0 0 0 0 0 0 0 0 0 0	.28 -1.18 -1.27 -1.20 -1.10 -1.10 -1.10 36 30	01 -1.25 -1.22 -1.05 -1.06 -1.06 -1.04 -1.04 -1.04 -1.04	21 -1.25 -1.25 -1.04 -1.03 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05 -1.05	-37 -1.21 -1.20 -1.04 -1.04 -1.01 -1.01 -1.01 -78 -78 -78	-57 -1.14 -1.13 -1.09 -1.10 -1.11 -1.11 -1.12 -1.00 89 85 85	76 -1.15 -1.12 -1.13 -1.13 -1.16 -1.17 -1.0591898078			.76 .74 .57 .39 .16 .03 .03 .03	.75 .19 .64 .26 .26 .10 .05 .04 .01	.74 .84 .73 .77 .37 .19 .11 .04 .04	.69 .86 .45 .25 .17 .08 .05	.65 .87 .87 .71 .73 .31 .22 .10 .06
0.31 þ/2	0 1.5 4.0 70.0 15.0 20.0 30.0 40.0 50.0 60.0 90.0	.36 -1.00 -1.36 -1.32 -1.38 -1.38 -1.30 -1.14 -1.00 55 55 24	.26 -1.12 -1.21 -1.18 -1.17 -1.16 -1.12 -1.00 81 55 55 43	.14 -1.16 -1.13 -1.06 -1.06 -1.06 -1.04 98 77 60 50	.556.64.4.9.538.58.68.55.55.55.55.55.55.55.55.55.55.55.55.55	09 -1.00 98 -1.01 84 80 79 76 71 70 65	16 -1.06 -1.00 94 92 86 81 79 75 75 75 68		.659 .30 at B. 11 .06 .06 .06 .13	.73 .79 .39 .31 .25 .18 .11 .06	.76 .66 .38 .34 .15 .10	.80 .73 .56 .47 .41 .31 .23 .15 .02	.81 .80 .64 .53 .46 .36 .26 .20 .09	.84 .85 .69 .59 .54 .33 .34 .25
0.375 b/2	0 1.5 1.0 10.0 15.0 20.0 30.0 70.0 70.0 70.0 70.0 70.0	22 -1.16 -1.16 -1.10 -1.05 -1.00 -1.05 -1.	8958848	9886566 86686	2 F F F F F F F F F F F F F F F F F F F	- 35 - 72 - 70 - 70 - 70 - 70 - 70 - 70 - 68 - 69 - 68 - 68	-51 -74 -74 -72 -72 -72 -72 -72 -71 -71 -70 -70 -70 -70 -70 -70 -70 -70 -70 -70		61.9 82.158 88.178	.66 .56 .59 .29 .23 .12 .06 06	୍ଟ୍ରେମ୍ବର ଜୁନ୍ନ ଅନ୍ତର୍ଶ୍ୱର	.66 .66 .51 .41 .34 .23 .14 .01	.66 .70 .58 .48 .12 .29 .21 .05 .02 .22	.63 .71 .61 .54 .46 .34 .26
0.44 5/2	0 1.5 7.0 15.0 20.0 20.0 50.0 70.0 80.0 95.0	15.808.88.74.75.888.75.44 1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.	5,16,16,6,6,6,6,6,6,6,6,6,6,6,6,6,6,6,6,	15988888888888	୬ ୬ ୬ ୬ ୬ ୬ ୬ ୬ ୭ ୬ ୭ ୬ ୭ ୭ ୭ ୭ ୭	- 43 - 65 - 65 - 65 - 65 - 65 - 65 - 65 - 65			.88 .54 .65 .65 .65 .65 .65 .65 .65 .65 .65 .65	.70 .68 .39 .14 .09 .106 .106		.66 .74 .65 .49 .305 .05 .00 .110	.64 .80 .72 .77 .39 .20 .02 .02 .08	.78 .80 .76 .63 .46 .90 .01 .06 .06 .06

TABLE XIII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.80; R = 1,000,000; PROPELLERS REMOVED - Concluded (b) $\alpha_{\rm u}$ = 10°, 12°, 14°, 16°, 18°, 20° - Concluded

· · · · · · ·	Per-			Upper	surface			П			Lower	surface		
Spanwise	cent				f attack						Angle o	of attack		
stations	ohord 0	10° 0.34 -1.00	12° 0.25 -1.09	140 0.15 -1.20	16° 0.05 -1.30	-0.06 -1.46	20° -0.20 -1.52	\vdash	10° 0.59	12°	14° 0,69	16°	18° 0.75	20°
0.56 b/2	1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 90.0 95.0	-1.00 -1.20 -1.23 -1.24 -1.31 -1.24 -1.16 62 49 43 30 17	-1.09 -1.31 -1.35 -1.31 -1.28 -1.05 64 42 37 34 24	-1.20 -1.47 -1.47 -1.42 -1.42 -1.37 -1.07 69 55 47 41 34	-1.30 -1.51 -1.48 -1.50 -1.45 -1.16 82 65 54 54 39	-1.46 -1.55 -1.55 -1.55 -1.56 -1.30 -1.01 84 63 50 44	-1.57 -1.54 -1.53 -1.53 -1.50 -1.35 -1.20 -1.04 58 49			.47 -29 .22 .18 .13 .09 .05 01	.36 .27 .24 .16 .12 .08		.69 51 .43 .37 .29 .21 .15 05 .04 05	.56 .47 .42 .32 .24 .19 .08 .05
0.68 b/2	0 1.5 2.0 10.0 15.0 20.0 30.0 50.0 60.0 70.0 80.0 90.0 95.0	.30 -1.05 96 92 95 85 75 61 55 40 29 26	.20 96 -1.01 86 86 84 77 73 66 50 51	.07 87 91 83 81 76 75 77 67 57 57	06 98 98 88 88 88 69 69 45 45	21 94 97 93 95 99 86 876 74 62 45	35 97 -1.00 97 97 97 97 46 46		.57 .40 .15 .12 .07 .05 .04 .04	.60 .48 .30 .21 .18 .10 .09 .05 .04 .05	.59 .52 .35 .26 .19 .14 .09 .05 .02 0	.59 .54 .40 .29 .24 .16 .11 .05 .01 .01	.57 .57 .57 .35 .39 .19 .15 07 .03 01 15	.59 .59 .48 .40 .54 .25 .18 .09 .03 .03 .15 .28
0.84 b/2	0 1.5 4.0 7.0 10.0 20.0 20.0 40.0 50.0 60.0 70.0 80.0 90.0 95.0	.17 -1.18 -1.23 -1.16 -1.11 -1.12 -1.02 86 79 70 62 52 43 33 25	.04 -1.17 -1.17 -1.07 -1.09 -1.09 88 83 72 66 79 59	11 -1.13 -1.20 -1.10 -1.11 -1.05 -1.02 90 87 71 66 61 53 48	25 -1.11 -1.16 -1.09 -1.11 -1.04 -1.01 89 89 78 71 66 59 53	41 -1.07 -1.11 -1.05 -1.06 -1.01 -1.01 94 92 82 75 68 61	53 -1.05 -1.05 -1.00 -1.01 99 -1.00 94 95 85 76 71		.56 .39 .24 .15 .13 .08 .05 .05 .05 .05	.59 .59 .59 .30 .20 .18 .11 .07 .06 .06 .04	.79 .50 .34 .24 .20 .14 .07 .05 .04 .01 .06	.77 .54 .37 .29 .23 .16 .05 .05 .01	.50 .50 .50 .20 .33 .28 .19 .06 .04 .04	.55 .58 .36 .30 .22 .11 .06 .09 .04 .13
0.94 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	.29 -1.23 -1.11 -1.05 -1.06 -1.06 -1.00 80 67 56 49 39 29 20 15	.19 -1.10 -1.09 -1.01 -1.05 94 79 73 65 59 51 35 30	.05 -1.02 -1.09 98 -1.01 93 79 74 65 55 54 46	10 99 -1.09 95 -1.00 94 81 76 71 69 64 50	25 93 97 88 93 87 81 81 75 74 69 63	- 25 - 66 - 66 - 67 - 69 - 61 - 59 - 59 - 59 - 59 - 59 - 59 - 59 - 59		.51 -28 .19 .11 .08 .03 .01 0	.56 .34 .25 .16 .13 .06 .04 .01 .01	.577 .38 .29 .20 .14 .08 .04 .01 	.58 58 33 .24 .19 .10 .01 05 05 05 25	.577 .45 .377 .29 .13 .07 .02 	.97 .45 .38 .29 .22 .13 .05 .01 10



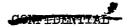


TABLE XIV.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING M = 0.90; R = 1,000,000; PROPELLERS REMOVED (a) α_u = -2°, 0°, 2°, 4°, 6°, 8°

Spenwise	Per-			Opper	surface f attack						Lower	surface of attack		
Stations	cent chord	-20	00	50	1º	6º	80	1	-20	6	20	A actaex	1 6º	80
0.10 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 50.0 60.0 70.0 80.0 95.0	0.53 .k3 .20 .06 008 1k 22 2h 31 31 34	0.63 .30 .09 -05 -24 -20 -24 -39 -47 -47 -47 -21 -09	0.70 .655 .066 .20 .25 .39 .41 .59 .59 .59	0.73 01 22 35 45 45 48 57 66	0.73 18 37 51 54 54 57 57 59 61 70 24	0.69 -149 -171 -68 -67 -66 -77 -66 -77 -66 -77 -86		-0.19 -39 -37 -35 -32 -36 -39 -22 -14	0.01 22 26 26 27 33 36 34 15	0.21 02 12 15 20 25 29 35 25	0.38 .14 .01 .03 .07 .11 .16 .24 .34 .26	0.51 .29 .14 .07 .04 .02 .07 -14 -17 09	0.64 .33 .25 .18 .14 .07 .01 .05 -01
0.19 5/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 50.0 60.0 70.0 80.0 95.0	.65 .44 .15 03 15 34 41 40 38 37 25 20	.73 .28 .017 .30 .505 .551 .551 .571 .333 .16	.76 .69 -31 -34 -45 -69 -70 -60 -61 -60 -61 -60 -60 -60 -60 -60 -60 -60 -60 -60 -60	115 8 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.67 .40 .67 .71 .75 .75 .75 .75 .75 .75 .75 .75	100 B B B B B B B B B B B B B B B B B B		17 34 41 50 48 43 46 51 46	.06 14 28 44 54 45 50 51 44	.29 .09 .09 .30 .355 .49 .50 .41 .27	145 25 06 16 168 188 0	.61 .41 .20 .02 .37 .65 .13 .02 0	.70 .55 .33 .11 .24 42 05 .01
0.31 b/2	0 1.5 1.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	538486853459845	- 45 - 16 - 13 - 25 - 33 - 45 - 53 - 59 - 59 - 59 - 59 - 59 - 59 - 59 - 59	50.00 M 1 1 7 7 8 8 8 7 7 7 8 8 8 7 7 7 8 8 8 7 7 7 8 8 8 7 7 7 8 8 8 7 7 8 8 7 7 8 8 8 7 7 8 8 8 7 8 7 8 8 8 8 7 8 7 8 8 8 8 7 8	\$ 14.55.55.55.55.55.55.55.55.55.55.55.55.55	.60 31 62 76 86 89 99 99 79 79 79 45	-55 -51 -79 -89 -91 -1.00 -1.00 -88 88 68 68		- 39 - 61 - 72 - 73 - 57 - 36 - 36 - 36 - 36 - 36 - 36 - 36 - 36	24 50 67 65 55 38 36 48	02 28 41 37 28 26 41	.18 20 18 27 20 20 34 16 06	.47 .15 .01 .05 .07 .11 .14 .25	.52 .31 .07 .05 .01 05 06
0.375 b/2	0 1.5 7.0 10.0 15.0 20.0 30.0 50.0 70.0 80.0 90.0 95.0	33617514 136 1 2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	\$ 23 - 20 - 20 - 20 - 20 - 20 - 20 - 20 - 20	.80 .30 .80 .89 .86 	& 21 - 25 - 66 - 67 - 81 - 79 - 24	.60 -47 -56 -71 -89 -94 89 76 66 57 43	- 52 - 72 - 81 - 99 - 93 - 91 - 80 - 73 - 66 - 66 - 67 - 57		53 77 84 76 74 51 15 15	30 -59 -56 -56 -56 -57 -7 -7 -7 -7 -7 -7 -7 -7 -7 -7 -7 -7 -7	.01 24 33 33 34 36 38 38	.26 .02 12 18 20 25 30 37 37	.44 .20 .04 .08 .14 .20 .36 .36	.55 .34 .16 .07 .02 .06 12 31 36
a.44 b/2	0 1.5 \$.0 7.0 10.0 15.0 20.0 30.0 \$0.0 70.0 60.0 70.0 80.0 95.0	% 51 000 2 1 1 0	8882-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1	.70 01 24 51 79 83 83 865 53 387 17	- 29 - 46 - 67 - 68 - 68 - 68 - 68 - 68 - 68 - 68 - 68	-63 -56 -67 -81 -75 -76 -66 -66 -66 -69 -44	.50 -77 -83 -76 -78 -79 -66 -67 -68 -64 -60 -59		-33 -61 -60 -66 -47 -35 -37 -40 -44 -39 -36	- 10 - 14 - 53 - 53 - 34 - 36 - 43 - 43 - 43 - 27	285 -151 -543 -543 -543 -543 -543 -543 -543 -543	.11 .16 .02 16 41 66 50 36 19	.17 0 25 67 46 11 01 16 26	.66 .48 .30 .13 .13 .49 .69 .30 .07 .05



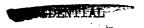


TABLE XIV.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.90; R = 1,000,000; PROPELLERS REMOVED - Continued (a) $\alpha_{\rm u}$ = -2°, 0°, 2°, 4°, 6°, 8° - Concluded

	Per-			Upper	surface					Lover	surface		
Spanwise stations	cent chord				fattack						of attack		
50501002	cnord	-20	œ	20	ĻΟ	€0	80	_2º	60	20	ħο	60	80
0.56 b/2	0 14 70000000000000000000000000000000000	0.26 .25 .01 .25 .34 .37 .37 .37 .37 .37 .37 .37 .37 .37 .37	0.35 .15 .15 .15 .15 .15 .15 .15 .15 .15 .1	\$ 54,838,8548,85158	577456588582888856	0.45 396 1.78 598 2.55 1.75 1.75 1.75 1.75 1.75 1.75 1.75 1	0.51 51 69 77 85 98 -1.01 -1.02 -1.02 -1.55 15 16 13	-0.55 74 84 66 57 53 36 05 01	-0.40 64 75 56 56 23 06 01	-0.09 -37 49 36 33 26 26 12	0.16	0.18 06 20 24 21 22 23 22 15 14	0.129 0.129 0.12866 0.16866 0.16866 0.16866
o.68 b/2	0 1.5 7.0 15.0 15.0 20.0 20.0 50.0 70.0 80.0 95.0	.10 .457 .17 .02 09 17 24 30 29 24 20 16	.25 .32 .01 -16 -26 -33 -40 -45 -41 -35 -30 -18 -12	.51 .15 .36 .47 .561 .64 .78 .23 .17 .04	864364658339100	.49 -29 -61 -75 -75 -75 -75 -75 -75 -33 -36 -33 -36		79 94 95 89 64 20 31 14	77 79 87 80 76 68 14 02 03 10 12	24 47 49 48 41 33 18 02 .03 .10 .12	.10 -113 -22 -26 -23 -119 -122 -122 -122 -124 -125 -126 -126 -126 -126 -126 -126 -126 -126	.26 .05 09 14 13 14 11 05 01 06	- 141 - 20 - 05 - 05 - 05 - 05 - 05 - 05 - 05 - 0
o.8o b/2	0 1.5 4.0 10.0 15.0 20.0 20.0 50.0 70.0 80.0 90.0	.32 .50 .29 .15 .05 05 12 18 20 21 19 14 13 11	.47 .38 .14 02 29 29 29 29 29 20 20 20 20	.61 .16 .25 .25 .35 .35 .35 .33 .33 .33 .33 .33 .33	63 1 33 9 5 6 6 7 6 5 5 8 1 4 6 5 8 6 5 8 1 4 6 5 8 6 5 8 1 4 6 5 8 6 5 8 1 4 6 5 8 6 5 6 5	.58 -37 -57 -77 -86 -85 -89 -79 -71 -50 -31 -10	. 49 61 78 67 64 58 58 58 53 43 43 23	69 60 59 57 46 36 29 24 11	72 79 58 58 27 10 03 .02 .07	28 44 43 38 32 25 01 01 01 10	.11 11 19 20 16 11 04 .01		.%1 .20 .04 .01 .02 05 01 .01 .04 .05 .04
0.94 b/2	0 1.5 4.0 70.0 15.0 20.0 30.0 50.0 50.0 60.0 90.0	.20 .51 .35 .21 .10 .01 05 16 20 26 21 19 15	.28 .12 .24 .09 02 11 18 25 26 27 17 17 17	\$\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	.63 63 63 63 63 63 63 63 63 63 63 63 63 6	.60 .31 .49 .67 .74 .667 .667 .461 .31 .30	.55 59 69 79 81 75 61 51 43 36 31	40 30 36 36 31 27 30 25 25 29 19	88 78 80 70 65 32 18 10	- 57 - 48 - 45 - 40 - 35 - 26 - 29 - 03 - 03 - 13 - 16 - 18	0 15 19 20 16 12 09 06	.24 .02 .05 01 08 09 06 04	.37 .04 01 04 06 07 06 01 .01

Constitution of the same



TABLE XIV.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.90; R = 1,000,000; PROPELLERS REMOVED - Continued (b) $\alpha_{\rm u}$ = 10.

<u> </u>	Per-		 Upper	surface				Lover	surface		
Spanwise stations	cent chord		 Angle	f attack				Angle	of attack	,	
0.10 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	10° 0.61665889818171748549				10° 0.73 .72 -35 .27 .22 .14 .09 .04 .01 .030713					
0.19 6/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 90.0 95.0	.39 84 -1.11 -1.16 -1.17 -1.27 -1.27 -1.11 95 66 41 30				.74 .64 .24 .08 14 05 03 01	•				
0.31 6/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 \$0.0 \$0.0 70.0 90.0 95.0	.49 67 96 -1.04 -1.01 98 96 95 85 84 77 67				.62 .43 .25 .17 .14 .09 .02 03 16					
0.375 b/2	0 1.5 1.0 15.0 15.0 15.0 15.0 15.0 15.0	.39 99 91 91 91 91 74 70 667 64				.63 .45 .27 .18 .11 .04 05 24 26					
0.14 b/2	0 1.5 2.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 90.0 95.0	3995 				.72 .79 .44 .25 .01 37 70 14 12 11					

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TABLE XIV.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.90; R = 1,000,000; PROPELLERS REMOVED - Concluded (b) $\alpha_u = 10^{\circ}$ - Concluded

	Per-		Upper s	urface .			Lower	aurface	
Spanwise stations	cent		Angle of	attack			Angle o	of attack	
B CE C LOUIS	chord	100				10°			
0.56 b/2	%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%	0.47 65 92 97 -1.08 -1.09 -1.06 -1.05 -1.00 82 65 39 39				0.52 .30 .05 .06 .04 -01 -09 -08 -14 -10			
0.68 b/2	0 1.5 7.0 10.0 15.0 20.0 30.0 \$0.0 70.0 70.0 90.0 90.0	- 44 - 69 - 91 - 83 - 83 - 83 - 81 - 75 - 66 - 50 - 50 - 49							
о.80 ъ/2	0 1.5 *.0 7.0 10.0 20.0 20.0 \$0.0 \$0.0 \$0.0 \$0.0 \$0.0 \$.37 79 96 -1.04 -1.07 -1.01 -1.00 94 81 69 57 54 42							
0.94 b/2	0 1.5 4.0 7.0 15.0 20.0 30.0 50.0 50.0 50.0 90.0 95.0	.44 85 87 81 84 79 72 66 61 56 49 37							



TABLE XV.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.165; R = 8,000,000; PROPELLERS REMOVED

(a) $\alpha_u = -2^\circ$, 0° , 2° , 4° , 6° , 8°

Spenwise	Per-			Upper	surface						Buriace		
stations	cent chord	-2°	O ^O	2º	d attack	60	T 6°	_e°	00	Angue o	f attack	_6°_	8°
0.10 b/2	0 1.55 4.0 7.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	48488845994559468	0 0 1951 1950 1950 1950 1950 1950 1950 1	**************************************	Kn499944978895	0.43 69 69 69 69 69 59 59 59	0 17 -1.09 -1.98 -1.98 -1.59 -1.59 -1.51 -1.43 -1.23 -1.08 -1.08	1 666 A 94 886 88 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	ର ଜଣ ଅନ୍ୟୁଷ୍ଟ ଅନ୍ତ । ସ୍ଥ ବିନ୍ନ୍ନ ଜଣ ଜଣ ଜଣ ଜଣ ଜଣ	87 98994498 8	138 589 1885 88	0.48 .27 .27 .06 .04 0	0.60 .43 .268 .45 .09 .06 .06 .06
0.19 b/2	0 1.5 7.0 15.0 20.0 30.0 \$0.0 \$0.0 \$0.0 \$0.0 \$0.0 \$0.0 \$	89.44.6.1.9 1.0.0.0.9.9.4.8.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0	47.0008 NAHWANA0000	25 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	51.58666682 1934 FT FL 65.007	-17 -1-102 -1-102 -1-103 -1-10	-1.73 -1.73 -1.66 -1.66 -1.55 -1.75	58 4825H 95 8	ଅଧି ଅନ୍ୟୁକ୍ଷ ଓଡ଼ିଶ୍ (ଞ୍ଜ ଅନ୍ତର ଅ	ହମ୍ମ ଅନ୍ତର୍ଥ । ଅଧି	579 95505 11 95505 11 90 0	.62 .55 .36 .30 .00 .03 .03 .06
0. <u>31</u> b/2	0 1.5 2.0 7.0 15.0 20.0 20.0 40.0 50.0 60.0 70.0 80.0 95.0	01.36 	338883289393742176 	\$138\$	5,460 660 595 45 593 4 29 21 5 	391 - 88 - 76 99 8 - 753 - 731 218 001		884 88554774 8 88	150 4333324 11-3433324 11-348	26 27 5 21 28 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	0 04	147.88 19.04.0 0.03 1.04.0 0.0	
0.375 b/2	0 1.5 4.0 7.0 15.0 20.0 30.0 40.0 50.0 70.0 80.0 95.0	142.8663.15 2.29.7.134.63	.26 .25 .02 26 29 27 24 29 24 30 30	2388848 1288848 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-51 56 60 63 58 38 38 39 26 19 05	.23 -1.12 94 98 88 72 36 29 36 20 06	-32 -1.80 -1.34 -1.22 -1.11 97 87 50 40 31 22 30 32	-1.06 -54 -54 -33 -18 -10	- 49 - 53 - 45 - 45 - 38 - 38 - 38 - 38 - 38 - 38 - 38 - 38	-03 -19 -23 -25 -23 -21 -17 -09 -04	30 50 10 10 10 10 10 10 10 10 10 10 10 10 10	.50 .30 .06 .02 01 01 01 .03 .05	.57 .46 -27 .19 .14 .08 .07 06 .07
0.44 6/2	0 1.5 4.0 7.0 15.0 20.0 30.0 50.0 60.0 70.0 90.0 95.0	14888444444444444444444444444444444444	.35 .20 018 23 32 34 35 24 24 24 24 24	57933645 77933645 77745 7777 7777 7777 7777 7777 7777	-51 66 66 53 53 53 53 53 53	.10 -1.33 -1.04 84 75 52 36 36 36 36	64 14 14 14 16 17 16 16 16 16 16 16 16 16 16 16 16 16 16	-1.08 -1.08	-53 -61 -54 -56 -56 -56 -28 -17 -09 -03	.05 -19 -32 -37 -30 -25 -37 -30 -20 -12 -05 0	.49 .15 0 11 -19 -13 -07 -08 .02	.59 .41 .09 01 07 02 0	्रेड्ड इ.स. १५८६१५५५५५५५५५५५५५५५५५५५५५५५५५५५५५५५५५५

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TABLE XV.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.165; R = 8,000,000; PROPELLERS REMOVED - Continued (a) α_u = -2°, 0°, 2°, 4°, 6°, 8° - Concluded

J	Per-			Upper	surface					Lover	surface		
Spanvise stations	cent			Angle o	of attack					Angle (f attack		
SCRC1ORS	chord	_2°	00	20	40	60	8º	~50	00	20	ŧο	6º	80
0 .5 6 b/2	0 1.50 70.00 15.00 150.	9.22 .37 .64 .64 .19 .117 .141 .131 .131 .133	0.22 19 19 24 25 23 24 23 24 23 24 23 23 24 25 23 24 23 24 23 24 23 24 23 24 23 24 23 24 23 24 23 24 23 24 23 24 23 24 23 24 25 25 25 25 25 25 25 25	0.45 0.08 0.08 0.08 0.08 0.08 0.08 0.08 0.0	0.05 PEGENT 1.00 PEGENT 1.	0.27 94 91 88 88 73 63 56 42 38 38 38 38 38	0.17 0.19 11	1000 1000 1000 1000 1000 1000 1000 100	-0.54 -57 -59 -38 -38 -35 -20 -125 -01	-0.11 -26 -29 -27 -24 -20 -17 -1* -08 -02	ଅଧିକଥିଲି । ଅଧିକଥିଲେ ।	0.67 .25 .03 .03 .04 .05	0.59 .42 .23 .16 .13 .09 .07 .05 .05
0.68 b/2	0 1.5 7.0 10.0 15.0 15.0 15.0 15.0 15.0 15.0 15	\$\$\$\$\$\$\$\$\$#########\$\$\$\$	ង្គៈ	8788833338649755 1111111115	**************************************	\$	5.34.28.56.56.56.56.56.56.56.56.56.56.56.56.56.	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	14 2 8 2 1 1 5 5 5 5 8 8 8 8 8 8 8 8 8 8 8 8 8 8	ଅଷ୍ଟ ଅଷ୍ଟ୍ରମଣ ଅନ୍ତର	ୀଟ୍ଟ୍ରିଡେଖିଶିଖି ଅନ୍ତର୍ଚ୍ଚ	1.500000 0000000000000000000000000000000	.54 .42 .26 .18 .15 .11 .10 .11 .11
0.80 b/2	0 1.5 4.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 90.0 95.0	388456 6248888	87.488477 (99748888) 111111111111111111111111111111111	କ୍ଷ୍ୟୁ ମଧ୍ୟର ବ୍ୟୁ ଅନ୍ତର ଜଣ୍ଡ ମଧ୍ୟର ବ୍ୟୁ ଅନ୍ତର	98848864 85554888	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-32 -1.49 -1.15 -1.03 81 81 51 34 26 17 03	15.6 85.4 % 485.8 88.8 88.8 88.8 88.8 88.8 88.8 88.	888 1738 20 115 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	ស្រង្គម្លាស់ ១៩៩៨	नुष्ठ ६५६४	4 ଜ ମ୪ ୫୯ ୭୪ ୧୫୫ ୧	.555 .42 .34 .17 .15 .11 .10 .10 .10
0.9h b/2	0 1.5 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0	1 0 1 5 0 1 0 0 1 0 0 0 0 0 0 0 0 0 0 0	15 4 % 7 7 7 7 7 7 8 8 8 7 8 8 8 7 8 8 8 8 8	.36 .19 0 -11 -15 -17 -15 -19 -17 -19 -17 -18 -18 -18 -18 -18 -18 -18 -18 -18 -18	54 -19835486 -1864-1866 -1864 -1864-1866 -1864 -1864-186 -1864-186 -1864-186 -1864-186 -1864 -1864-186 -1864 -	. 59 . 63 . 63 . 63 . 63 . 63 . 63 . 63 . 63	195585558 105581 10558558 10568 10568 1056858 105686 1056858 1	625 4 1 1 1 0 0 0 0 0 0 0	-1.10 -57 -49 -39 -30 -21 -14 -07	1.30 1.30 1.30 1.30 1.30 1.30 1.30 1.30	0 004 000 000 0000	33 1120 200 200 200 200 200 200 200 200 20	.51 .25 .19 .12 .06 .05 .06 .06 .07



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TABLE XV.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.165; R = 8,000,000; PROPELLERS REMOVED - Continued (b) α_u = 10°, 12°, 14°, 16°, 18°, 20°

	Per-			Upper	surface					Lower	surface		
Spanwise stations	cent		,	Angle o	f attack						f attack		
0.10 ъ/2	0 1.5 4.0 7.0 10.0 20.0 30.0 50.0 60.0 70.0 80.0 90.0	10° -0.25 -1.58 -1.35 -1.35 -1.39 -1.46 -1.38 -1.46 -1.38 -1.46 -1.38 -1.46 -1.38 -1.46 -1.38 -1	12° -0.78 -1.43 -1.43 -1.43 -1.55 -1.43 -1.55 -1.53 -1.53 -1.53 -1.55 -1	14°	16° -9.16 -9.37 -1.61 -1.33 -1.9054 -1.349054 -1.349054	18° -2.82 -3.68 -2.69 -1.73 -1.42 -3.69 -3.69 -3.69 -3.4 -3.4 -3.4 -3.4 -3.4 -3.4 -3.4 -3.4	80° 7.3337.845.7588.835.83	10° 0.65 .55 .36 .29 .24 .17 .14 .19 .11	28°	14° 0.59 .70 .56 .46 .32 .27 .23 .20 .20 .20 .20	.60 .74 .53 .53 .47 .37 .38 .25 .23 .25	18° 0.40 .77 .68 .58 .54 .34 .24	20°
0.19 6/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 90.0 95.0	1.25 -4.15 -4.34 -1.34 -1.56 -	-2.30 -3.26 -2.27 -1.79 -1.28 -1.59 -1.33 -1.68 -1.33 -1.06 -1.05	7-15-5-1-82-1-1-5-5-1-1-1-5-5-1-1-1-5-5-1-1-1-5-5-1-1-1-5-5-1-1-1-5-5-1-1-1-5-5-1-1-1-5-5-1-1-1-5-5-1-1-1-5-5-1-1-1-5-5-1-1-1-5-5-1-1-1-5-5-1-1-1-5-5-1-1-1-1-5-1	-5.80 -5.20 -5.40 -1.55 - 93 - 5.56 - 29 - 1.55 - 1.56 - 1	+2379796666 +217966666 +1179677677	98 11 55 5 5 8 8 1 1 1 1 1 1 1 1 1 1 1 1	.54 .63 .51 .36 .22 .19 .07	.66 .48 .75 .19 .13 .09 .11		25 56 55 8 1 1 1 1 6 6	-25 -58 -79 -70 -51 -31 -21 -17 -17 -02	29 .57 .81 .74 .82 .31 .16 .19 .60
0.31 b/2	0 1.5 4.0 7.0 15.0 20.0 20.0 40.0 50.0 60.0 90.0 95.0		10.00 10.00	*555125585888888888888888888888888888888	######################################	-1.97 -1.66 -3.12 -2.53 -1.70 -1.39 98 -7.60 -1.39 50 -1.30 -1	15.18 12.16	.61 .57 .37 .29 .18 .19 .06 .06 .06	- 156 - 156	.17 .19 .17 .17 .10 .19	WE ESSIVE 9 906	.19 .70 .56 .46 .36 .30	05 68 76 69 61 34 21 03
0.375 b/2	0 1.5 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	4888220 8423888 444444 11111	134481238 12848388 474777 11110	848 848 85 85 85 85 85 85 85 85 85 85 85 85 85	75774468 8882848 7577444 11111	5577443460398 80391284435	-6.03 -5.09 -2.96 -2.96 -2.96 -1.52 -1.52 -1.23 -1.94 76 76 39	.53 .55 .43 .25 .17 .11 .11 .11 .99 .68			156 85588 N. 17 188	.34 .53 .66 .59 .53 .42 .34 .21 .21 .21	-53 .50 .68 .63 .57 .37 .23 .17
0. 4 4 b/2	0 1.5 1.0 7.0 15.0 15.0 340.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0 7.0	7980774158873848860	73447771 ((() () () () () () () () (\$518\$18\$\$\$6\$\$\$860 \$479444411111111	**************************************	717534 114534 1146 1146 1166 1166 1166 1166 1166 11	73.63 74.41 74.43 74.83 74.80	24 88884884 88	.08 .64 .53 .42 .25 .14 .14 .12 .05	និទ្ធ ដៃមិនិធម៌ និស្ស មិនិធម៌ និស្ស និស្ស និស និស្ស និស្ស និស និស្ស និស	ង ខ្លាំង	-28 -59 -76 -57 -57 -57 -57 -57 -119 -107 -13	-,41 -,56 -,78 -,71 -,61 -,41 -,27 -,14 -,10 -,08 -,15

A THE RELATION



TABLE XV.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.165; R = 8,000,000; PROPELLERS REMOVED - Concluded (b) $\alpha_{\rm u}$ = 10°, 12°, 14°, 16°, 18°, 20° - Concluded

	Per-			Upper	aurface			_			Lover	surface		
Spanwise stations	cent chord			Angle		·		Ì				fattack		
0.56 6/2	0 1.5 4.0 7.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 90.0 95.0	90 90 90 90 91 91 91 91 91 91 91 91 91 91 91 91 91	9 19558888755885	-2.63 -3.74 -2.62 -2.18 -1.52 -1.52 -1.62 -1.63	16° -3.33 -4.27 -2.27 -1.56 -1.56 -1.56 -1.56 -1.56 -1.56	80 714494111111118	20° -4.71 -4.80 -3.54 -2.54 -2.65 -1.33 99 77 61 48 38 29 19		00 0.61 .55 .57 .37 .28 .18 .15 .11 .11 .08	150 0.58 190 190 190 191 191 191 191 191 191 191	140 0.39 .68 .59 .50 .43 .35 .24 .16 .11	160 0.0	18°	20°
0.68 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 90.0	886749878887 11111111111111111111111111111111	2.33 -3.43 -3.55 -1.55 -	7.7744444411111111111111111111111111111	99.637.5.4.7.4.68888.8.196.05	55867888817848824 	7.33 75.95 74.55 74.55 74.75 7		.53 .53 .37 .28 .25 .19 .16 .15 .14 .13	386 56 386 386 386 386 386 311 386 311 386	.08 .57 .52 .44 .39 .31 .27 .21 .18 .18	20 53 56 443 35 30 411 66	- 50 .46 .46 .40 .33 .25 .21 .17 .10	67 .37 .59 .51 .43 .36 27 .22 .17
0.80 b/2	0 1.5 1.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 99.0	-1.24 -2.27 -1.62 -1.03 89 58 38 38 02 02	-2.45 -3.05 -2.15 -1.76 -1.28 -1.09 - 53 - 109 - 109 - 109 - 109 - 109 - 109 - 109	-3.92 -3.87 -2.67 -2.64 -4.47 -1.22 -73 -24 -24 -04	5.27 -4.69 -2.65 -1.63 -1.76 769 26 108 06	-6.72 -5.35 -3.50 -2.78 -1.44 58 26 18 12	5536688655 12988 F554 55 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		.56 .52 .36 .27 .24 .18 .14 .13 .14 .13	. Ag . 555 - 142 . 36 . 31 . 25 - 17 . 16 . 15 . 13 . 11	.19 .57 50 .43 .37 .30 19 .19 .17 .10	09 .53 55 .48 .43 .35 25 .22 .19 .11	-, 11 , 146 , 51 , 146 , 38 , 27 , 24 , 20 , 16 , 10 , 06	- 19 54 60 54 39 27 23 18 04 03
0.94 1/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 50.0 50.0 60.0 70.0 90.0 95.0	61 -1.62 -1.34 -2.43 -1.00 84 67 46 39 39 30 22 12	-1.61 -2.28 -1.81 -1.28 -1.04 85 53 32 23 23 01	-2.88 -3.02 -2.27 -1.83 -1.51 -1.21 97 45 34 23 11 01	-4.17 -3.67 -2.69 -2.14 -1.36 -1.09 -62 -47 -33 -21 -03 02	-5.61 -4.36 -3.09 -4.41 -1.93 -1.50 -1.21 65 48 33 20 12 09 08	\$\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\		.56 .37 .28 .21 .17 .12 .10 .09 	.52 - 45 .38 .30 .25 .17 .12 09 .08 .07	.33 .51 .42 .37 .30 .21 .16 .14	.11 	18 57 .54 .46 .40 .30 .22 .17 10 .06 .03 01	

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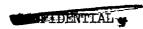


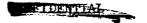
TABLE XVI.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.80; R = 2,000,000; PROPELLERS REMOVED (a) $\alpha_{\rm u}$ = -2°, 0°, 2°, 4°, 6°, 8°

B	Per-			Upper	r surface			٦				surface		
Spanwise stations	cent				of attack			1				f attack		- 00
0.10 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0 95.0	-2° 0.42 .39 .16 .0305131925262626262626	0° 0.55 .24 .01 12 39 34 35 35 35 31 29 24 08	2° 0.64 06 19 34 39 45 45 43 35 35 35 35 36 36	0.67 16 36 54 55 55 57 57 57 57 57 57	60 0.65 60 60 60 60 60 60 60 60	8° 0.5870829786848678763639		-0.353 -5.53	0 0 0 10 13 13 13 13 13 13 13 13 13 13 13 13 13	្ត ១. 1. ១ ១. ១. ១. ១. ១. ១. ១. ១. ១. ១. ១. ១. ១. ១	34 0.34 1.036 1.036 1.151 1.04 1.05 1.05 1.05 1.05 1.05 1.05 1.05 1.05	0.50 .38 .03 .03 .02 .05 .04	8° - 3° - 4° - 5° - 5° - 5° - 5° - 5° - 5° - 5
0.19 b/2	0 1.5 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 90.0 95.0	%	65 22 25 25 25 25 25 25 25 25 25 25 25 25	- 60 - 78 - 60 - 78 - 55 - 44 - 37 - 37 - 37 - 37 - 37 - 37 - 37 - 37	88 kacanaa, 88aasa	.53 -737 -999 -1.04 -1.03 -997 -634 -364 -364 -364 -364 -364 -364 -364	. 1.22 -1.33 -1.32 -1.45		96 (सर्व (सर्व ५८) ।	09 28 59 59 51 59 51 59	89 89 854 88 88	ំ ខ្មែរ មួស ១ ខ្មែរ ខ្មាំ ខ្មែរ ខ្មារ ខ្មែរ ខ្មារ ខ្មែរ ខ្មាំ ខ្មាំ ខ្មែរ ខ្មែរ ខ្មាំ ខ្មែរ ខ្មែរ ខ្មែរ ខ្មែរ ខ្មែរ ខ្ម	.59 .40 .17 .36 .36 .80 .09	ទំ ខ្មែន ទំព័ត្ធមាន
0.31 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 50.0 50.0 50.0 95.0	888511886118851888888888888888888888888	44 - 16 - 26 - 34 - 44 - 45 - 39 - 35 - 30 - 20 - 20	\$5%\$	535 - 67 - 781 - 87 - 884 - 19 - 35 - 20 - 20 - 20 - 20 - 20 - 20 - 20 - 20	2.64 05 -1.05 -1.16 -1.19 -1.35 -1	- 57 -1.18 -1.28 -1.36 -1.36 -1.37 -1.30 -1.37 -1.30 -1.37 -1.30 -1.37 -1.37		- 58 - 81 - 90 - 78 - 79 - 79 - 79 - 38 - 24 - 100	- 31 - 54 - 56 - 50 - 45 - 37 - 34 - 25 10 - 01	23 30 31 30 27 27 26 21	.26 .03 .11 .15 .15 .15 .16 .17	.44 .24 .06 .01 .01 .04 .06 .08	. 58 .39 .20 .13 .10 .05 .01 .02 .07
0.375 b/2	0 1.5 1.0 10.0 15.0 20.0 20.0 50.0 50.0 70.0 80.0 95.0	.23 .39 .16 .23 .23 .30 .37 .37 .39 .37	- 45 - 22 - 03 - 21 - 30 - 45 - 45 - 36 - 36 - 30 - 28 - 30	588398865 G535131666	- 59 - 47 - 61 - 88 - 97 - 99 - 69 - 69 - 69 - 69 - 69 - 69 - 69	-50 -91 -90 -1.06 -1.19 -1.26 -1.26 -1.26 -36 -36	.35 -1.15 -1.27 -1.31 -1.29 -1.25 -1.25 84 71 63 56 56		80 -1.06 98 75 61 55 32 21 17	- 38 - 60 - 59 - 57 - 57 - 45 - 35 - 20 - 15 - 04 - 01	.01 -23 -34 -35 -35 -35 -35 -35 -06	.30 .06 .06 .15 .18 .21 .22 .15 .01	.49 .27 .09 .01 .03 .08 -11 .05 -01	.59 .41 .22 .13 .06 .01 .01 .04 .02
0.44 b/2	0 1.50 7.00 15.00 15.00 20.00	38 44 15 13 13 13 13 13 13 13 13 13 13 13 13 13	*9688*65*99*8829°	.64 -14 -36 -36 -36 -36 -36 -36 -36 -36 -36 -36	.64 76 73 -1.01 -1.15 -1.21 -1.06 40 39 29 04	- 59 -1.05 -1.164 -1.21 -1.21 -1.69 - 59 - 35 - 1.4 09	.32 -1.18 -1.24 -1.14 96 86 80 80 77 57 57		66 95 80 71 29 37 45 45 45	- 26 - 51 - 60 - 49 - 35 - 44 - 45 - 43 - 34	.14 14 26 45 71 75 38 20 06	.14 .17 .19 .45 .66 .08 .01 .04	. 60 . 40 . 80 . 80 . 80 . 80 . 80 . 80 . 80 . 8	.68 .54 .35 .17 .06 .21 .05 .05 .01



TABLE XVI.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.80; R = 2,000,000; PROPELLERS REMOVED - Continued (a) α_u = -2°, 0°, 2°, 4°, 6°, 8° - Concluded

	Per-			Upper	surface			Г		Lower	surface		
Spanwise stations	cent			Angle o	f attack					Angle	of attack		
BURGIONS	chord	ပို	o°.	20	40	60	80	~2°	00	20	¥0	.6°	go .
ი.56 ъ/2	0 1.5 7.0 15.0 15.0 30.0 50.0 50.0 50.0 95.0	ଶ୍ୱର ଅଧିକ ଅଧିକ ଅଧିକ ଅଧିକ ଅଧିକ ଅଧିକ ଅଧିକ ଅଧିକ	0.40 -140 -0.84 -1.33 -1.33 -1.33 -1.33 -1.38 -1	55288528822388528 6111111111188528	0.55 -33 -570 -770 -951 -69 -321 -3218 -64	0.51 -57 -75 -78 -1.00 -1.09 89 89 36 32 06	0.45 74 91 97 -1.16 -1.15 -1.09 41 50 35 36 06	-0.55 -0.55 -0.55 -0.55 -0.55 -0.55 -0.55 -0.55 -0.55 -0.55 -0.55	-0.37 69 61 52 33 26 15 04	9.36 1.35 1.35 1.37 1.38 1.38 1.38 1.38 1.38 1.38 1.38 1.38	0.24 01 16 15 11 12 11 06 01	0.40 .16 .04 04 05 05 06 05 06	0.50 .28 .31 .05 .04 .01 .01 .01 .01
0.68 b/2	0 1.5 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	ଞ୍ଚିଷ୍ଟ ପ୍ରଥମ ଅନ୍ଧ୍ୟ ସେଥି ଅନ୍ଧ୍ୟ ଅନ୍ତ ପ୍ରଥମ ଅନ୍ଧ୍ୟ ଅନ୍ଧ୍ୟ ଅନ୍ଧ୍ୟ ଅନ୍ତ ପ୍ରଥମ ଅନ୍ଧ୍ୟ ଅନ୍ତ ପ୍ରଥମ ଅନ୍ଧ୍ୟ ଅନ୍ତ ପ୍ରଥମ	1,766,999,48,756,48,48,48,48,48,48,48,48,48,48,48,48,48,	848545254 8668888888888888888888888888888888888	.60 23 57 71 84 78 84 75 29 29 29 29	5584 \$ 0.0 \$ 85.9 \$ 4.55 	- \$7 - 75 - 1.96 99 91 66 59 50 34 25 20	12.25 11.12.55 11.12.	73 92 79 70 54 31 21 05 01 08 11	-36 -36 -35 -35 -37 -37 -37 -37 -37 -37 -37 -37 -37 -37	- 10 - 10 - 10 - 10 - 10 - 10 - 10 - 10	.40 .20 .20 .05 .01 .02 .03 .01 .04 .06 .09	.50 .50 .50 .50 .50 .50 .50 .50 .50 .50
o.80 b/2	0 1,5 4,0 7,0 10,0 30,0 30,0 40,0 50,0 60,0 90,0 95,0	.21 .52 .30 .17 .03 10 18 19 16 10 10	- 19 - 19 - 11 - 120 - 1	21 14 14 14 14 14 14 14 16 16 16 16 16 16 16 16 16 16 16 16 16	.64 28 50 64 71 75 70 68 56 12 12 03	-52 -62 -80 -90 -97 -94 -89 -86 -76 -42 -30 -11 -01	-39 -87 -1.04 -1.01 -1.12 -1.02 -1.01 98 -80 62 49 16 10	80 74 70 64 54 54 10 03	89 86 74 69 52 25 10 04 03 03	35 35 31 35 31 35 31 39 39 39 39 39 39	.23 .09 10 09 06 06 .04 .04 .13	.42 .22 .06 .01 .02 .01 .07 .07 .09 .10	.52 .30 .15 .09 .07 .04 .09
0.94 b/2	0 1.5 10.0 10.0 15.0 20.0 40.0 50.0 60.0 70.0 80.0 90.0	.11 .51 .35 .20 .09 .01 06 15 18 17 14 14	.20 .42 .24 .10 01 16 21 22 16 13 18 06	.50 .22 .01 .22 .21 .23 .31 .33 .33 .26 .21 .28 .18	.65 15 34 53 53 55 47 41 37 19 12 05	.59 53 66 79 89 81 75 53 21 16 11 03	.48 84 98 97 90 82 86 49 19 19 04	149 1 455 1 439 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-1.07 89 56 32 26 14 06	50 37 37 38 06 06 06 15 16	.10 06 12 13 11 09 04 02	.36 .04 0 0 01 0 .02 05 .06 .08	.\bar{47} -\bar{22} .1\bar{4} .005 .003 .003 .003 .003 .009 .009



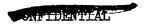


TABLE XVI.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.80; R = 2,000,000; PROPELLERS REMOVED - Continued (b) $\alpha_{\rm U}$ = 10°, 12°, 14°, 16°, 18°, 20°

S	Per-			Upper	nurface	<u>`</u>				Lower	surface		
Spenyise stations	cent chord			Angle o							attack		,
о.10 ъ/2	0 1.5 4.0 7.6 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	100 0.49 -1.01 -1.05 -1.17 -1.11 -1.09 94 95 57 64 71 41 22 18	12° 0.39 -1.19 -1.25 -1.34 -1.27 -1.29 -1.049979637180613933	14° 0.26 -1.37 -1.49 -1.49 -1.40 -1.19 -1.069284805154	16° 0.14 -1.41 -1.32 -1.30 -1.21 -1.18 -1.10 -1.0197878607061	18° 0.01 -1.29 -1.27 -1.21 -1.20 -1.17 -1.16 -1.12 -1.029793998073	20° 0.11 -1.14 -1.33 -1.37 -1.37 -1.38 -1.26 -1.26 -1.21 -1.16 -1.099968	35° -23° -354 -28° -23° -15° -111 -09° -06° -02° -02°	12° 0.79 .64 .36 .31 .24 .19 .10 .11	14° 0.84 .72 .53 .43 .29 .23 .19 .14 .13	16° 0.89 .79 .60 .50 .44 .35 .29 .19 .16	189 0.91 .85 .56 .51 .41 .35 .29 .23 .20	0.9h -91 -73 -62 -57 -46 -40 -33 -28 -24 01
0.19 b/2	0 1-5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 90.0 95.0	.18 -1.21 -1.40 -1.27 -1.25 -1.18 -0.4 -1.13 -1.047458443327	.01 -1.30 -1.32 -1.07 -1.05 -03 -1.08 -1.06 87 73 61 49	21 -1.25 -1.15 -1.00 -1.00 -1.04 -1.05 93 32 79	-37 -1.14 -1.04 95 93 .01 95 91 86 84 63 60	55 -1.07 -1.06 98 98 0 -1.00 -1.00 92 91 65 63	77 -1.19 -1.15 -1.11 -1.11 -1.12 -1.13 -1.11 -1.00 93 86 80	.74 .66 .46 .27 .04 .03 .02 .04	.75 .73 .73 .38 .16 .04 .04	.74 .78 .67 .46 .26 .10 .07 .03 .01	.74 .62 .72 .55 .36 .18 .12 .04 .03	.69 .8k .63 .44 .2k .16 .06 .04	.64 .37 .34 .70 .52 .32 .22 .10 .07
0.31 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 90.0 95.0	.36 -1.02 -1.34 -1.43 -1.38 -1.37 -1.18 -1.00 81 61 49 34 25 20	.29 -1.10 -1.36 -1.29 -1.31 -1.22 -1.15 -1.01 65 65 60 40	17 -1.24 -1.24 -1.19 -1.19 -1.14 -1.19 -1.14 -1.00 -1.70 -66 -59 -59	-1.25 -1.26 -1.15 -1.16 -1.06 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00 -1.00	04 -1.19 -1.17 -1.00 -1.04 -1.03 93 91 81 74 65	1.99.3.38.88.5.5.5.5.68.8 1.99.3.88.86.5.5.5.5.68.8 1.99.3.88.86.5.5.5.5.68.8	.66 .49 .29 .22 .18 .11 .06 .03	.70 .57 .38 .89 .25 .18 .19 .05	.75 .65 .36 .30 .24 .14 .10	.80 .72 .53 .45 .39 .30 .21 .01	.63 .78 .53 .45 .35 .26 .19 .04	.91 .83 .69 .60 .52 .35 .25 .25
0-375 b/2	0 1.5 20.0 15.0 20.0 30.0 50.0 50.0 70.0 90.0 95.0	.22 -1.30 -1.32 -1.21 -1.05 -1.01 -0.01 -0.01 -0.00 -0	00000000000000000000000000000000000000	- 188 - 189 - 189	- 23 - 280 - 76 - 77 - 77 - 76 - 75 - 76 - 76 - 76 - 76 - 76 - 76 - 76 - 76	- 41 - 81 - 81 - 75 - 75 - 75 - 75 - 77 - 77 - 77 - 71 - 71	51 74 75 74 73 73 0 72 72 72 72 70 70	.64 .49 .30 .21 .15 .07 .03 04 05	.65 .56 .56 .38 .22 .13 .06 06	.67 .61 .35 .29 .18 .09 06	.66 .66 .41 .34 .24 .15 .01 05	.64 .69 .57 .40 .29 .20 .03 .24 .36	.63 .72 .62 .54 .36 .36 .26
o.44 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	.14 91 93 86 75 75 75 76 59 43	07574 - 12688888888 - 8888888888888888888888888888	- 13 - 74 - 75 - 76 - 76 - 66 - 66 - 66 - 66 - 75 - 75 - 75 - 75 - 75 - 75 - 75 - 75	29 -7373 -1288 -1373 -13	- 45 - 70 - 70 - 69 - 69 - 69 - 69 - 69 - 69 - 69 - 63 - 60 - 55	61 69 69 69 70 70 60 61 61	.70 .61 .27 .07 .05 14 06 06 06	.70 .57 .51 .35 .14 09 10 10 09	.69 .71 .58 .½2 .23 01 06 11 10	.64 .49 .49 .31 .66 03 06 10	.63 .70 .70 .56 .39 .13 .01 .04 .06 10	.59 .90 .76 .63 .46 .20 .06 .01 09 08



TABLE XVI.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.80; R = 2,000,000; PROPELLERS REMOVED - Concluded (b) $\alpha_{\rm u}$ = 10°, 12°, 14°, 16°, 18°, 20° - Concluded

Spanwise	Per-				surface			٦				surface		
stations	cent chord		120	Angle o	of attack	180	20°		100	12°0	Angle o	160	180	20°
0.56 b/2	01.4.0000000000000000000000000000000000	10° 0.34 -1.04 -1.25 -1.27 -1.26 -1.31 -1.14614741362916	12° 0.26 -1.10 -1.34 -1.39 -1.33 -1.066246332420	14 0.15 -1.22 -1.50 -1.51 -1.51 -1.52 -1.64 51 40 33 29	160 0.051 1-1-1-555 1-1-1-1-1-1-1-1-1-1-1-1-1-1	904605555456885543 9777777777777777777777777777777777777	-0.19 -1.64 -1.69 -1.63 -1.53 -1.53 -1.12 -1.02 -76 -65		0.59 .39 .31 .31 .07 .04 .08 .01 .00	0.64 .¥6 .20 .16 .10 .07 .04	0.68 .53 .35 .26 .29 .15 .07	0.72 .79 .34 .38 .22 .11 .01 .08	10.56 19.9557.79.7.15.988.7.15.888.7.10.15.888.7.15.888.7.15.888.7.15.888.7.15.888.7.15.888.7.15.888.7	0.76 .73 .56 .48 .34 .26 .34 .26 .09
0.68 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	.29 -1.08 -1.11 -1.09 -1.09 91 71 63 38 26	.19 99 91 85 74 66 51 34 32	.06 89 84 85 83 76 76 75 37	07 -189 89 89 64 54 41	1888888888884 1111	38 11.05 996 996 1388 14.05 16.05 16		9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	.59 .15 .29 .16 .10 .07 .06 .04 .05	.59 .50 .54 .24 .20 .13 .09 .06 .03 .03 .04 .04	.55 .53 .53 .53 .54 .54 .54 .55 .55 .55 .55 .55 .55 .55	ું કર્જ જન્મ ! કર્વ જ મું ક્ષ	.54 .59 .47 .38 .31 .24 .17 .08 .03 .04 17
0. 8 0 b/2	0 1.5 4.0 7.0 10.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	.16 -1.21 -1.35 -1.26 -1.27 -1.20 -1.0687796961382619	.05 -1.27 -1.25 -1.19 -1.16 -2.98 88 67 60 51	11 -1.05 -1.05 -1.05 -1.05 97 86 83 76 72 661 54	25 96 95 90 90 84 85 79 57 57	% 44.44.65 44.44.66 46.66 46 46 46 46 46 46 46 46 46 46 46 46 4			.57 .40 .25 .16 .14 .09 .07 .08 .09 .05	.59 .45 .29 .20 .16 .10 .06 .06 .06 .08	.60 ,19 .31 .25 .20 .13 .07 .06 .05	.79 .53 .37 .29 .24 .15 .06 .04 .01 10	84. 1. 2. 8. 5. 8. 5. 6. 5. 5. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6.	.55 .56 .34 .39 .29 .20 .09 .06 .01 05 15
0.94 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 90.0 95.0	.28 -1.34 -1.20 -1.20 -1.16 -1.04 81 66 51 40 26 17 09	.19 -1.29 -1.23 -1.22 -1.18 -1.01 94 75 64 75 64 75 24	.04 -1.15 -1.20 -1.11 -1.07 96 93 78 71 67 59 72 43 38	11 -1.04 -1.11 -1.03 95 81 74 69 59 59	- 25 - 25 - 25 - 26 - 26 - 26 - 26 - 26 - 26 - 26 - 26	- 35 - 80 - 80 - 80 - 77 - 72 - 76 - 63 - 63 - 63 - 63 - 51		.52 .29 .29 .12 .10 .05 .03 .04 .06 .05	.56 .33 .24 .15 .01 .01 .01 .01	.56 .28 .20 .11 .07 .02 .01	.56 .30 .24 .18 .30 .04 .07 .07	.55 .35 .26 .20 .10 .05 .01 .05 .16 .16 .27	.52 .45 .37 .29 .21 .13 .05 .01 16 24

TABLE XVII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.90; R = 2,000,000; PROPELLERS REMOVED
(a) $\alpha_{\rm U}$ = -2°, 0°, 2°, 4°, 6°, 8°

	Per-			Upper	Burface					Lower	Surface		
Spanvise Stations	cent			Angle o	f attack					Angle o	f attack		
0.10 5/2	0 1.5 4.0 7.0 10.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	-2° 0.50 -41 -19 -05 -01 -16 -24 -27 -34 -36 -36 -36 -30 -11	0° 0.61 .30 .08051320323445514508	0.68 0.15 0.26 0.38 0.38 0.38 0.38 0.39 0.39 0.39 0.39 0.39 0.39 0.39 0.39	0.72 01 36 39 37 52 53 53 53 53 53 53 53	6° 0.7221545557626161638327	8° 0.581156717269677266798836	थ । तथ । ध्रम्भ सम्बद्ध मन	0.01 27 27 27 27 36 36 33 13	0.18 -14 -15 -17 -21 -25 -30 -10 -07	0.36 .13 0 -04 06 11 16 23 36 27	0.51 .28 .07 .04 .02 .02 .07 .14 .19 .04	8° 0.64 .41 .24 .17 .06 .02 .04 .05 .01
0.19 b/2	0 1.5 4.0 7.0 10.0 20.0 30.0 40.0 50.0 60.0 90.0	63 44 35 19 50 19	726 02 02 1 50 1 50 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	810 80 10 10 10 10 10 10 10 10 10 10 10 10 10	#17##\$883 -8867P#173817#	-66 -44 -774 -68 -78 -78 -78 -78 -78 -78 -78 -78 -78 -7	.54 66 96 96 -1.12 -1.17 86 84 84 85			.66. - 56. -	. 45 . 25 . 06 - 16 - 37 - 01 - 01 - 01 - 05	.60 .40 .20 .02 .38 .74 .03 .04	.69 .54 .33 .11 -23 46 05
0.31 b/2	0 1.5 4.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 90.0	254545454848484484444444444444444444444	455575473568638445	11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	515586188813864138	58 1.06 1.76 1.997 1.09 5.56 9.56 9.56 9.56 9.56 9.56 9.56 9.5	-55 -53 -53 -53 -53 -58 -58 -1.09 -1.00 -1	466 887 655 45 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1030 1051 1051 1051 1051 1051 1051 1051	- 05 - 29 - 34 - 32 - 28 - 29 - 43 - 12 - 03	16 - 06 - 18 - 20 - 19 - 17 - 20 - 24 - 34 - 39 - 19	36 03 06 06 08 11 14 26 34	50 30 H2 57 55 H 57 7 N 35 H 57 1 N 35 H 5
0.375 b/2	0 1.5 7.0 15.0 20.0 50.0 70.0 70.0 90.0 95.0	A 3 5 4 8 5 4 8 5 4 9 8 6 4 9 8 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	.48 .22 01 21 33 1 43 1 67 1 69 1 69 1 60 0	\$3300 \$500 \$600 \$600 \$750 \$600 \$750 \$600 \$750 \$600 \$750 \$750 \$750 \$750 \$750 \$750 \$750 \$7	38288888888888888888888888888888888888	59 -59 -59 -68 -59 -68 -68 -68 -69 -74 -74 -75	.51 	548 SB885 55 49	28 57 63 57 49 34 14 9 12 66 12 66	da a	ង្គ នៃមានស្លា និង ខ្មែ	.44 .21 .04 -08 -14 -20 -36 -42	AB 45857 88 78
0.44 b/2	01.500000000000000000000000000000000000	539998333856843888	\$252555684356722922 	?0584555888553886538888	######################################	63971.843.886676668.9977.43	\$\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	48 GERSSEAN 11	5% BESSB894 80 { { { { { { { { { { { { { { { { { { }}}}}}	28 148664752 55	44.46 51.51.50 51.	.58 .35 .01 .24 59 83 02 .02 16 26	१६५ मन्त्रम् ४८५४ तुम्र

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TABLE XVII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.90; R = 2,000,000; PROPELLERS REMOVED - Continued (a) $\alpha_{\rm U}$ = -2°, 0°, 2°, 4°, 6°, 8° - Concluded

	Per-			Upper	surface			П			Lower	surface		
Spanwise stations	cent chord			Angle o	f attack			[f attack		
74001022	enora	_00_	_0°	20	No.	6°	80	_	_e°	00	20	70	6º	_8º
0.56 b/2	0 1.50 70.0 15.0 15.0 30.0 50.0 70.0 70.0 80.0 95.0	0.24 	0.38 .11 .150 30 576 63 56 56 29 14 02	0.47 02 34 73 73 80 22 15 01	0.54 198 58 693 89 96 30 30 19 03	0.54 35 55 68 90 96 -1.92 89 36 36 36 08	0.51 -53 79 86 -1.04 -1.09 -1.05 51 51 18 15		9888888 1 88888 1 88888 1 1 1 1 1 1 1 1 1	-0.34 60 79 63 50 43 43 20 04	-0.11 -39 -35 -36 -39 -24 -15 -03 -03 -08	0.10 -15 -26 -27 -23 -23 -23 -23 -23 -23 -24 -25 -25 -25 -25 -25 -25 -25 -25 -25 -25	0.28 .04 10 14 13 14 14 15 05 05	0.41 .17 .01 04 06 09 10 12 07 10 08
0.68 b/2	0 1.4.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.	##\$\$\$\$################################	885188888488458	\$7188885#\$888\$989 	.57 08 156 78 80 17 89 17 19 17	\$#5%\$\$\$\$\$\$\$##&8 	.53 -58 -59 -59 -59 -58 -58 -58 -58 -58 -58 -58 -58		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1.54 1.75 1.84 1.85 1.42 1.14 1.02 0.03 0.12 1.14	-21 -42 -43 -37 -23 -23 -01 -04 -09 -11	19 19 19 19 19 19 19 19 19 19 19 19 19 1	.27 .06 07 1k 13 03 01 .05	.40 .19 .04 05 07 06 01 .01 .01 06 12
ი. მი ъ/2	0 1.00000000000000000000000000000000000	ଞ୍ଚୁଞ୍ଜୁଟ୍ଟେମ୍ବର୍ଷ ଅଷ୍ଟ୍ରମ୍ପର ଜଣ୍ଣ ମଧ୍ୟ ସମ୍ବର	୬.୮.ଅ୬୩ ଅଞ୍ଚଳ ଅନ୍ୟ ଅନ୍ତ । ୮୮୮୮୮୮୮୮୮୮୮୮୮୮୮୮୮୮୮୮୮୮୮୮୮୮୮୮୮୮୮୮୮୮୮୮	&7985\$5\$8\$*\$989 	643686555568556885568855688	\$\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	. \$9 80 80 96 -1. 06 -1. 01 74 51 51 28 17		7380 555,555 H& 84,44,68	73 85 76 74 64 23 08 01 04 09	140 140 130 0 00 111 13	1 1 8 2 8 8 9 9 1 7 3 8 8 9 7 7	309 309 309 309 309 309 309 309 309 309	.43 .21 .06 0 0 03 01 .00 .06 .07
o.9k b/≥	0 1 5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ଞ୍ୟୁ ଅନ୍ତର୍କ ମୁଖ୍ୟ ଅଧ୍ୟ ସ୍ଥର୍ଚ୍ଚ	ଷ୍ୟ ଅଟ୍ୟ ମନ୍ଧ୍ୟ ଷ୍ଟ୍ରଅନ୍ଥ ସ୍ଥ	នុក្សក្នុងនគនិង ប្រព័រ្ធ ព្រះព្រះ	58838888844584 666666688844584	\$	5.67485586758655566515665127		157 155 145 145 145 145 145 145 145 145 145	999 0455740 155740 1757417	1.35 1.45 1.39 1.33 1.20 1.09 1.14 1.15	dh	୍ଷ୍ଟ ଚ୍ଚ୍ଚମ୍ମ ଚ୍ଚ୍ଚମ୍ଚ	.39 .13 .05 01 05 05 05 05 01 .01

TABLE XVII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.90; R = 2,000,000; PROPELLERS REMOVED - Continued (b) $\alpha_{\rm U}$ = 10°

			The	surface	 		 		
Spanwise Stations	Fer-			of attack			 Angle	of attach	
	chord	10°				10°			
0.10 b/2	0 1.5 4.0 7.0 10.0 20.0 30.0 40.0 50.0 60.0 70.0 90.0	0.61 66 87 88 83 77 894 7894 43				0.72 .53 .34 .27 .22 .14 .09 .05 .01			
0.19 6/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 70.0 80.0 95.0	. 39 -1.86 -1.12 -1.17 -1.19 -1.29 -1.31 -1.10 95 85 85 85 41 33 27				.46 .24 .28 .31 .30 .31 .31			
0.31 b/2	0 1.50 0 1.50 7 19.50 150.00 1	.889.99.99.99.99.99.99.99.99.99.99.99.99				.61 .13 .24 .16 .16 .00 .00 .00 .00			
0.375 b/2	0 1.5 7.0 10.0 15.0 20.0 30.0 50.0 60.0 70.0 80.0 95.0	.40 91 -1.05 -1.05 -1.05 -1.03 77 77 71 70 66 66				.61 .45 .16 .10 .02 05 25 26			
0.44 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 \$0.0 \$0.0 60.0 70.0 80.0 95.0	.35 -1.86 -1.77 77 71 69 70 70 70 58				.70 .58 41 .24 01 37 56 11 12 29 40			

CONTENTAL



TABLE XVII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.90; R = 2,000,000; PROPELLERS REMOVED - Concluded (b) $\alpha_{\rm U}$ = 10° - Concluded

	Per-		Upper sur	face	 T	 Lover	surface	
Spanwise stations	cent chord		Angle of a	ttack		 Angle	of attack	
0.56 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 50.0 60.0 70.0 80.0 90.0	10° 0.46698798 -1.10 -1.12 -1.16 -1.141107150403026			10° 0.50 0.50 0.710 0.04 0.0105061411415			
0.68 b/2	0 1.5 4.0 70.0 15.0 20.0 30.0 \$0.0 70.0 80.0 90.0	. 43 67 1.02 -1.00 -1.00 -1.00 79 75 76 72 71 64 55 40			.47 .27 .11 .03 .05 .05 .05 .05 .05 .05			
0.80 5/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 70.0 80.0 95.0	.37 81 99 -1.06 -1.10 -1.05 -1.05 -1.05 -1.92 80 71 58 51 55			- 148 - 28 - 111 - 04 - 03 - 03 - 01 - 01 - 01 - 05 - 19			
0.94 5/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 70.0 80.0 90.0 95.0	. 44 			- 16 .04 0 - 05 - 07 - 06 - 06 - 06 - 06 - 15			

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TABLE XVIII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.165; R = 8,000,000; PROPELLERS REMOVED (a) α_u = -2°, 0°, 2°, μ °, 6°, 8°

Spanwise	Per_			pper surf	ace			Т	т	L	ower surf	ace		
stations	chord		An	gle of at	taok			3		An	gle of at			
 -	 	_e°	00	S _o	40	6°	Я ^O	1_	-2°	00	20	40	60	, 8°
0.10 b/2	0 1.5 1.0 7.0 10.0 150.0 30.0 40.0 70.0 80.0 90.0	0.16 .34 .02 09 14 21 21 15 15 11 03	0.42 -17 -0.4 -13 -22 -29 -31 -30 -26 -20 -20 -17 -13 -05	0.54 - 03 - 29 - 36 - 36 - 31 - 36 - 31 - 20 - 104 - 03	0.54 -333 -446 -52 -52 -51 -38 -31 -26 -24 -17 -16	0.45 66 66 66 53 33 36 33 36 33 36	0.22 -1.02 86 87 86 72 80 34 38 36 38		- 68d - 5*91 38 50 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-0.31 -37 -36 -39 -25 -19 -19 -02 -03 .04	0.01 13 25 19 15 11 09 04	0.25 .07 11 09 07 05 01 .04	0.43 .25 .06 0 .01 .01 .09 .08	0.55 .39 .19 .10 .10 .07 .07 .06 .09 .10
0.19 b/2	0 1.5 7.0 19.0 19.0 30.0 \$0.0 \$0.0 \$0.0 \$0.0 \$0.0 \$0.0 \$0	.06 .37 .08 .02 04 15 24 19 16 15 11	.39 .22 12 16 20 30 31 24 21 17 13 03	.54 14 37 38 43 39 36 29 24 29 03	.52 53 66 56 56 58 44 35 27 23 15 03	-30 -99 -97 -77 -75 -75 -51 -40 -31 -25 -17 -03	10 -1.55 -1.34 -1.03 97 89 65 57 35 28 04		1.65 1.43 1.43 1.48 1.68 1.68 1.69 1.69 1.69 1.69 1.69 1.69 1.69 1.69	- 31 - 32 - 32 - 33 - 23 - 21 - 11 - 05 - 05	16 16 15 11 08 0	.30 .11 01 05 05 03 03 .06	.47 .28 .07 .04 .03 .04 .05 .06	.55 .41 .24 .15 .13 .09 .08 .10
0.31 ъ/2	0 1500000000000000000000000000000000000	55 -45 -53 -45 -47 -47 -47 -47 -47 -47 -47 -47 -47 -47		កុំខ្លួននេះខ្លួននេះគឺក្រុងជួនខ្លួននេះ ក្រុកក្រុកក្រុកក្រុងជួនខ្លួននេះគឺក្រុងជួនខ្លួន	.50 47 59 58 57 52 45 45 37 31 24 01	.35 95 96 79 74 56 51 34 34 19 04	23 -1.49 -1.15 -1.03 90 65 57 38 38 01		-76 -68 -30 -35 -35 -35 -31 -30 -31 -30 -35 -35 -35 -35 -35 -35 -35 -35 -35 -35	130 1-36 1-37 1-37 1-37 1-37 1-37 1-37 1-37 1-37	.06 07 13 15 12 10 06 02	.35, .16 .03 02 02 01 .02 02 03	.50 .33 -15 .08 .07 .04 .04 .06	.55 .55 .29 .19 .11 .10 .11 .10 .11 .10 .10 .10 .10 .10
0.375 ъ/2	0 1.50 7.0 10.0 15.0 20.0 30.0 40.0 50.0 70.0 80.0 95.0	.05 03 15 20 15 20 15 15 15	.39 .19 01 14 20 25 26 27 21 21 14 03	-54 -17 -29 -343 -41 -39 -30 -21 -30 -21 -04	- 48 - 59 - 56 - 58 58 35 35 17 05	81588358 12258 55 1111111111	- 32 -1.74 -1.29 -1.18 -1.06 -93 -84 - 36 - 36 - 29 - 04		24 67 51 43 36 26 19 06 02	29 35 30 28 24 18 12 03 .01	08 09 13 14 12 06 01 04	.36 .15 .01 01 01 01 0 .05 .05 .09	.51 .35 .18 .11 .10 .06 .06	.56 .45 .29 .21 .17 .13 .11 .11 .12
0.44 b/2	0 1.5 \$.0 7.0 10.0 15.0 20.0 30.0 \$0.0 50.0 70.0 80.0 95.0	04 .41 .20 .06 01 14 19 19 16 14 11	.37 .102 13 19 24 26 27 26 24 21 19 14	.54 39 40 38 38 38 36 36 153 05	.50 59 60 59 59 59 24 24 05	11588868889985588 11111111111	31 -1.71 -1.33 -1.20 -1.93 83 696 466 36 166 02		83 70 51 35 20 20 01 06 01	-32 -40 -32 -28 -28 -27 -17 -14 -07 -03 .03	.09 08 13 14 09 07 01 .05 06	.38 .14 .04 01 01 01 01 .04 .08	.53 .34 .18 .12 .10 .07 .05 .08 .09 .11	.56 .46 .29 .22 .18 .14 .11 .11 .13 .10 .10



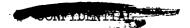


TABLE XVIII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.165; R = 8,000,000; PROPELLERS REMOVED - Continued (a) $\alpha_{\rm U}$ = -2°, 0°, 2°, 4°, 6°, 8° - Concluded

	Per-			Upper	surface			Т			Lower	surface		
Spanvise stations	cent chord				of attack]				f attack		
BOLIOLD	anara.	- <u>2</u> °	00	20	40	Ġ.	80	1_	-50	00	50	40	ρ.	βc
0.56 b/2	0 1.5 7.0 10.0 10.0 15.0 30.0 40.0 60.0 90.0 95.0	-0.11 .14 .23 .10 008 09 14 17 17 13 10 01	0.34 -21 02 12 18 22 23 24 22 20 11 01	0.52 -1.29 -1.35 -1.36 -	0.16 	0.11 -1.12 88 83 74 56 47 40 32 25 06	-0.51 -1.78 -1.36 -1.32 -1.09 73 75 35 16 01		982 52589 # 1 589 9 1 1 1 1 1 1 1 0 589	-36 -39 -39 -39 -39 -39 -39 -39 -39 -30 -30 -30 -30 -30 -30 -30 -30 -30 -30	0.04 09 14 15 09 09 09 09 09 09	0.37	0.52 .34 .18 .11 .10 .07 .08 .08 .08	\$\\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\
0. 68 ъ/2	0 1400000000000000000000000000000000000	.50 .26 .13 .05 08 18 15 12 11 09		୍ ଓଟ୍ଟେକ୍ଟେକ୍ଟେକ୍ଟେକ୍ଟେକ୍ଟେକ୍ଟେକ୍ଟେକ୍ଟେକ୍ଟେ	- 1.59 - 1.57 - 1.57 - 1.47 - 1.39 - 1.22 - 1.25 - 1.04	- 96 - 97 - 89 - 89 - 66 - 57 - 40 - 31 - 124 - 17 - 03	-1.58 -1.35 -1.36 -1.90 80 80 35 35 35 36		-1.13 -1.82 -1.57 -1.46 -1.37 -1.26 -1.20 -1.05 -1.01 -1.05 -1.01 -1.05	-,51 -,49 -,35 -,30 -,25 -,27 -,19 -,12 -,01 -,02 -,01 -,05 -,06	- 1.04 - 1.15 - 1.16 - 1.19 - 1.18 - 1.19 -		16 16 10 10 10 10 10 10 10 10 10 10 10 10 10	1.48 8.08 1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1
0.80 ъ/2	0 1.5 1.0 10.0 15.0 20.0 30.0 50.0 60.0 80.0 95.0	18 .50 .31 .09 .01 0k 0k 11 12 11 10 08	.33 .32 .09 03 08 14 17 19 16 14 10	.77 .027 .128 .299 .297 .208 .209 .209 .209 .209 .209 .209 .209 .209	54 144 144 144 144 144 144 144 144 144 1	.19 92 83 71 65 59 47 37 30 16	- 45 -1.55 -1.10 -1.06 57 51 51 43 34 03		-1.32 89 61 50 39 28 07 01 .02 .05	- 66 - 58 - 49 - 34 - 34 - 35 - 36 - 19 - 65 - 65 - 65 - 65 - 65	15 21 18 14 11 04 01 .05 .07		. 45 .33 .57 .66 .64 .55 .68 .68 .69	.57 .42 .27 .18 .15 .11 .09 .09 .10
o.94 b/2	0 1.5 4.0 7.0 10.0 20.0 30.0 40.0 50.0 70.0 80.0 90.0	82 .52 .36 .22 .13 .06 .03 0 08 11 09 06	- 39 - 39 - 39 - 65 - 68 - 68 - 69 - 15 - 14 - 15 - 65 - 65 - 65	.40 .16 05 15 15 13 21 21 21 21 21	.54 38 38 39 37 27 27 11 11 05	17 - 59 - 69 - 50 - 150 - 135 - 129 - 120 - 105	80408685945882768		-1.73 54 51 80 27 18 10 06 .06	- 57 - 525 - 36 - 36 - 37 - 38 - 38 - 38 - 38 - 36 - 35 - 36 - 36 - 36 - 36 - 36 - 36 - 36 - 36	39 26 29 22 17 13 09 05 05 .04	.07 06 10 10 08 06 05 01 01	.36 .33 .05 .01 .05 .02 .05 .05 .05 .05	.53 .26 .19 .12 .10 .06 .05 .05 .06 .06

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TABLE XVIII.- PRESSURE COEFFICIENTS AT NINE, SPANWISE STATIONS OF THE WING. M = 0.165; R = 8,000,000; PROPELLERS REMOVED - Continued (b) $\alpha_{\rm U}$ = 10°, 12°, 14°, 16°, 18°, 20°

Spanwise	Per-			Upper	mirface						Lower	surface		
stations	cent			Angle o	fattack						Angle o	f attack		
	ohord 0	10°	12°	11.0°	16 ⁸	18° -2.74	20 [°] -3.76	Н	10°	12º	Ile ^C	160	18°	50°
0.10 1/2	1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 70.0 80.0 95.0	-1. \$2 -1. 21 -1. 06 99 89 89 67 56 36 29 22 06	-1.56 -1.32 -1.66 -7.60	-2.13 -1.88 -1.97 -1.39 -1.06 89 50 41 06 01	-2.99 -2.198 -1.75 -1.31 -1.89 54 43 43 43 43 43	-1.75 -2.54 -1.75 -1.45 -1.75 -1.35	1183385888555554495		0.62 .50 .30 .19 .13 .11 .13 .14 .19 .08	0.64 .60 .30 .28 .20 .16 .17 .17	0.60 .66 .49 .39 .35 .24 .22 .22 .21 .14	0.53 .70 .57 .45 .41 .38 .26 .25 .27	0.40 77 64 71 89 393 393 86 189	0.24 -73 -69 -58 -54 -38 -34 -33 -30 -19
0.19 5/2	0 1.5 7.0 10.0 15.0 20.0 30.0 50.0 60.0 70.0 80.0 90.0	66		4588641385548446	\$	1.757.46 1.757.46 1.758.658.6486.112.89 1.758.658.6486.112.89	-6.28 -6.38 -1.89 -2.89 -1.53 -1.53 -1.53 -1.80 14 20		.56 .50 .35 .26 .22 .16 .15 -13 .14	.48 .57 .57 .35 .30 .24 .20 .16 .16	.32 .59 .59 .50 .37 .30 .25 .20 .20	195 199 198 178 198 198 178	-17 -53 -59 -53 -49 -41 -35 -26 -25 -06	-53 -53 -59 -59 -45 -45 -40 -31 -29 -16
0.31 8/2	0 1.50 7.00 15.00 15.00 20.00	-87 -9-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-	444444 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	858833888885588333 47441111110	87148638E581105	-5.49 -5.63 -6.81	-7.08 -6.40 -4.18 -3.17 -2.59 -2.01 -1.10 -7.76 33 -25 09 15		.51 .54 .37 .29 .24 .19 .15 .15	39.57 5.56 % % % % % % % % % % % % % % % % % % %	.16 .56 .52 .39 .31 .34 .4 .20 .11 .09	-114 -20 -255 -355 -356 -36 -21 -21	52 .42 .59 .53 .48 .40 .35 .30 .25	95 29 50 58 53 35 35 26 13
0.375 b/2	0 1100 7100 7100 1500 1500 1500 1500 1500	1.42 1.42 1.43 1.43 1.43 1.63 1.33 1.63 1.33 1.63 1.63 1.63 1.6	99228885482545850 97477771111	11 99 14 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1.991498663867385384991	-5.60 -5.60 -5.60 -2.33 -1.50	1982 1982 1984 1986 1986 1986 1986 1986 1986 1986 1986		.51 .54 .39 .30 .26 .27 .15 .15 .12	.36 .77 .45 .38 .33 .26 .22 .17	.13 .54 .53 .43 .49 .327 .20	-,18 -,50 -,51 -,51 -,45 -,37 -,31 -,26 -,24 -,16	56 .41 .59 .53 .49 .36 .28 .26 .17	-1.00 .28 .51 .52 .45 .39 .31 .27
0.44 b/2	0 1.5 4.0 7.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	1.05 -2.37 -1.76 -1.33 -1.97 -1.63 -1.51 -1.39 -1.39 -1.16 -1.01	4.19 -3.29 -1.29 -1.31 -1.31 -1.56 -1.31 -1.56 -1.31 -	7.00 4.00 4.00 1.00 1.00 1.00 1.00	1.59 1.587 1.581 1.586 1.1466 1.1466 1.1466 1.1467 1.1467 1.1467 1.1467	-6.16 -5.82 -2.43 -2.43 -2.43 -1.54 -1.84 -1.84 -1.11	\$554.388843863953888		.51 .55 .39 .39 .36 .20 .16 .15 .15	.32 .58 .46 .38 .34 .26 .21 .29 .19 .18	.66 .56 .53 .39 .39 .38 .25 .21 .21 .21	31 .50 .50 .46 .37 .31 .29 .26 .24	76 .40 .59 .59 .59 .35 .38 .86 .14 .88	-1.31 .27 .58 .58 .54 .46 .39 .35 .31 .28



TABLE XVIII.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.165; R = 8,000,000; PROPELLERS REMOVED - Concluded (b) $\alpha_{\rm u}$ = 10°, 12°, 14°, 16°, 18°, 20° - Concluded

	Per-			Upper	surface		1			Lower	surface		
Spenvise	cent			Angle o	of attack					Angle	of attack		
stations	chard	10°	120	T/t _Q	160	180	20°	100	120	11,0	16 ⁰	180	20°
0.56 b/2	0 1.5 4.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	1.38 -2.49 -1.753 -1.534 -1.575 -1.575 -1.58 -1.58 -1.58 -1.59 -1.	-2.56 -3.40 -2.34 -1.94 -1.66 -1.35 -1.11 89 55 40 31 04	+.89 +.29 -2.83 -1.59 -1.59 -1.59 74 58 17 17 01	-5.37 -5.30 -2.63 -2.68 -1.39 -1.69 -1.79 -1.80 -1.79 -1.80 -1.80 -1.80	7.16 -7.16 -7.89 -4.99 -1.90 -1.83 -1.83 -1.83 -1.83 -1.83 -1.99	-8.99 -7.14 -3.32 -2.72 -2.04 -1.14 -2.71 -1.74 -7.75 -20	0.51 .55 .39 .31 .26 .20 .18 .16	0.30 -57 -46 -39 -34 -26 -23 -20 -19 -16 -11	0.02 .58 .55 .40 .37 .27 .27 .21 .19 .14	-0.34 .51 .57 .58 .57 .33 .29 -12 .20 .15	-0.82 -1	*** \$5.45.85 \$8.44.4
0.68 b/2	0 1.5 10.0 10.0 10.0 10.0 10.0 10.0 10.0	\\ \?\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\				7.696 -2.43 -2.57 -1.57 -1.57 -1.14 -1.14 -1.14		8.55 8.888.886 15.7.7.7.7.7.9.0 15.7.7.7.7.7.9.0 15.7.7.7.7.7.9.0 15.7.7.7.7.7.9.0 15.7.7.7.7.7.9.0 15.7.7.7.7.7.9.0 15.7.7.7.7.7.9.0 15.7.7.7.7.7.9.0 15.7.7.7.7.7.9.0 15.7.7.7.7.7.9.0 15.7.7.7.7.7.9.0 15.7.7.7.7.7.9.0 15.7.7.7.7.9.0 15.7.7.7.7.9.0 15.7.7.7.9.0 15.7.7.9.0 15.7.7.9.0 15.7.0 15.7.	**************************************	.08 .58 .53 .36 .39 .31 .26 .21 .18 .15	- 1.53 - 1.55 -	- 24 - 85 - 85 - 48 - 48 - 88 - 88 - 88 - 88 - 88 - 88	1. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2.
0.80 ъ/2	0 1.5 4.0 7.0 10.0 20.0 30.0 40.0 50.0 60.0 70.0 90.0 95.0		-9.68 -3.02 -2.14 -1.76 -1.57 -1.27 -1.82 59 39 15 15 15 15 15	+ .88 + .86 + .86 + .87 + .17 + .17	\$444444	7.53 -5.58 -2.59 -1.80 -1.80 -1.57 57 25 14 12	-9.53 -6.44 -4.07 -3.09 -2.52 -1.55 -1.08 -78 -36 -36 -36 -36 -36 -36 -36	.37 .28 .24 .18 .13 .11 .10	.43 .55 .36 .31 .25 .16 .15 .10	.21 .58 .51 .43 .38 .30 .22 .19 .17 .14		41 47 59 538 39 85 39 39 31 15 06	
0.94 7/2	0 1.5 7.0 15.0 15.0 20.0 50.0 76.0 76.0 76.0 76.0 76.0 76.0 76.0 7	- त्राप्त । १९८५ - त्राप्त । १९८५ - १९८५ - १९८५ - १९८५	-1.66 -1.86 -1.86 -1.51 -1.03 -1.03 -1.03 -1.41 -1.01 -1.01	8553885298535882100 44441111111111111111111111111111111	######################################	5-1-94-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-	7.73 -5.22 -3.655 -2.18 -1.36 -1.895 35 35 18 18	.56 .38 .32 .21 .17 .11 .09 .06 .06	93998 HHH H H H H H H H H H H H H H H H H	.35 -52 .36 .36 .30 .22 .16 .14 -09 .06	19 5555	- 21 - 28 - 25 - 26 - 39 - 31 - 24 - 10 - 06 - 02 - 01	60 57 58 59 59 59 59 59 59 59 59

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TABLE XIX.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; PROPELLERS REMOVED

(a) $\alpha_{\rm u}$ = 2°, 4°, 6°, 8°, 10°, 12°

	Per-				Surface					Lower S			
Spanise stations	cent chord				f attack	T ==0			10	Angle of	attack go		120
0.10 ъ/2	0 1.5 4.0 7.0 10.0 15.0 20.0 50.0 50.0 70.0 80.0 90.0	0 884848888844444	* 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	8 0.25 5.55 6.25 8.88 8.89 8.79 8.79 1.11	80 -0.15 -1.72 -1.03 -1.67 -1.57 -1.	10° -0.69 -2.07 -1.40 -1.23 -1.10 -1.84 -73 -554 -551 -51	20 -4.40 -4.70 -4.70 -1.12 -1.	0.00 000000000000000000000000000000000	0.43 20 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0	0.59 .41 .25 .26 .14 .14 .17 .20 .25	0.66 5.4 .37 .30 .26 .22 .22 .25 .30	10° 0.66 .63 .47 .40 .30 .39 .88 .88 .88 .88 .88	0.610 .548 .333 .334 .335 .335 .335 .335 .335 .335
0.19 b/2	0 1.5 4.0 7.0 15.0 15.0 20.0 20.0 50.0 60.0 60.0 80.0	11111111111111111111111111111111111111	.27 -1.17 -1.07 -93 -83 -63 54 54 54 40	######################################	-1.37 -4.87 -1.55 -1.20 56 56 56 56	\$\$\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	-3.96 -4.18 -2.91 -2.25 -1.59 -1.59 -1.66 -58 -60 -38 -31	150 00 15	.57 .41 .23 .13 .05 -10 .07 -19 .25	.62 .58 .40 .38 .19 .13 .14 .22 .29	53.65 54.43 54.35 2.82 2.83 1.03 1.04 46	NG SBTRE NB TP	59 265 83 38 48 - 38 48
0-31 b/2	0 14.00 19.00 10.0	4607477747965 77747965 551-551-5595 551-5595	.23 -1.07 -1.07 -1.01 97 82 71 68 53 53	-21 -1.46 -1.45 -1.57 83 67 67 67 53	**************************************	1741116581166821 1741111111111111111111111111111111111	-2.86 -2.84 -2.85 -2.00 -1.73 -1.19 -1.01 74 57 50		.19 .31 .15 .09 .10 .08 .08 .10	.60 .49 .30 .23 .20 .18 .16 .18	.61 .61 .85 .86 .84 .84 .84	.52 .67 .45 .45 .30 .30 .30 .30	3.50 3.50 3.50 3.50 3.50 3.50 3.50 3.50
0.375 b/2	0 1.5 1.0 10.0 15.0 20.0 30.0 40.0 60.0 70.0 80.0 95.0	28787674 955588444 	.03 -1.43 -1.19 -1.13 -1.02 86 69 69 55 53 50 41	-64 -2.19 -1.57 -1.42 -1.16 -1.05 -78 -60 -55 -51 -40	-1.66 -3.08 -1.63 -1.63 -1.27 -88 -59 -54 -39	9.55 9.55 9.55 9.55 1.56 1.56 1.55 1.55 1.55 1.55 1.55 1	-1.57 -5.33 -3.26 -2.28 -1.86 -1.61 -1.05 861 -1.63 541 35	.39 .18 .05 .01 .04 .08 .18 .27	.55 .38 .14 .14 .12 .15 .33 .46	.58 .52 .36 .27 .24 .20 .20 .20 .25 .34 .47	.46 .59 .40 .35 .29 .28 .36 .36	.25 .60 .49 .44 .37 .35 .40 .39 .38	14 55 56 52 45 45 45 41 52
о.44 ъ/2	0 1.5 1.0 7.0 10.0 15.0 20.0 20.0 40.0 50.0 70.0 80.0 95.0	35 1	-25 -1.41 -1.23 -1.01 91 66 55 38	-1.20 -2.57 -1.63 -1.44 -1.09 -767 -767 -755 -1.35	2.58 -2.41 -2.75 -1.75 -1.26 -1.26 -1.26 -1.26 -1.25 -	-1.32 -1.53 -3.50 -2.17 -1.45 -1.45 -1.97 58 33 26	65.79.95 94.4.1.98.75 1.75 1.75 1.75 1.75 1.75 1.75 1.75 1	.53 .33 .16 .06 .01 .01 .09 .26 .11 .19 .26	.61 .53 .24 .17 .10 .13 .17 .22 .28	- 51.64 - 52.99.31.21.22.25.30 - 39.45	- 22 - 65 - 53 - 53 - 53 - 53 - 53 - 53 - 53 - 5	-27 -57 .73 .64 .56 .40 .33 .30 .35 -41 .48	- 93 - 40 - 72 - 66 - 40 - 73 - 73 - 73 - 73 - 73 - 73 - 73 - 73

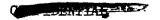




TABLE XIX.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; PROPELLERS REMOVED - Continued (a) α_u = 2° , 4° , 6° , 8° , 10° , 12° - Concluded

	Per-			Upper	surface						Lower	surface		
Spanwise	cent			Angle o	of attack			-			Angle	of attack		
stations	chord	₹°	ΙP	6°	8	10	120	Li	20	4º	6°	80	10°	120
0.56 b/2	0 1.5 4.0 7.0 15.0 20.0 30.0 50.0 70.0 80.0 95.0	0.46 	0.19 -1.09 -1.05 -1.05 -1.06 70 66 49 49 35 10 0	-0.33 -1.46 -1.33 -1.101 -1.55 -1.55 -1.55 -1.55 -1.56 -1.56 -1.56 -1.00	1.11 -2.44 -1.45 -1.45 -1.24 -1.25 -1.24 -1.25 -1.24 -1.25 -1.27 -1.27 -1.03	-2.14 -3.29 -2.37 -4.47 -1.24 -1.24 -1.25 -3.42 -1.47 -1.26 -1.47 -1.26 -1.47 -1.26 -1.47 -1.26 -1.47 -1.26 -1.47 -1.26	44444444444444444444444444444444444444		98666669	0.51 .28 .10 .07 .04 .02 .01 .05 .04	0.60 .46 .20 .20 .15 .10 .09 .07	0.60 .57 .40 .32 .25 .18 .13 .13 .05	0.49 .66 .51 .42 .36 .26 .23 .19 .06	0.28 .69 .62 .52 .46 .30 .26 .30 .26
0.68 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 20.0 40.0 50.0 70.0 80.0 95.0	5975996399394786	335688 F888 8 9 3 6 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	### NASKER\$####### 17474	1.05 -2.88 -1.85 -1.40 -1.06 -5.40 -1.10 -	4.37.488.7.4688.7.69.5.388.69.5.69.5.388.69.5.69.5.388.69.5.69.5.388.69.5.69.5.388.69.5.69.5.388.69.5.69.5.388.69.5.69.5.388.69.5.69.5.388.69.5.69.5.388.69.5.69.5.388.69.5.69.5.388.69.5.69.5.388.69.5.69.5.388.69.5.69.5.388.69.5.69.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5.5	######################################		- 100 - 100	प्राच्य वर्ष हरू ।	.56 .43 .26 .18 .10 .10 .10	1 51 5 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	.32 .57 .46 .38 .32 .24 .20 .14 .14	01 55 46 41 32 26 21 19 16
0.80 1/2	0 1.5 1.0 15.0 15.0 15.0 15.0 20.0 50.0 70.0 70.0 80.0 95.0	557 3946 - 446 - 445 - 455 - 455 - 4	327757486555541353245034	-24 -1.10 -1.10 -1.00 70 70 57 52 34 03	1.13 12.16 1.55 1.23 1.89 1.89 1.38 1.38 1.38 1.38 1.38 1.38 1.38 1.38	43.88 43.80 41.75 44.66 653 42.55 653 653 653 653 653 653 653 653 653 6	ምትላ ተተተ ፣ ፣ ፣ ፣ ፣ ፣ ፣ ፣ ፣ ፣ ፣ ፣ ፣ ፣ ፣ ፣ ፣		1985 1985 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	୍ୟରୀ ୍ଟେଖରୀ ପ୍ରତ୍ତେଶ	.56 .39 .22 .24 .13 .10 .10 .10	.56 .50 .25 .20 .16 .11 .11 .10 .09	. 42 .56 .34 .30 .22 .16 .15 .14 .11	19.56 51.228 30.21 21.22 21.22
0.94 7/2	0 1.5 1.0 10.0 15.0 20.0 30.0 40.0 50.0 70.0 80.0 95.0	.52 -04 -20 -29 -331 -33 -33 -27 -26 -20 -15 0	53 - 51 - 51 - 52 - 52 - 52 - 52 - 52 - 52 - 52 - 52	.24 94 87 82 71 64 49 37 32 28 28 12 0	38 -1.56 -1.20 -1.10 81 67 53 47 31 21 01	-1.32 -2.19 -1.67 -1.41 -1.19 80 50 51 40 33 22 12 0	4.52 4.55 4.55 4.74 1.74 1.75 1.75 1.75 1.75 1.75 1.75 1.75 1.75		16 17 20 16 15 09 01 01 03 .08 .10	N 0480000000000000000000000000000000000	.44 .20 .13 .07 .05 .04 .05 .05 .06 .07	.53 .34 .25 .16 .13 .10 .07 .07 .07	.49 -44 .35 .25 .21 .11 .10 .07 .06 .05	.34 .34 .36 .38 .38 .39 .15 .13 .68 .66 .63

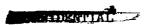


TABLE XIX.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; PROPELLERS REMOVED - Continued (b) α_U = 14°, 16°, 18°, 20°

	Per-	L.		Upper	surface	 11		<u></u>	Lower	surface	 _
Spanwise stations	cent chord				fattack] [-10	1 .2		fattack	
0.10 ъ/2	0 1.5 1.0 7.0 10.0 20.0 30.0 50.0 60.0 70.0 80.0 90.0	14°	16° -4.90 -3.97 -4.80 -1	18° -3.69 -4.86 -4.86 -4.15 -4.95 -4.15 -4.95 -4.57 -4.57 -4.57 -4.57	20 4.53 611 7.53 61 7.		0.50 .72 .53 .50 .42 .39 .39 .41	16° 0.38 .73 .67 .58 .45 .41 .44 .54	18° 0.21 .73 -72 .63 .78 .48 .47 .44 .46 .54	20° 0.04 .69 .76 .53 .51 .46 .49	
0.19 b/2	0 1.5 4.0 70.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	5.43 5.17 -3.57 -2.57 -1.12 98 63 540 540 540	-6.82 -5.78 -2.78 -2.86 -1.14 -2.77 -7.76 -54 -35	57 11 04 08 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-6.01 -2.83 -1.79 -1.63 -1.77 -1.71 -1.43 -1.77 -2.77 -2.77 -2.77 -2.78		48 47 76 76 60 44 38 35 35 35 35 35	-92 -35 -78 -77 -57 -50 -42 -38 -42 -47 -54	- 79 - 41 - 81 - 89 - 52 - 45 - 48 - 52	-91 -91 -83 -82 -73 -56 -47 -40 -44 -34	
0.31 b/2	0 1.5 4.0 7.0 15.0 20.0 20.0 20.0 20.0 20.0 20.0 20.0 2	3.87 5.238 61.256 1.65 1.1.26 1.26 1.26 1.65	153534341111111111111111111111111111111	55589939894993949888	5.59 -5.23 -4.95 -4.35 -4.35 -4.35 -4.13 -4.13 -4.13 -4.71		.12 .68 .63 .58 .50 .43 .40 .41	67 759 .64 57 43 49 57	-23 -65 -78 -78 -59 -46 -44 -50	- 27 .67 .83 .76 .70 .52 .44 .44 .49 .59	
0.315 b/2	0 1.5 4.0 7.0 15.0 20.0 30.0 40.0 70.0 60.0 90.0	5.88 5.87 7.38 7.19 7.19 7.19 7.19 7.19 7.19 7.19 7.19	-6.11 -6.01 -3.38 -2.45 -1.20 -1.03 -1.04 -1.02 -1.03 -1.04 -1.02 -1.03 -1.04 -1.02 -1.03 -1.04 -1.02 -1.03	\$3884431 8588888 \$5997777 777 177	444444 P C C C C C C C C C C C C C C C C		.43 .50 .66 .58 .50 .45 .45 .41 .52	.550 .666 .606 .533 .404 .404 .3950	7.46 7.864.55.9 1.14 39.50	137 1288568 145 145	
0.4* b/2	0 1.5 4.0 79.0 150.0 20.0 40.0 76.0 76.0 76.0 76.0 76.0 76.0 76.0 7	-4.88 -2.73 -1.59 -1.43 -1.43 -1.43 -1.43 -1.43 -1.45	18 1.14 98 99 1.17 1.18 1.19 1.19 1.19 1.19 1.19 1.19 1.19	୫% ୫% ୫% ୫% ୯୯୭ ୭୯୭ ୭୯୭ ୧୯୯୬ ୧୯୯୬ ୧୯୯୭ ୧୯୯୭ ୧୯୯୭ ୧୯	89 95 55 55 50 95 55 56 95 56 55 56 55 56 55 56 55 56 55 56 55 56 56		760 -54 -77 -78 -48 -40 -37 -36 -39 -43 -50	44 PPB28888 25	្តី ខ្លួននុក្សង ខ្លួ	198 8588888 1955 1981 86888888 1955	

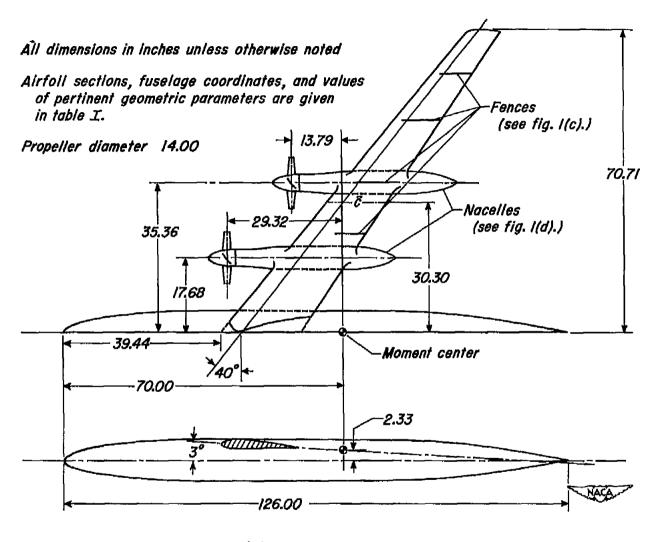




TABLE XIX.- PRESSURE COEFFICIENTS AT NINE SPANWISE STATIONS OF THE WING. M = 0.082; R = 4,000,000; PROPELLERS REMOVED - Concluded (b) $\alpha_{\rm u}$ = 14°, 16°, 18°, 20° - Concluded

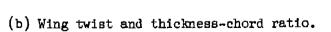
	Per-	Upper surface							Lower surface					
Spanvise stations	cent chord				fattack				- X		fattack			
0.56 ъ/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 95.0	14° 88 49 550 12 7 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	थ त्रुष्ट्रक्ष्ण्यम् । । । । । । । । । । । । । । । । । । ।	8 8 2 2 2 2 2 4 8 5 8 2 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	ତ୍ର ଚନ୍ଦ୍ରଶ୍ନ୍ୟ ଅଞ୍ଚଳ ଅନ୍ୟୁଷ୍ଟ ସମୟ ଅନ୍ୟର ଜଣ ହେଉଛି । ଜଣ			14° 0.15 .6663 .55 .50 .40 .33 .2901 .18	16° 0.10 0.57 -52 -43 -30 -01 -01 -09	18°	20° -0.12 -65 -71 -65 -59 -10 -10 -10 -10 -10 -10			
o.68 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	\$\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	%55944895588948 45594477711111	3853\$855555\$8888 F\$4774111111	\$			33 48 59 49 36 30 23 19 10	.34	99 .31 .57 .55 .51 .42 .36 .21 .26 .21 .09	59 .45 .56 .56 .51 .41 .35 .24 .18 .03 06			
0.80 b/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 90.0	54.564.5638.868.8888.8111	55.955888888888 55.955888888888888888888	6.50.55 6.4.95 6.7.4.3.4.15 7.7.15 7.7.15 7	-3.88 -1.14 -1.13			11 -51 -53 -43 -34 -24 -20 -15 -15	.44 .56 .50 .46 .38 .27 .24 .19	-, 48 . 46 . 59 . 52 . 48 . 40 . 24 . 18 . 11 . 04				
0.94 5/2	0 1.5 4.0 7.0 10.0 15.0 20.0 30.0 40.0 50.0 60.0 70.0 80.0 90.0	-3.80 -3.21 -2.53 -2.01 -1.65 -1.32 -1.76 -1.76 -1.79 -1.43 -1.33 -1.11 -1.06 -1.06	5-1-9-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-	-5.18 -3.59 -2.60 -1.85 -1.11 -65 -543 -543 -543 -543 -1.55	-2.29 -1.52 -1.18 93 84 77 59 47 55 47 35 33			.12 .55 .49 .41 .34 .24 .16 .24 .16 .05 .05	14 56 .53 .45 .37 .29 .20 .16		20 54 .49 .41 .24 .18 .12 04 0			

COATT



(a) Dimensions.

Figure 1.- Geometry of the model.



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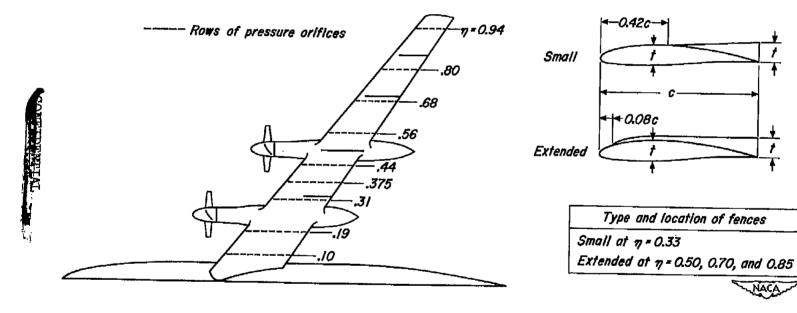
Fraction of semispan, $\frac{y}{b/2}$

Figure 1.- Continued.

Thickness-chord ratio, (1/c)

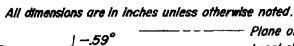
.2

.3

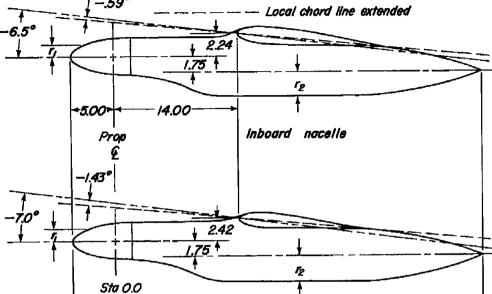


(c) Location of pressure-orifice stations and details of the four-fence configuration.

Figure 1.- Continued.

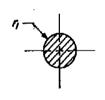


- Plane of root chord and L.E. of wing

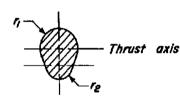


Outboard nacelle

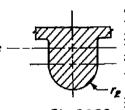
47.25



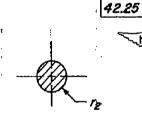
Sta 0.0



Sta 6.00



Sta 24.00



Nacelle coordinates

.385

.567

.788

.951

1.242

1.472

1.670

1.871 1.985

2.100

2.100

Sta

-500

-479

-458

-4.25 -3.95

-325

-255 -1.80

- .80

200

12.00

0

Sta

300

4.00

5.00

6.00

7.00

2.00 0.350

.419

.6/6

919

1.290

1.685

8.00 2.056

9.00 2.359 10.00 2.556

11.00 2.625

30.50 2.625

32.50 2.450

34.50 2.220 36.50 1.825

1.270

.675

.275

38.50

40.50

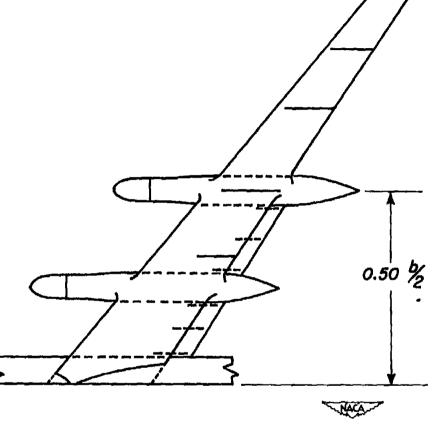
41.50

Sta 36.00

(d) Dimensions of the nacelles.

Figure 1.- Continued.

Typical section through flap and normal to reference sweep line



(e) Flap details.

Figure 1.- Concluded.

Developed plan form

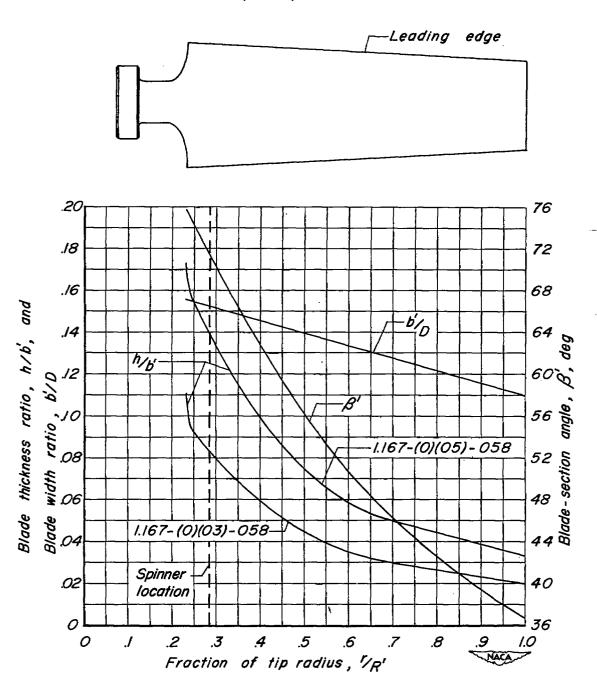
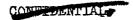


Figure 2.- Blade-form curves for the NACA 1.167-(0)(05)-058 and the NACA 1.167-(0)(03)-058 three-blade propellers.





A-17525.2

Figure 3.- Model mounted in the wind tunnel.



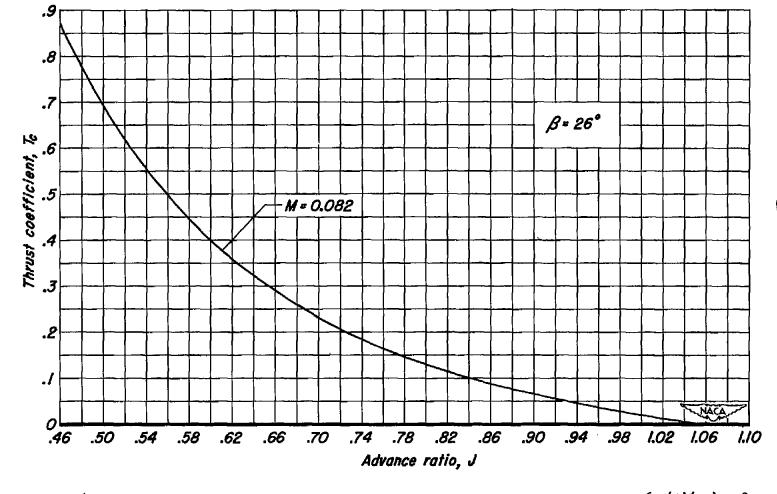


Figure 4.- The variation of thrust coefficient with advance ratio for the NACA 1.167-(0)(05)-058 propeller. Thrust axis parallel to the air stream. M = 0.082, R = 4,000,000.

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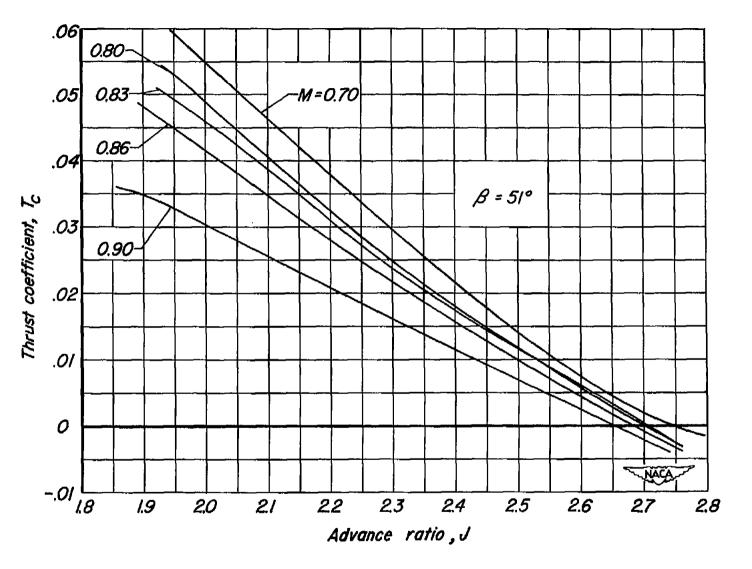


Figure 5.- The variation of thrust coefficient with advance ratio for the NACA 1.167-(0)(03)-058 propeller for several Mach numbers. Thrust axis parallel to the air stream. R = 1,000,000.

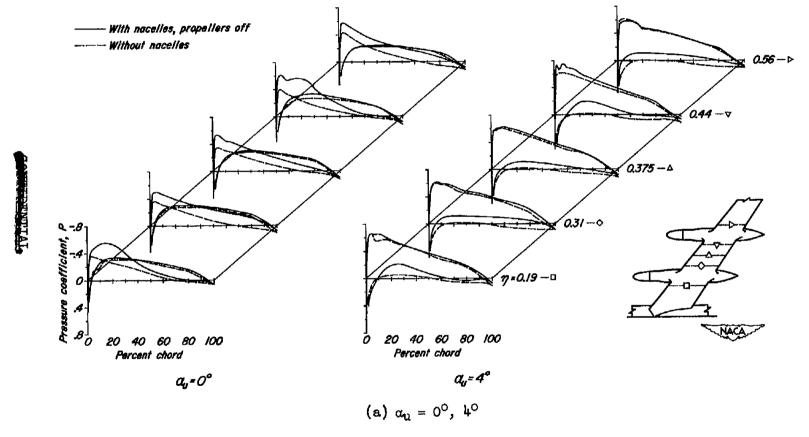


Figure 6.- A comparison of the chordwise distributions of pressure coefficient at five semispan stations of the wing for the wing-fuselage and the wing-fuselage-nacelles configurations. M = 0.165, R = 8,000,000.

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\$ 1.7r

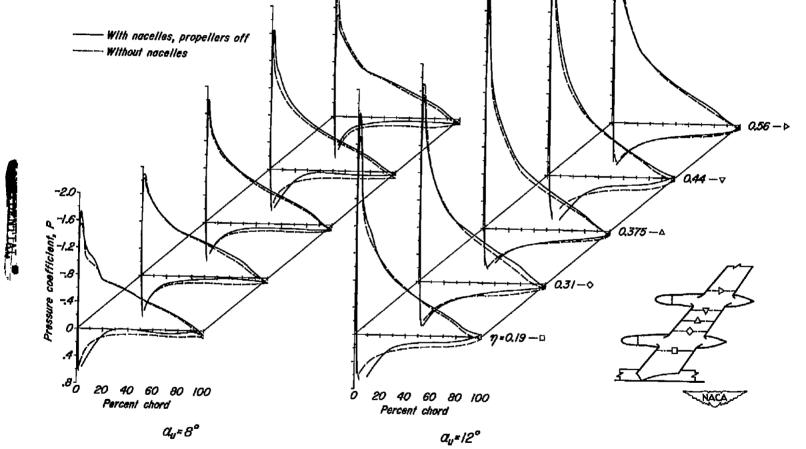


Figure 6.- Continued.

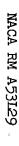
(b) $\alpha_u = 8^{\circ}$, 12°

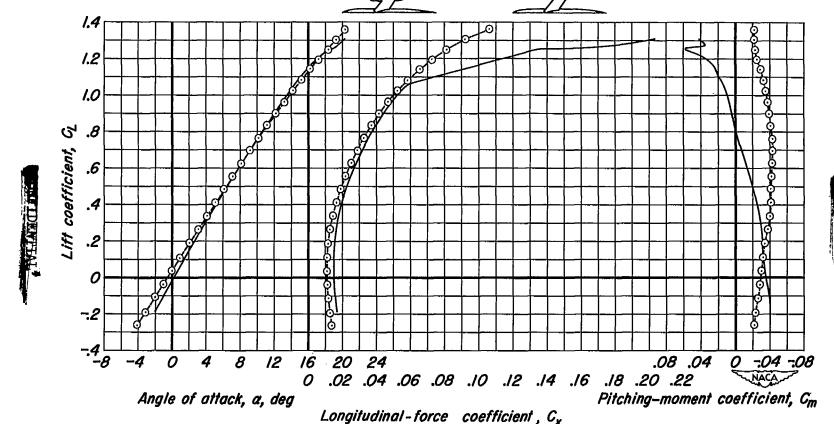


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Figure 6.- Concluded.

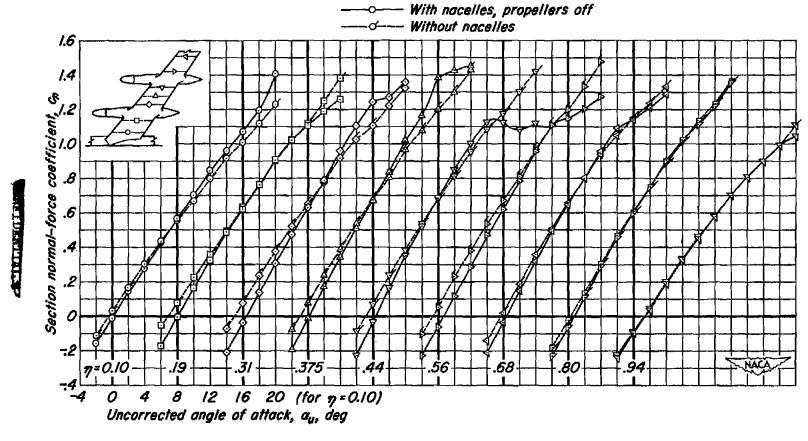
(c) $\alpha_{\rm u} = 16^{\rm o}$, $20^{\rm o}$





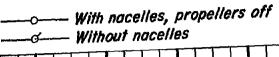
(ref. 4)

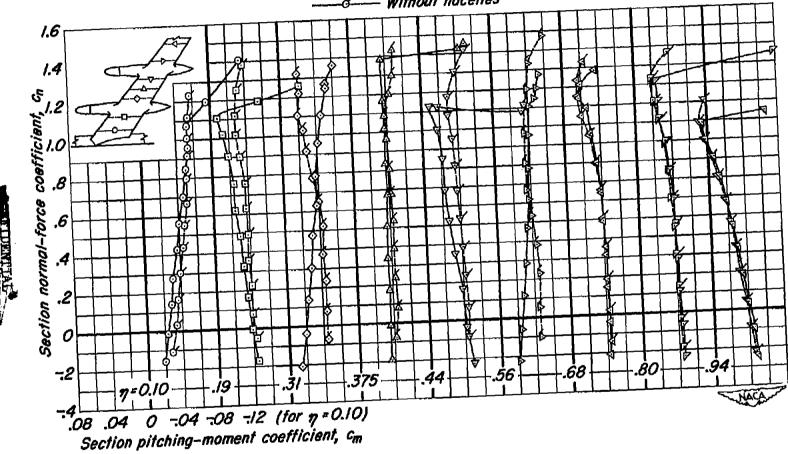
Figure 7.- A comparison of the aerodynamic characteristics of the wing-fuselage and wing-fuselage-nacelles configurations and their corresponding section normal-force and section pitching-moment characteristics at nine semispan stations of the wing. M = 0.165, R = 8,000,000.



(b) Section normal force.

Figure 7.- Continued.





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(c) Section pitching moment.

Figure 7.- Concluded.

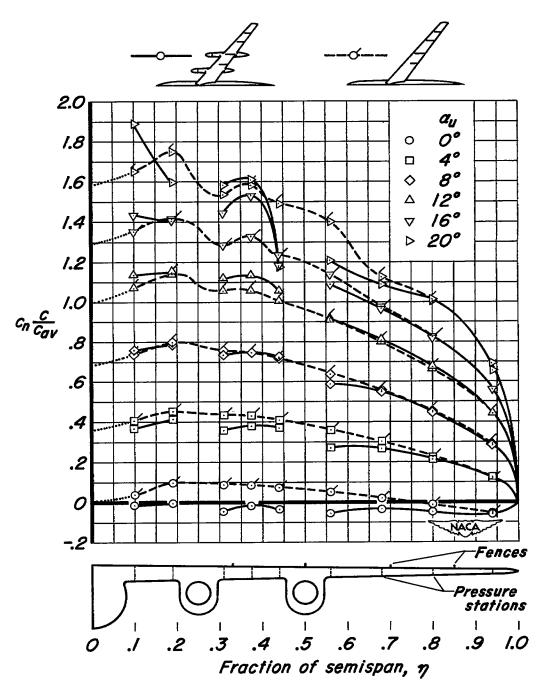
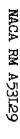
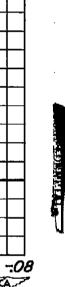


Figure 8.- The spanwise distribution of $c_n \frac{c}{c_{av}}$ as affected by the addition of nacelles to the wing-fuselage combination for several angles of attack. M = 0.165, R = 8,000,000.







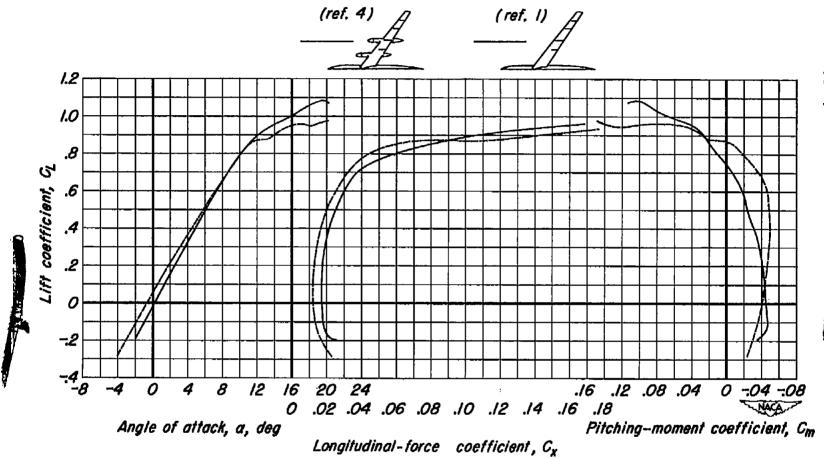
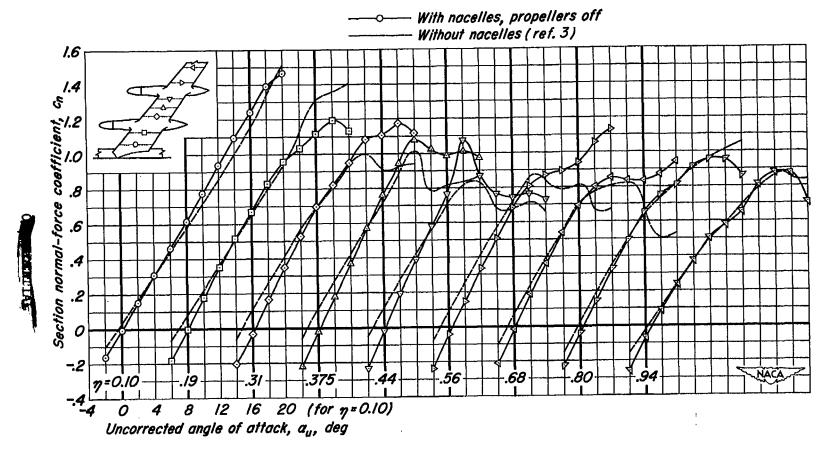
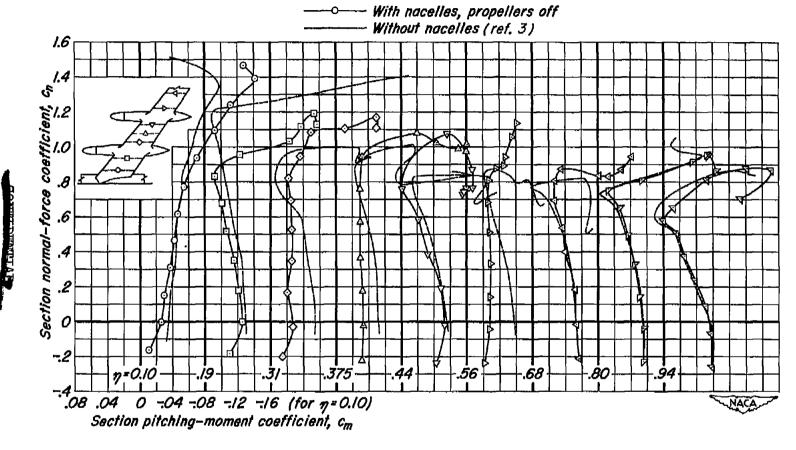


Figure 9.- A comparison of the aerodynamic characteristics of the wing-fuselage and wing-fuselagenacelles configurations and their corresponding section normal-force and section pitchingmoment characteristics at nine semispan stations of the wing. M = 0.60, R = 2,000,000.



(b) Section normal force.

Figure 9.- Continued.



(c) Section pitching moment.

Figure 9.- Concluded.

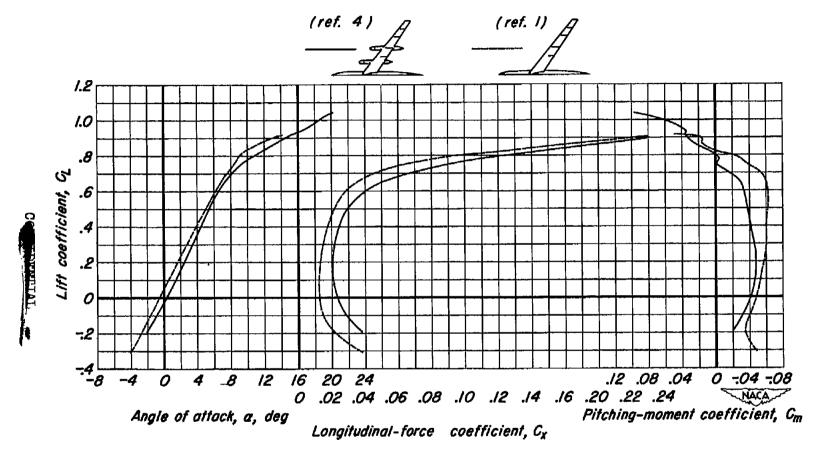
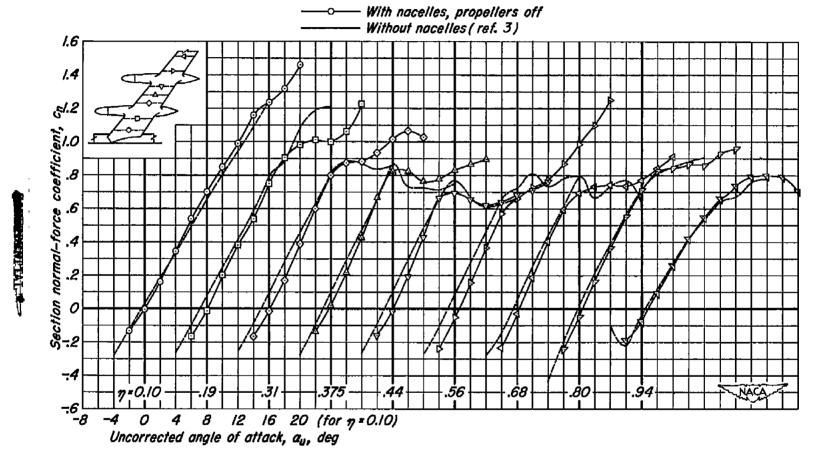
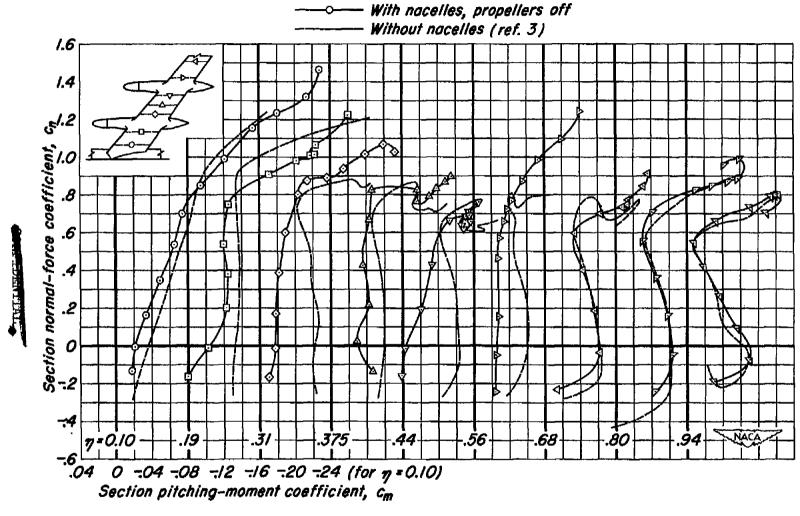


Figure 10.- A comparison of the aerodynamic characteristics of the wing-fuselage and wing-fuselage-nacelles configurations and their corresponding section normal-force and section pitching-moment characteristics at nine semispan stations of the wing. M = 0.80, R = 2,000,000.



(b) Section normal force.

Figure 10.~ Continued.



(c) Section pitching moment.

Figure 10.- Concluded.

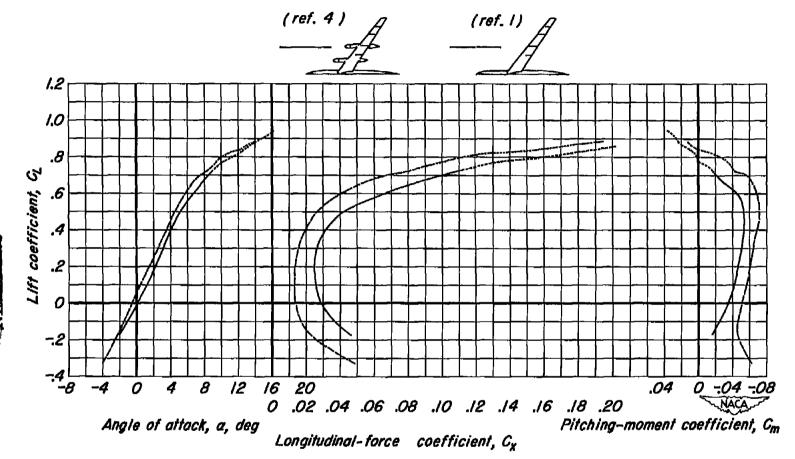
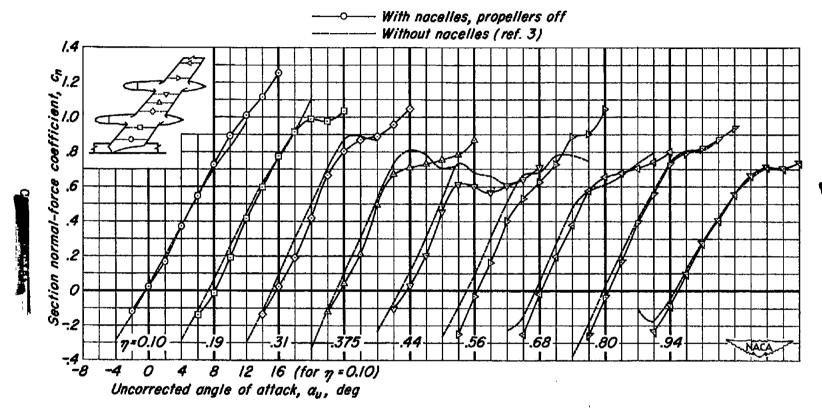


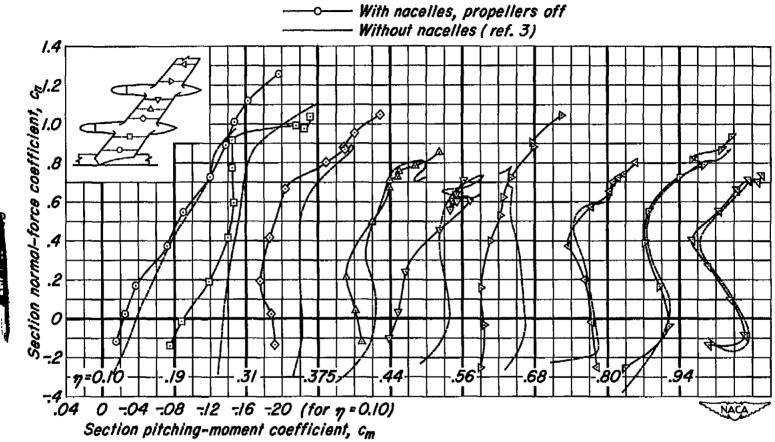
Figure 11.- A comparison of the aerodynamic characteristics of the wing-fuselage and wing-fuselage-nacelles configurations and their corresponding section normal-force and section pitching-moment characteristics at nine semispan stations of the wing. M = 0.86, R = 2,000,000.



(b) Section normal force.

Figure 11.- Continued.





(c) Section pitching moment.

Figure 11 .- Concluded.

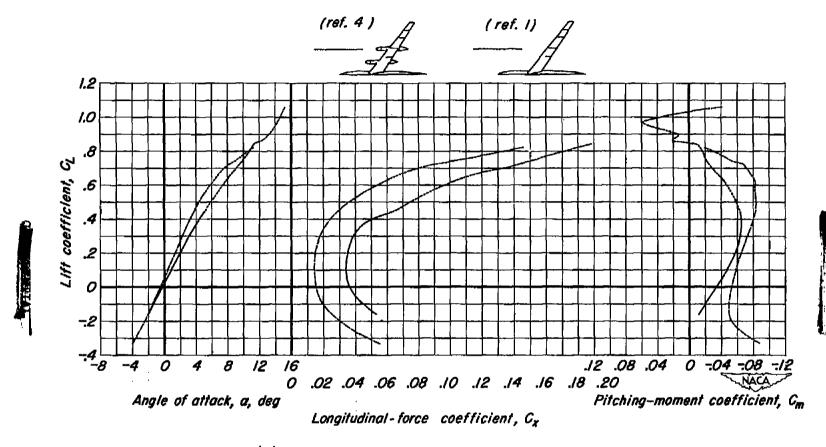
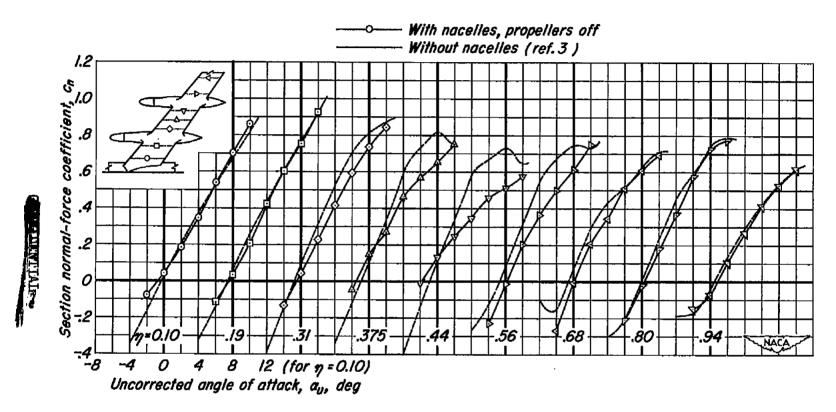
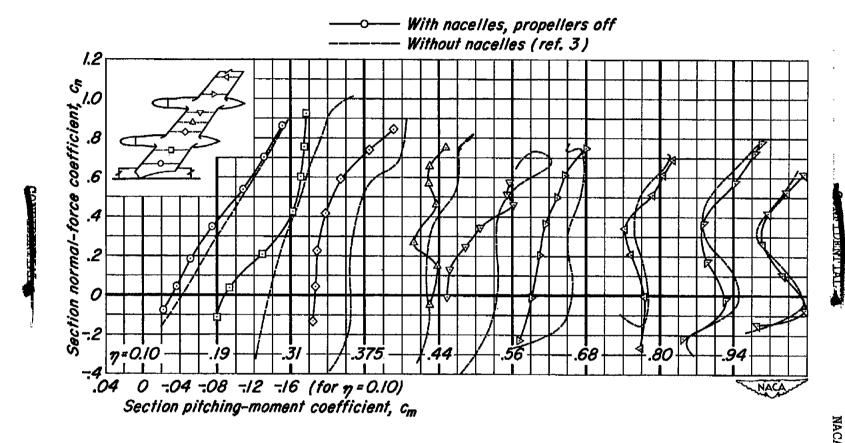


Figure 12.- A comparison of the aerodynamic characteristics of the wing-fuselage and wingfuselage-nacelles configurations and their corresponding section normal-force and section pitching-moment characteristics at nine semispan stations of the wing. M = 0.90, R = 2,000,000.



(b) Section normal force.

Figure 12. - Continued.



(c) Section pitching moment.

Figure 12.- Concluded.

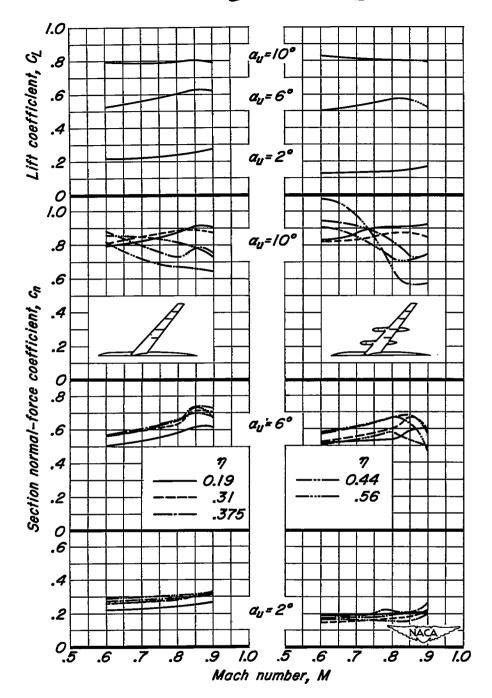
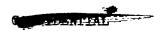


Figure 13.- The variations with Mach number of the lift coefficient and the section normal-force coefficient for several angles of attack of the wing-fuselage and the wing-fuselage-nacelles combinations. R = 2,000,000.





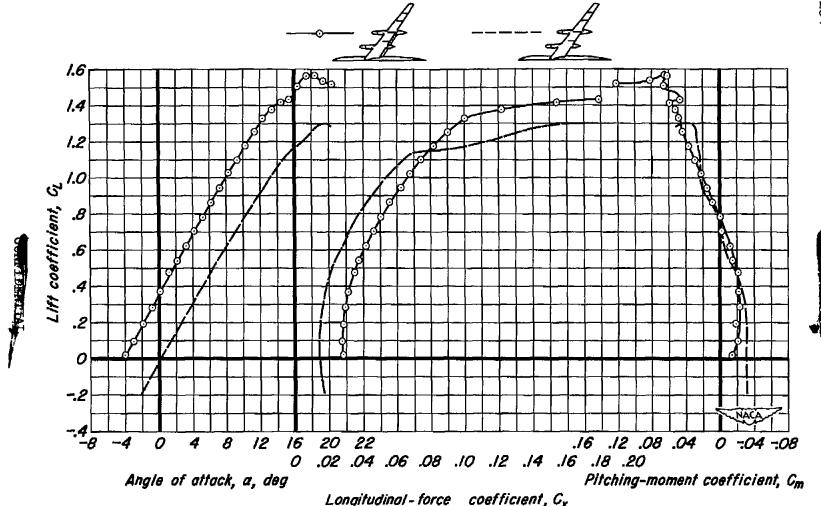
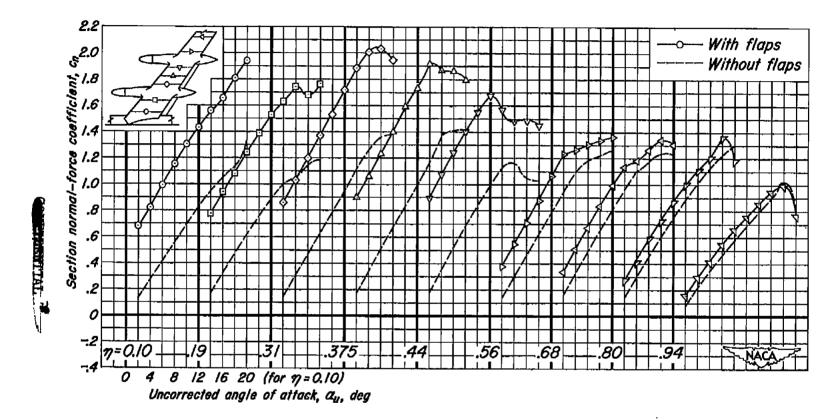
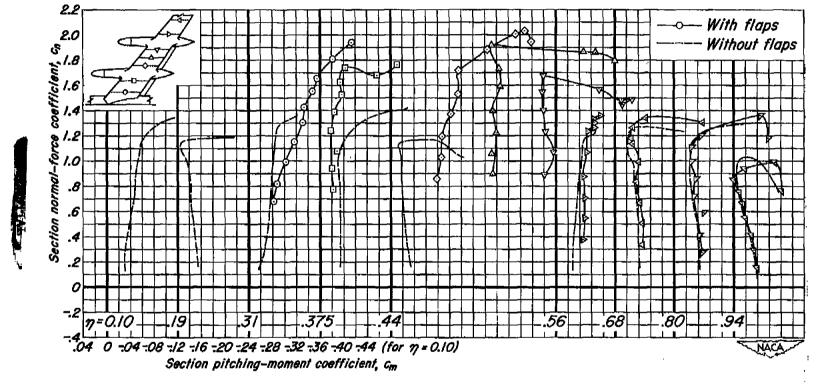


Figure 14.- The effect of flaps on the aerodynamic characteristics of the wing-fuselage-nacelles configuration and on the corresponding section normal-force and section pitching-moment characteristics at nine semispan stations of the wing. $\delta = 30^{\circ}$, M = 0.082, R = 4,000,000.



(b) Section normal force.

Figure 14. - Continued.



(c) Section pitching moment.

Figure 14.- Concluded.

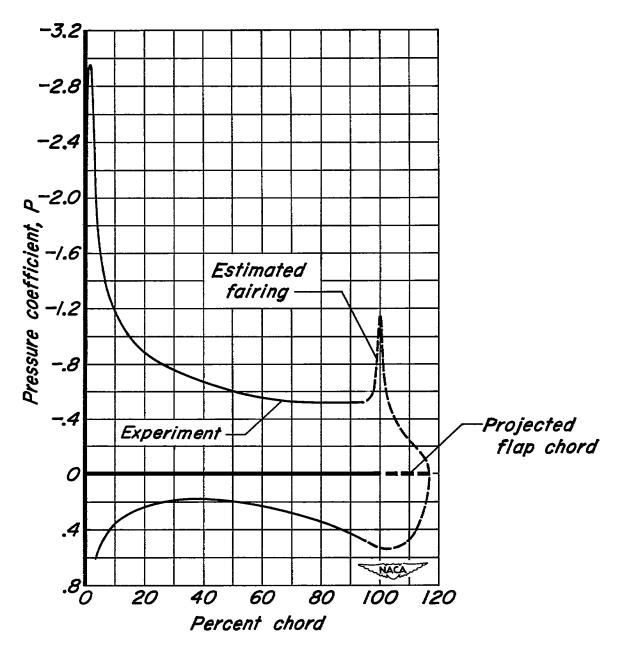


Figure 15.- Representative distribution of pressure coefficient for sections having a trailing-edge flap. δ = 30°, M = 0.082, R = 4,000,000.



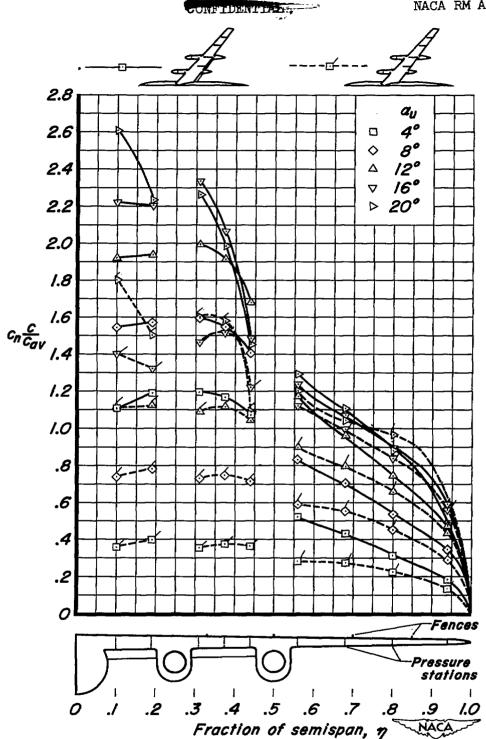


Figure 16.- The effect of flap deflection on the spanwise distribution of $c_n \frac{c}{c_{av}}$ for the wing-fuselage-nacelles configuration at several angles of attack. M = 0.082, R = 4,000,000.





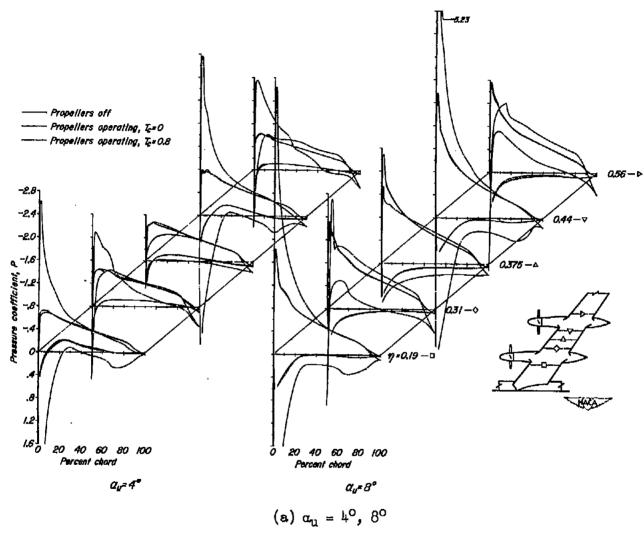


Figure 17.- The effect of increasing thrust coefficient on the chordwise distributions of pressure coefficient at five semispan stations of the wing. M = 0.082, R = 4,000,000.

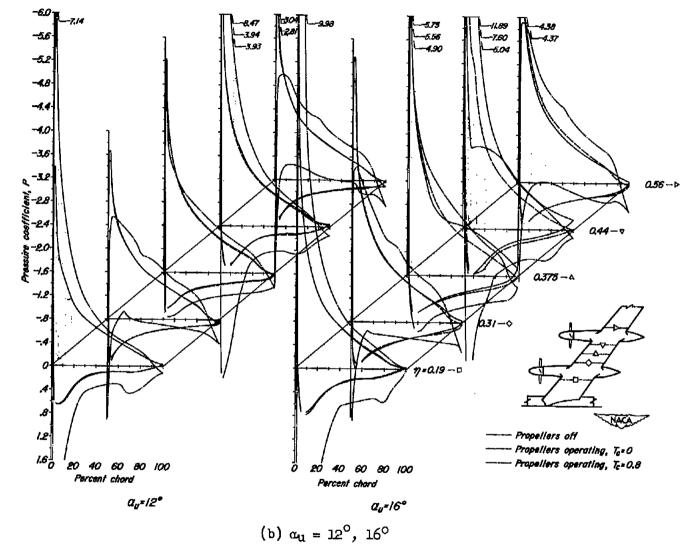


Figure 17.- Concluded.

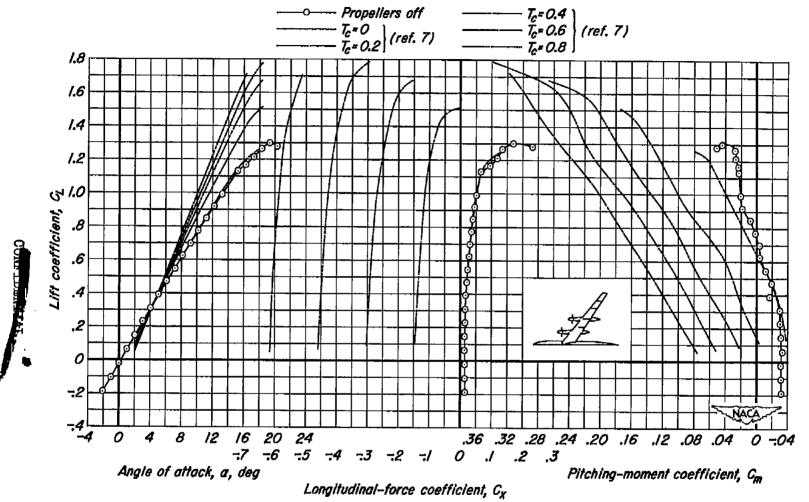
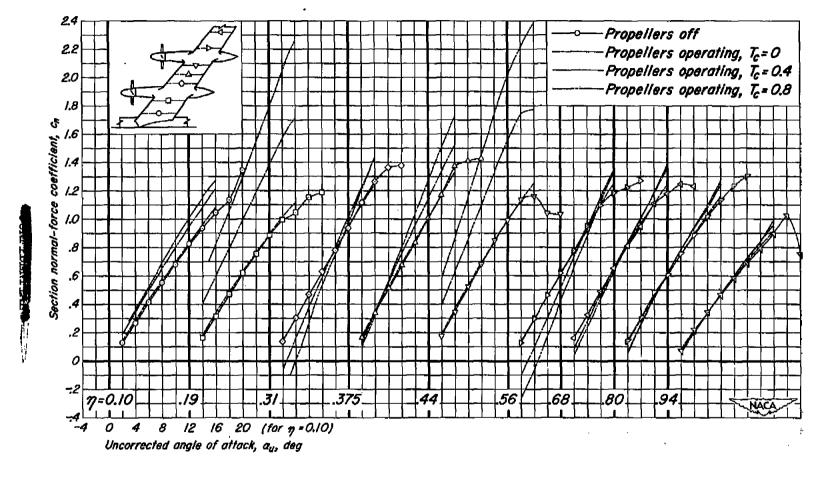


Figure 18.- The effect of increasing thrust coefficient on the aerodynamic characteristics of the wing-fuselage-nacelles configuration and the corresponding section normal-force and section pitching-moment characteristics at nine semispan stations of the wing. M = 0.082, R = 4,000,000.

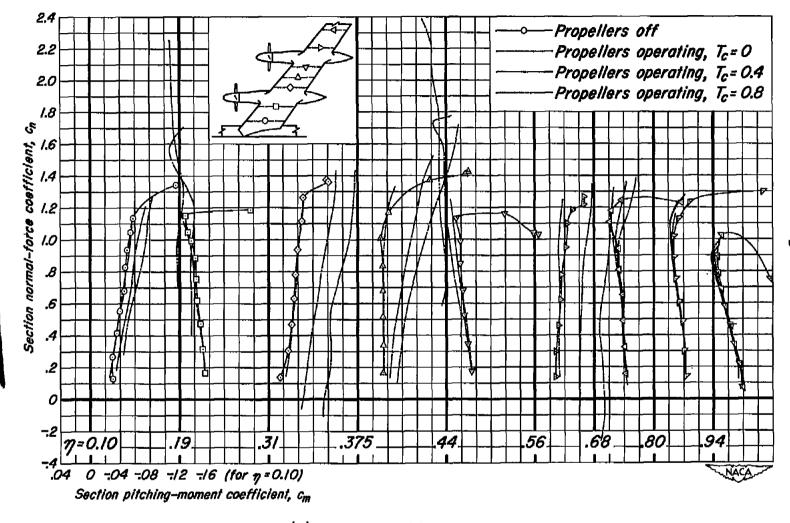
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(b) Section normal force.

Figure 18.- Continued.

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(c) Section pitching moment.

Figure 18.- Concluded.

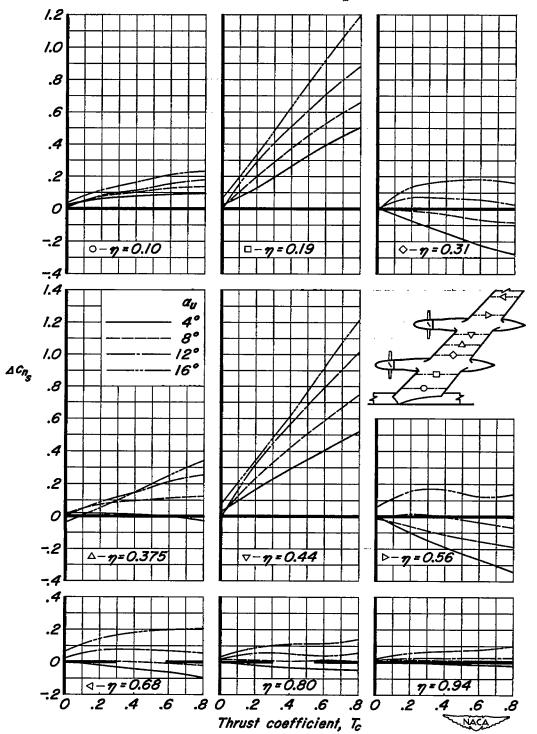


Figure 19.- The variations with thrust coefficient of the changes in section normal-force coefficient. M = 0.082, R = 4,000,000.



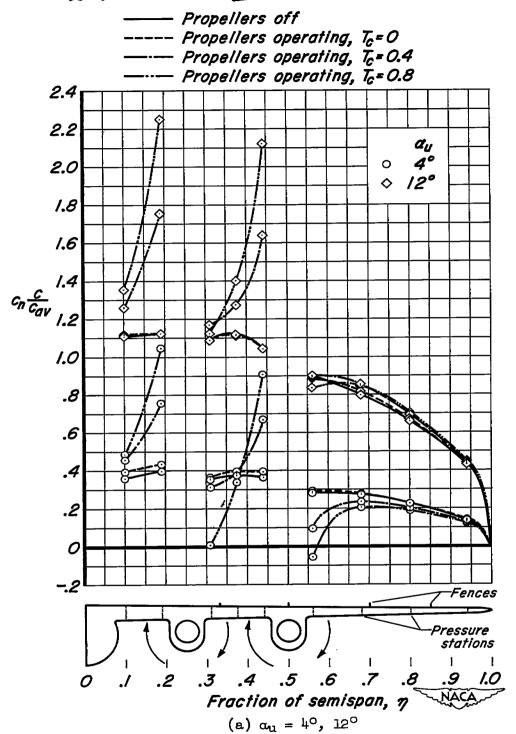


Figure 20.- The spanwise distribution of $c_n \frac{c}{c_{av}}$ as affected by thrust coefficient for several angles of attack. M = 0.082, R = 4,000,000.



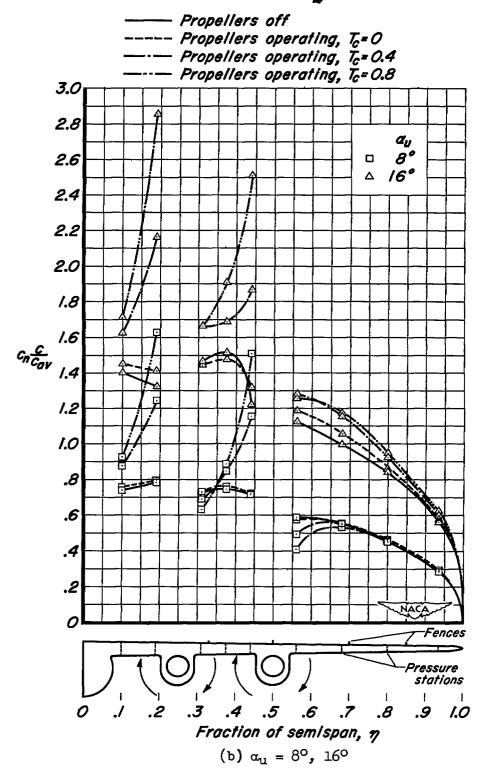


Figure 20.- Concluded.

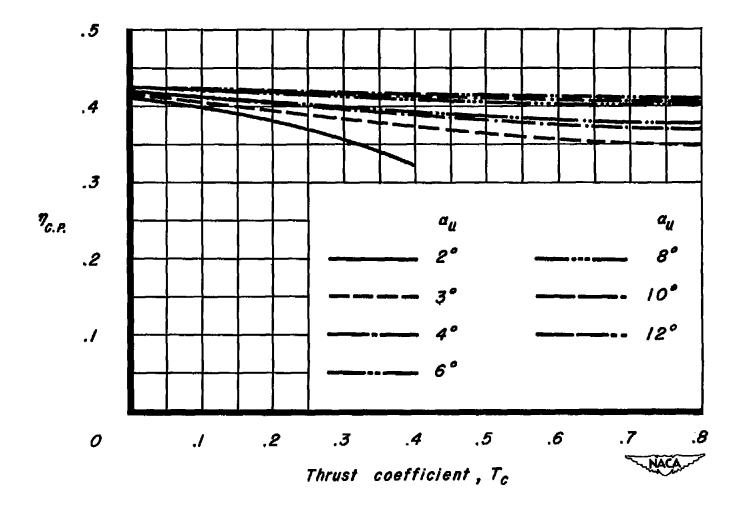


Figure 21.- The variation of the spanwise location of the center of pressure with thrust coefficient. M = 0.082, R = 4,000,000.

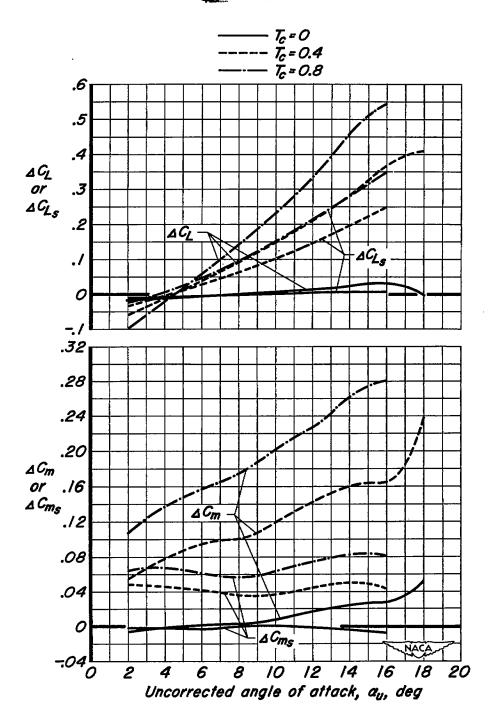


Figure 22.- The variation with angle of attack of the changes in the lift and pitching-moment coefficients due to increasing thrust coefficient and that due to propeller slipstream. M = 0.082, R = 4,000,000.



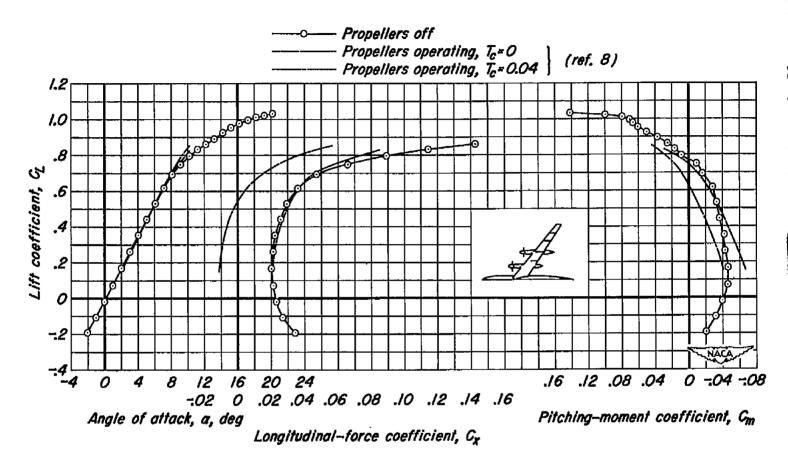
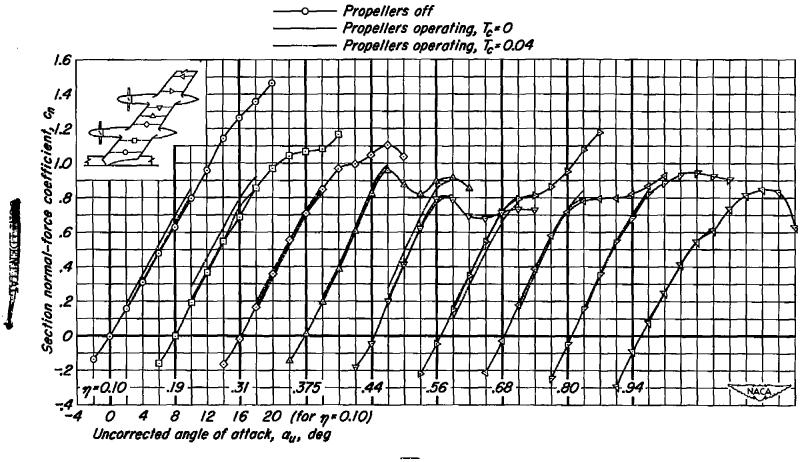


Figure 23.- The effect of increasing thrust coefficient on the aerodynamic characteristics of the wing-fuselage-nacelles configuration and the corresponding section normal-force and section pitching-moment characteristics at nine semispan stations of the wing. M = 0.70, R = 1,000,000.



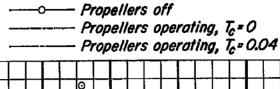
(b) Section normal force.

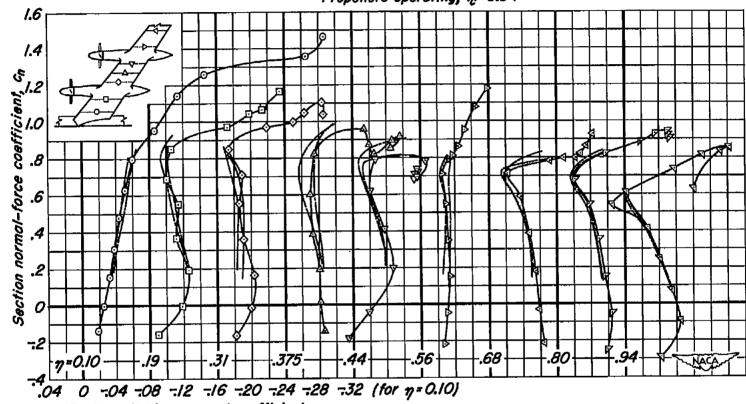
Figure 23.- Continued.

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Section pitching-moment coefficient, cm

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(c) Section pitching moment.

Figure 23.- Concluded.

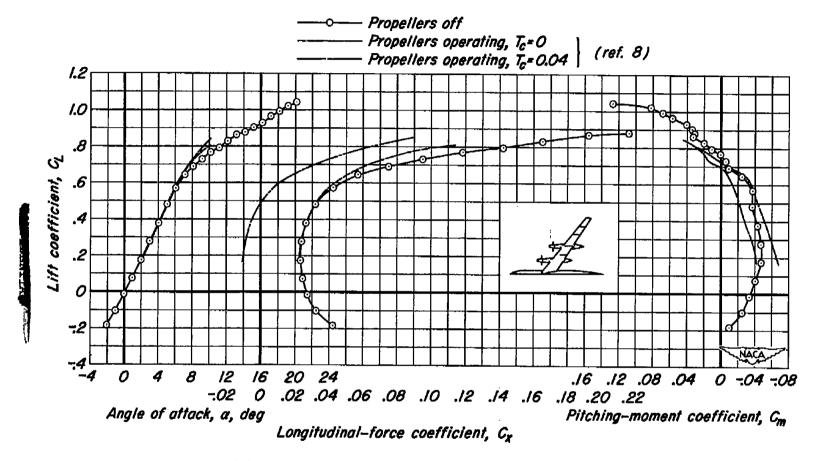
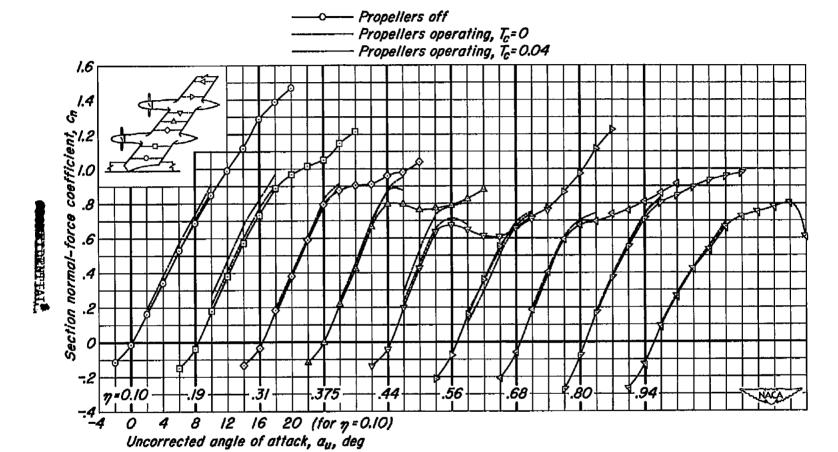
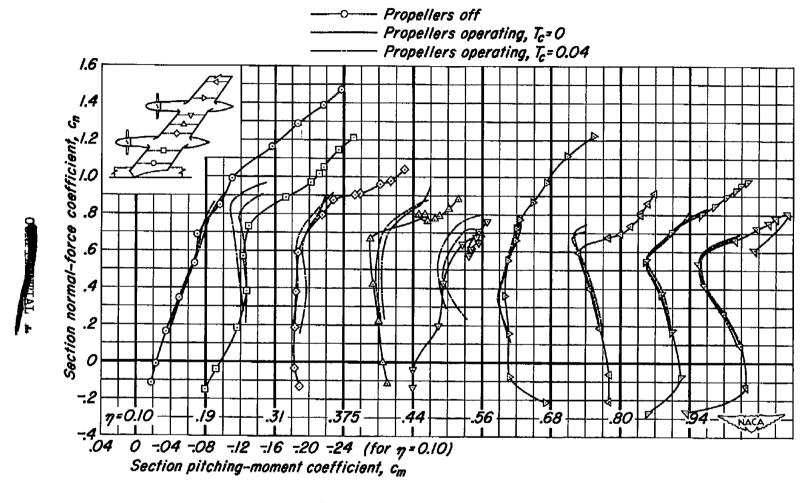


Figure 24.- The effect of increasing thrust coefficient on the aerodynamic characteristics of the wing-fuselage-nacelles configuration and the corresponding section normal-force and section pitching-moment characteristics at nine semispan stations of the wing. M = 0.80, R = 1,000,000.



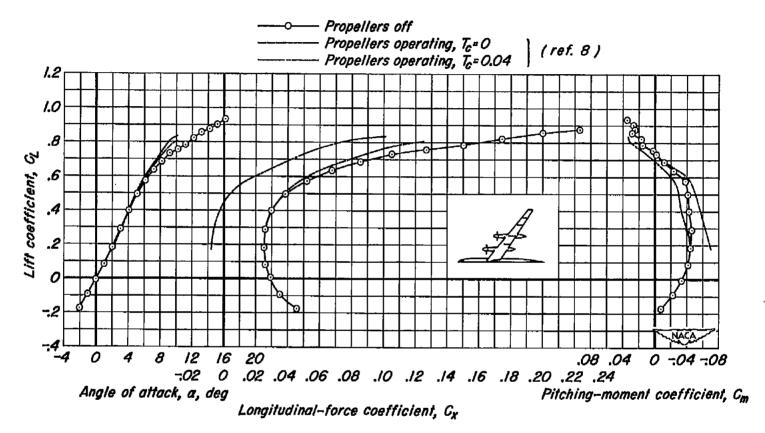
(b) Section normal force.

Figure 24.- Continued.



(c) Section pitching moment.

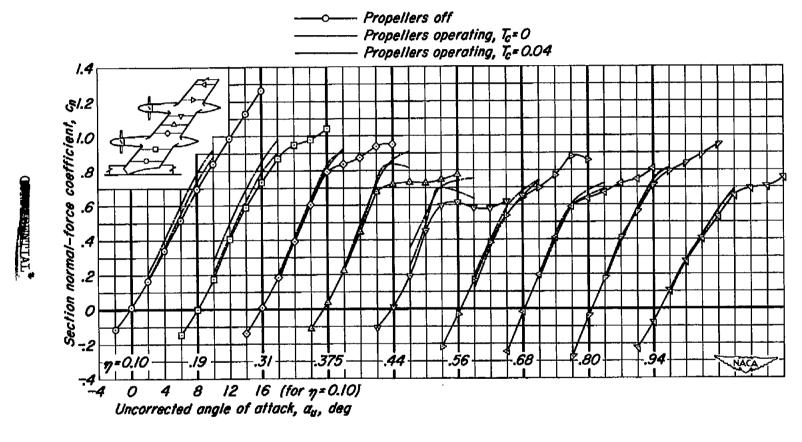
Figure 24.- Concluded.



(a) Lift, longitudinal force, and pitching moment.

Figure 25.- The effect of increasing thrust coefficient on the aerodynamic characteristics of the wing-fuselage-nacelles configuration and the corresponding section normal-force and section pitching-moment characteristics at nine semispan stations of the wing. M = 0.83, R = 1,000,000.

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(b) Section normal force.

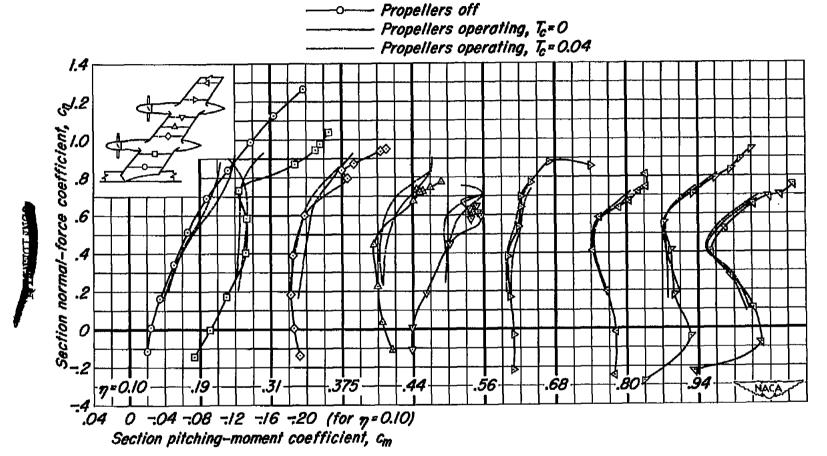
Figure 25.- Continued.

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(c) Section pitching moment.

Figure 25.- Concluded.

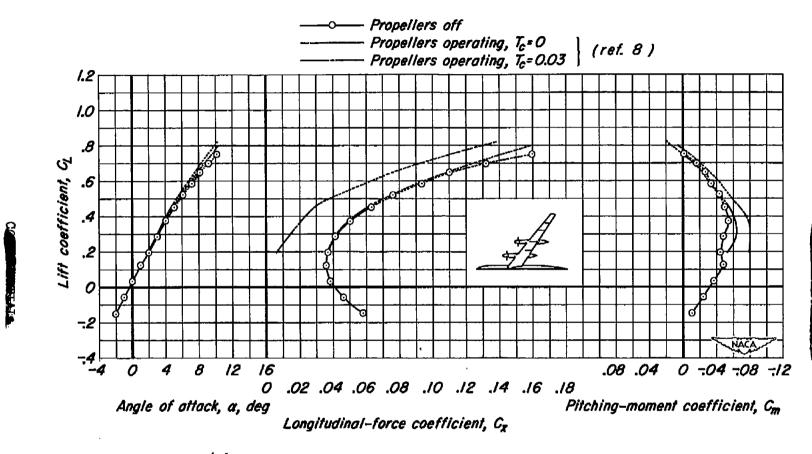
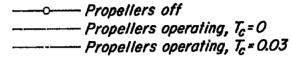
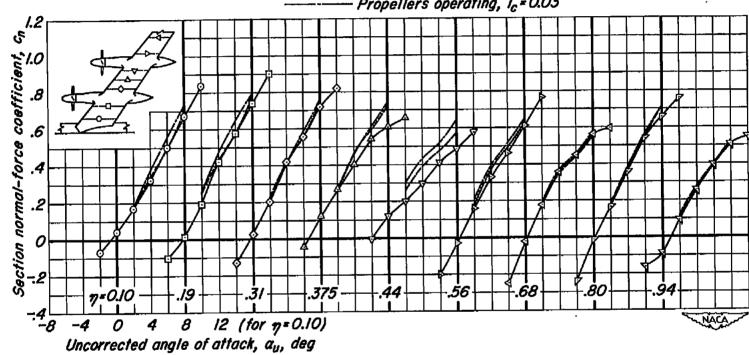


Figure 26.- The effect of increasing thrust coefficient on the aerodynamic characteristics of the wing-fuselage-nacelles configuration and the corresponding section normal-force and section pitching-moment characteristics at nine semispan stations of the wing. M = 0.90, R = 1,000,000.

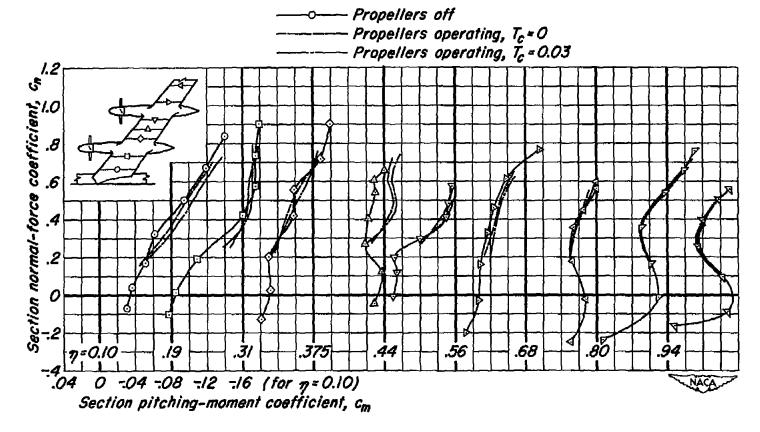




(b) Section normal force.

Figure 26.- Continued.

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(c) Section pitching moment.

Figure 26.- Concluded.

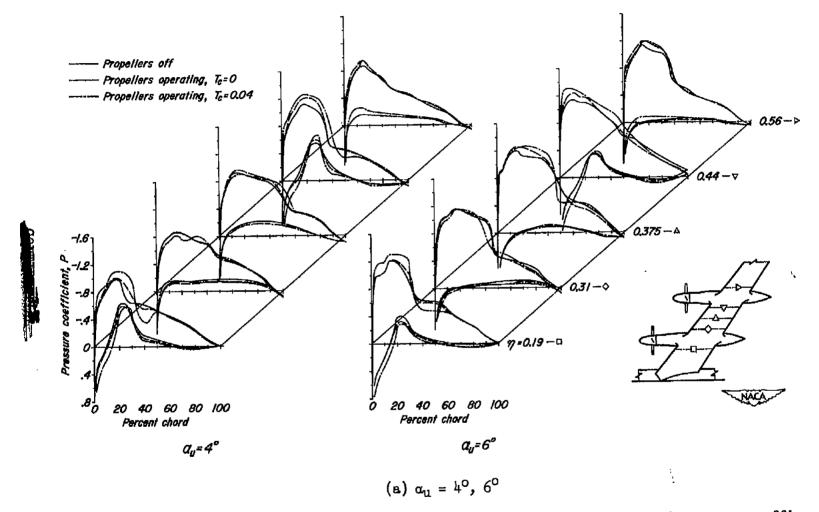


Figure 27.- The effect of thrust coefficient on the chordwise distributions of pressure coefficient at five semispan stations of the wing. M = 0.80, R = 1,000,000.

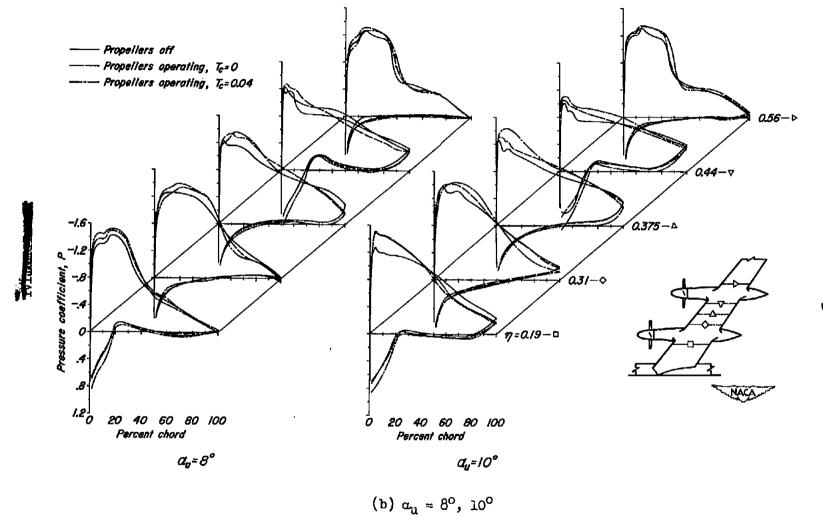


Figure 27.- Concluded.

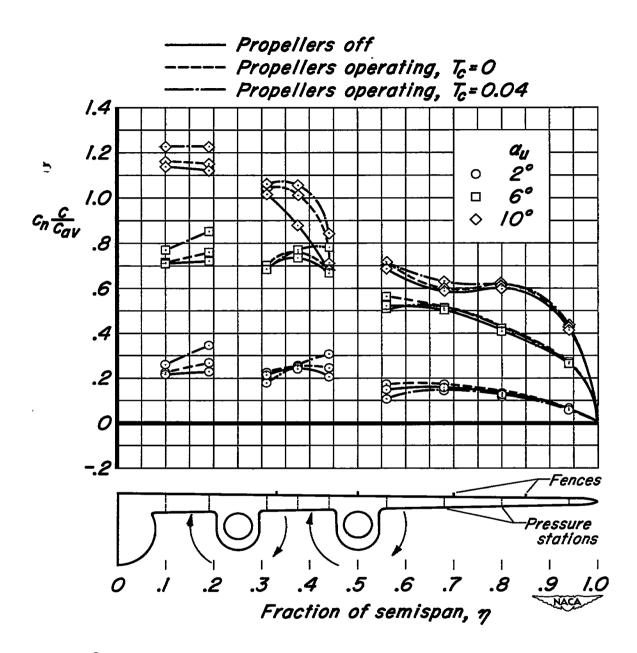


Figure 28.- The effect of thrust coefficient on the spanwise distribution of $c_n \frac{c}{c_{av}}$ for three angles of attack. M = 0.80, R = 1,000,000.